## NASA TECHNICAL NOTE



NASA TN D-5805

C . 1



LOAN COPY: RETURN TO AFWL (WLOL) KIRTLAND AFB, N MEX

BUFFET AND STATIC AERODYNAMIC CHARACTERISTICS OF A SYSTEMATIC SERIES OF WINGS DETERMINED FROM A SUBSONIC WIND-TUNNEL STUDY

by Edward J. Ray and Robert T. Taylor Langley Research Center Hampton, Va. 23365

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION • WASHINGTON, D. C. • JUNE 1970

1. Report No.		0132569								
NASA TN D-5805	2. Government Accession No.	3. Recipient's Catalog No.								
	ODYNAMIC CHARACTERISTICS OF	5. Report Date June 1970								
A SYSTEMATIC SERIES OF SUBSONIC WIND-TUNNEL S	WINGS DETERMINED FROM A STUDY	6. Performing Organization Code								
7. Author(s)  Edward I Ray and Robert T	Taylor	8. Performing Organization Report No.  L-7011								
Edward 9. Itay and Hobert 1	Edward J. Ray and Robert T. Taylor									
9. Performing Organization Name and Address	10. Work Unit No. 126-14-12-02-23									
NASA Langley Research Cer	nter	11. Contract or Grant No.								
Hampton, Va. 23365		it. Contract of Grant No.								
		10 T as of Barrier I Build Control								
12. Sponsoring Agency Name and Address		13. Type of Report and Period Covered								
National Aeronautics and Sp	ace Administration	Technical Note								
<u>-</u>	ace Administration	14. Sponsoring Agency Code								
Washington, D.C. 20546										
15. Supplementary Notes										
16. Abstract										
	estion has been conducted in the I am	rlow high ground 7 by 10 foot								
·	gation has been conducted in the Lang									
	et and static aerodynamic character									
series at Mach numbers rai	nging from $0.23$ to $0.94$ . The results									
Scries at mach numbers rai	iging from 0.20 to 0.04. The results	s nave indicated that for a								
	gs which display superior aerodynam									
given Mach number the wing	• •	ic efficiency characteristics								
given Mach number the wing generally display the highes	gs which display superior aerodynam	nic efficiency characteristics naracteristics exhibited by								
given Mach number the wing generally display the highes the wings which were consid	gs which display superior aerodynam t buffet-free lift coefficient. The ch dered have indicated that correlation	aracteristics exhibited by s can be made between the								
given Mach number the wing generally display the highes the wings which were considerated onset of buffeting and select	gs which display superior aerodynam t buffet-free lift coefficient. The character that correlation dered have indicated that correlation and divergences in the static aerodyn	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial								
given Mach number the wing generally display the highes the wings which were considerated onset of buffeting and select	gs which display superior aerodynam t buffet-free lift coefficient. The ch dered have indicated that correlation	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial								
given Mach number the wing generally display the highes the wings which were considerated onset of buffeting and select	gs which display superior aerodynam t buffet-free lift coefficient. The character that correlation dered have indicated that correlation and divergences in the static aerodyn	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial								
given Mach number the wing generally display the highes the wings which were considerated onset of buffeting and select	gs which display superior aerodynam t buffet-free lift coefficient. The character that correlation dered have indicated that correlation and divergences in the static aerodyn	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial								
given Mach number the wing generally display the highes the wings which were considerated onset of buffeting and select	gs which display superior aerodynam t buffet-free lift coefficient. The character that correlation dered have indicated that correlation and divergences in the static aerodyn	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial								
given Mach number the wing generally display the highes the wings which were considerated onset of buffeting and select	gs which display superior aerodynam t buffet-free lift coefficient. The character that correlation dered have indicated that correlation and divergences in the static aerodyn	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial								
given Mach number the wing generally display the highes the wings which were considerated onset of buffeting and select	gs which display superior aerodynam t buffet-free lift coefficient. The character that correlation dered have indicated that correlation and divergences in the static aerodyn	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial								
given Mach number the wing generally display the highes the wings which were considerated onset of buffeting and select	gs which display superior aerodynam t buffet-free lift coefficient. The character that correlation dered have indicated that correlation and divergences in the static aerodyn	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial								
given Mach number the wing generally display the highes the wings which were considerated onset of buffeting and select	gs which display superior aerodynam t buffet-free lift coefficient. The character that correlation dered have indicated that correlation and divergences in the static aerodyn	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial								
given Mach number the wing generally display the highes the wings which were considerated onset of buffeting and select	gs which display superior aerodynam t buffet-free lift coefficient. The character that correlation dered have indicated that correlation and divergences in the static aerodyn	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial								
given Mach number the wing generally display the highes the wings which were considerated onset of buffeting and select	gs which display superior aerodynam t buffet-free lift coefficient. The character that correlation dered have indicated that correlation and divergences in the static aerodyn	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial								
given Mach number the wing generally display the highes the wings which were considerated onset of buffeting and select	gs which display superior aerodynam t buffet-free lift coefficient. The character that correlation dered have indicated that correlation and divergences in the static aerodyn	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial								
given Mach number the wing generally display the highes the wings which were considered onset of buffeting and select force has been found to be to	gs which display superior aerodynament buffet-free lift coefficient. The charmed have indicated that correlation and divergences in the static aerodynament he most sensitive static component to	tic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial o the onset of buffeting.								
given Mach number the wing generally display the highes the wings which were considered onset of buffeting and select force has been found to be to the select force has been found to be to the select force has been found to be to the select force has been found to be to the select force has been found to be to the select force has been found to be to the select force has been found to be the select force has been found to be the select force has been found to be the select force for the select force has been found to be the select force force has been found to be the select force f	gs which display superior aerodynam t buffet-free lift coefficient. The character that correlation dered have indicated that correlation and divergences in the static aerodyn	tic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial o the onset of buffeting.								
given Mach number the wing generally display the highes the wings which were considered onset of buffeting and select force has been found to be to be to be to be to be force (Suggested by Author(s)).  Buffet Thi Static aerodynamic r	t buffet-free lift coefficient. The chared have indicated that correlation and divergences in the static aerodynam he most sensitive static component to the component to the static aerodynam he most sensitive static component to the component to the component to the static aerodynam he most sensitive static component to the com	tic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial o the onset of buffeting.								
given Mach number the wing generally display the highes the wings which were considered onset of buffeting and select force has been found to be	ckness-to-chord atio of maximum	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial o the onset of buffeting.								
given Mach number the wing generally display the highes the wings which were considered onset of buffeting and select force has been found to be to see that the force has been found to see that the force has been force has been found to see that the force has been for	t buffet-free lift coefficient. The chared have indicated that correlation and divergences in the static aerodynam he most sensitive static component to the component to the static aerodynam he most sensitive static component to the component to the component to the static aerodynam he most sensitive static component to the com	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial o the onset of buffeting.								
given Mach number the wing generally display the highes the wings which were considered onset of buffeting and select force has been found to be	ckness-to-chord atio of maximum	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial o the onset of buffeting.								
given Mach number the wing generally display the highes the wings which were considered onset of buffeting and select force has been found to be to see that the second to be to see the second to be to see the second to be to see the second to secon	ckness-to-chord atio of maximum	nic efficiency characteristics naracteristics exhibited by s can be made between the amic characteristics. Axial o the onset of buffeting.								

# BUFFET AND STATIC AERODYNAMIC CHARACTERISTICS OF A SYSTEMATIC SERIES OF WINGS DETERMINED FROM A SUBSONIC WIND-TUNNEL STUDY

By Edward J. Ray and Robert T. Taylor Langley Research Center

#### SUMMARY

A wind-tunnel investigation has been conducted in the Langley high-speed 7- by 10-foot tunnel to determine the buffet and static aerodynamic characteristics of a systematic wing series at Mach numbers ranging from 0.23 to 0.94. The results have indicated that for a given Mach number the wings which display superior aerodynamic efficiency characteristics generally display the highest buffet-free lift coefficient. The characteristics exhibited by the wings which were considered have indicated that correlations can be made between the onset of buffeting and selected divergences in the static aerodynamic characteristics. Axial force has been found to be the most sensitive static component to the onset of buffeting.

#### INTRODUCTION

The maneuverability and performance of aircraft engaged in air-to-air combat at high subsonic speeds are limited by the flow separation on the wing which manifests itself in a buffeting of the airframe and pronounced increases in drag. There are several approaches which the designer of new aircraft may employ in order to alleviate buffeting and its effects. An obvious method is the use of low wing loadings; however, this approach is limited by such considerations as cruise performance, structural weight, gust response, and so forth. A more desirable approach would be to determine methods of increasing the lift coefficient at which buffeting occurs by proper selection of planform, airfoil section, and variable-geometry devices.

As a contribution to the information needed for a proper selection of wing design parameters such as planform and airfoil section, a research program has been conducted to study the effects of systematic variations in wing design parameters on buffeting tendencies. The primary method for determining buffeting onset in this study has been by the wing-root bending-gage technique. However, another objective of this study was to evaluate other methods of determining buffet onset, such as particular variations in the static aerodynamic characteristics.

The study made use of 11 buffet models covering systematic variations of sweep, thickness-to-chord ratio, position of maximum thickness, camber, and aspect ratio. The study has been conducted over a range of Mach number from a minimum of about 0.23 to a maximum of 0.94. The purpose of this paper is to present the results of this buffet research program and to interpret the various wind-tunnel measurements with respect to buffeting.

#### **SYMBOLS**

The coefficients of forces and moments for the plotted longitudinal aerodynamic results are referred to the stability axis system with the exception of the axial-force and normal-force coefficients, which are referred to the body axis system. In addition to the plotted presentation, tabulations of the static longitudinal and lateral characteristics utilizing both body and stability axis systems are presented herein. The static aerodynamic forces and moments have been nondimensionalized by using the individual geometric characteristics of each wing (shown in table I). Pitching moments are referred to the quarter-chord point of the individual wing mean geometric chords.

The units used for the physical quantities in this report are given both in the U.S. Customary Units and in the International System of Units (SI). Factors relating the two systems are given in reference 1.

Α	aspect ratio
b	wing span, in. (cm)
c	local chord of wing, in. (cm)
ē	mean geometric chord, in. (cm)
$c_{\mathbf{r}}$	wing root chord, in. (cm)
$\mathbf{c}_{t}$	wing tip chord, in. (cm)
$c_A$	axial-force coefficient, $\frac{Axial force}{qS}$
$(C_A)_{\alpha=0}$	axial-force coefficient at angle of attack of $0^{\rm O}$

 $C_{
m D}$  drag coefficient,  $\frac{{
m Drag}}{{
m qS}}$ 

 $\mathbf{C_{D.i}}$  theoretical induced-drag coefficient

 $C_L$  lift coefficient,  $\frac{Lift}{qS}$ 

 $C_{L_{\alpha}}$  lift-curve slope (near angle of attack of 00)

 $\mathbf{C_{L(L/D)}_{max}}$  lift coefficient at maximum lift-drag ratio

 $C_m$  pitching-moment coefficient,  $\frac{\text{Pitching moment}}{\text{qS\bar{c}}}$ 

 $\mathbf{c}_{\mathbf{m}_{\mathbf{C}_{\mathbf{L}}}}$  static margin (taken at low-lift coefficients),  $\frac{\partial \mathbf{c}_{\mathbf{m}}}{\partial \mathbf{c}_{\mathbf{L}}}$ 

 $c_N$  normal-force coefficient,  $\frac{Normal\ force}{qS}$ 

L/D lift-drag ratio

 $M_{WSg}$  root-mean-square moment of wing bending gage, in. lb (m-N)

q free-stream dynamic pressure,  $lb/ft^2$  (N/m<sup>2</sup>)

r radius, in. (cm)

R Reynolds number per foot (per meter)

S wing reference area, ft<sup>2</sup> (m<sup>2</sup>)

s ratio of actual to theoretical leading-edge suction force (ref. 2)

 $\alpha$  angle of attack, deg

 $\Lambda_{c/4}$  wing quarter-chord sweepback, deg

Subscript:

max

П

maximum

#### **ABBREVIATIONS**

FS fuselage station (measured from nose of model), in. (cm)

L.E. leading edge

rms root mean square

#### MODELS

A two-view sketch of the general model arrangement is shown in figure 1. The reference center of gravity was assumed to be in the plane of symmetry of the fuselage at the quarter-chord point of the wing mean geometric chords. The geometric characteristics of the various wings which were studied in this investigation are presented in table I.

Eleven buffet wings were used in the study which covered systematic variations of sweep, thickness-to-chord ratio, position of maximum thickness, camber, and aspect ratio. Each wing was constructed of a solid SAE 4130 steel panel, and particular care was taken to insure that the steel wings were rigidly attached to the steel portion of the fuselage to minimize structural damping. The buffet gages, which constituted a complete moment bridge of four active strain gages, were embedded beneath the upper and lower surface of one wing panel near the fuselage juncture on the 50-percent-chord line. (See fig. 1.) The recesses over the gages were filled in and faired to the contour of the wing surface. All wiring was routed internally through the model into the balance chamber.

Most of the wings were tested in combination with the fuselage having the rounded forebody. Several tests, however, were performed with a fuselage having a pointed forebody (see fig. 1) to determine whether the buffet-onset or buffet-intensity characteristics were affected by forebody bluntness.

#### MEASUREMENTS AND CORRECTIONS

## Measurement of Buffet Characteristics

The primary source of buffet information for this investigation was obtained by the wing-root bending-gage technique (ref. 3). The buffet gages consisted of four active

strain gages forming a complete bending-moment bridge. As shown in figure 1, the gages were located near the wing-fuselage juncture and oriented along the 50-percent-chord line of the wing. The gages located in this manner, that is, on or near the effective flexural and cantilever axes, respond readily to any fluctuating aerodynamic load disturbance on the wing panel due to flow separation.

Prior to the wind-on investigation of the buffet models, each wing was oscillated with a vibrator through a range of frequencies varying from about 0 to 600 Hz to determine the bending characteristics of the wings and to insure that the gages were sensitive to oscillations at the fundamental bending frequency. The equipment used in this static survey included an oscillator with associated electronic equipment, a hand-held vibration pickup, and an oscilloscope. The models were driven through the known frequency range, and the phase relationship and amplitude of the oscillator and vibrator pickup were monitored on the oscilloscope. Because the vibration probe could be held at various locations on the models, the fundamental bending frequencies could be identified, and the nodal patterns of the various buffet wings could be determined.

At the outset of this investigation, the onset of buffeting was determined by visually monitoring the wind-on root-mean-square outputs of the wing-bending gages on a simple root-mean-square voltmeter (test 768). This method for determining buffet onset appeared to be adequate in most cases; however, at the higher values of gage output it became difficult to ascertain a quantitative level of buffet intensity because of large fluctuations of the root-mean-square meter. This was particularly true in the high-subsonic Mach number range where the rise in buffet intensity appeared to become a more gradual process in contrast to the well-defined, abrupt onset of buffeting indicated at the lower Mach numbers.

In order to establish a higher degree of repeatability of the buffet responses, a root-mean-square meter which linearly converts alternating-current input into direct-current outputs (test 778) and a direct-current integrator were incorporated into the system. The final arrangement of the buffet instrumentation is shown in figure 2.

A brief study was conducted to determine a realistic integration time with respect to available test time and repeatability of the buffet results. The bending-gage outputs were monitored on strip charts for intervals ranging from 2 minutes to 30 seconds at several angles of attack and Mach numbers. It was determined that for a typical test wing at several different tunnel conditions, an acceptable degree of repeatability could be obtained by integrating the output of the bending gages for a period of about 45 seconds. Therefore, the buffet results presented herein (with the exception of the results for wing 4) represent the average root-mean-square values of the alternating currents emitted from the wing moment bridge during a 45-second sampling interval. (The buffet

results shown for wing 4 (test 768, see fig. 7(g)) were determined by the earlier method which relied on visual observation of the simple-root-mean-square meter.)

### Measurements of Static Aerodynamic Forces and Moments

The static aerodynamic forces and moments were measured by means of a six-component electrical strain-gage balance which was installed within the model. The static aerodynamic data were recorded simultaneously with the integrated root-mean-square output of the wing bending gages.

Transition strips of No. 150 carborundum grit were placed 0.50 inch (1.27 cm) behind the leading edges of the wings and 1.00 inch (2.54 cm) aft of the fuselage nose in the manner described in reference 4 to insure turbulent flow in the model boundary layer at Mach numbers above approximately 0.50. It should be emphasized here that several studies were made with transition at Mach numbers below 0.50, and therefore, the drag results at the low subsonic Mach numbers should be used with caution. Wings 8 and 9 were investigated with the transition strips completely removed to determine the effects of the artificial roughness on the buffet and static aerodynamic characteristics.

#### Corrections to Static Aerodynamic Results

The angles of attack shown herein have been corrected for the combined bending of the sting and balance system due to aerodynamic loading. Balance cavity pressures were monitored throughout the investigation by means of differential pressure gages and the axial-force and drag-coefficient data have been adjusted to correspond to a condition of free-stream static pressure at the base of the model. Jet boundary and blockage corrections were applied to the results as prescribed in references 5 and 6.

## TEST CONDITIONS

The investigation was conducted in the Langley high-speed 7- by 10-foot tunnel which is a continuous-flow facility having, for this study, a closed test section. The Mach numbers for the various tests performed are listed in the run schedule contained in table II. The variations of the average Reynolds number and dynamic pressure with Mach number are shown in figure 3. In general, the Mach number range of this investigation extended from a minimum of about 0.23 to a maximum of about 0.94. The models were tested at 0° of sideslip through an angle-of-attack range which was varied from about 0 to a maximum of about 22°. At the higher Mach numbers, the angle-of-attack range was reduced because of balance limitations.

#### RESULTS AND DISCUSSION

#### Presentation of Results

Table II presents a run schedule for the buffet and static aerodynamic results presented in table III. Results are tabulated for all the wings which have been investigated with the exception of the buffet results for wing 4. (The buffet data for wing 4, determined in a preliminary investigation, were recorded and computed manually and therefore are not included in table III.)

Plotted results have been included for wings 1 to 11. (The wings were tested with transition grit on and with the fuselage having the rounded forebody except where specifically noted.) The results are presented in the following figures:

T)	gui C
Static longitudinal aerodynamic and buffet characteristics:	
Wing 1 (A = 6; $\Lambda_{c/4} = 25^{\circ}$ ; airfoil section, NACA 63A008)	4
Wing 2 (A = 6; $\Lambda_{c/4} = 35^{\circ}$ ; airfoil section, NACA 63A008)	5
Wing 3 (A = 6; $\Lambda_{c/4} = 45^{\circ}$ ; airfoil section, NACA 63A008)	6
Wing 4 (A = 6; $\Lambda_{c/4} = 35^{\circ}$ ; airfoil section, NACA 63A006)	7
Wing 5 (A = 6; $\Lambda_{\rm C}/4$ = 35°; airfoil section, NACA 63A010)	8
Wing 6 (A = 6; $\Lambda_{c/4} = 35^{\circ}$ ; airfoil section, NACA 64A008)	9
Wing 7 (A = 6; $\Lambda_{\rm C}/4$ = 35°; airfoil section, NACA 65A008)	10
Wing 8 (A = 6; $\Lambda_{c/4} = 35^{\circ}$ ; airfoil section, NACA 63A208);	
transition grit off	11
Wing 8 (A = 6; $\Lambda_{\rm C}/4$ = 35°; airfoil section, NACA 63A208)	12
Wing 9 (A = 6; $\Lambda_{\rm C}/4$ = 35°; airfoil section, NACA 63A408);	
pointed forebody; transition grit off	13
Wing 9 (A = 6; $\Lambda_{\rm C}/4$ = 35°; airfoil section, NACA 63A408);	
transition grit off	14
Wing 9 (A = 6; $\Lambda_{\rm C}/4$ = 35°; airfoil section, NACA 63A408)	15
Wing 10 (A = 4; $\Lambda_c/4 = 35^\circ$ ; airfoil section, NACA 63A008)	16
Wing 11 (A = 5; $\Lambda_{c/4} = 35^{\circ}$ ; airfoil section, NACA 63A008)	17
•	
Comparison of longitudinal aerodynamic and buffet characteristics:	18
Effect of wing sweep	19
Effect of thickness-to-chord ratio	
Effect of position of maximum thickness	20
Effect of camber	21
Effect of aspect ratio	22
Effect of transition grit	23
Effect of forebody shape and transition grit	24

Timuno.

${f F}$	igure
Summaries of longitudinal aerodynamic and buffet characteristics:	
Effect of wing sweep	25(a)
Effect of thickness-to-chord ratio	
Effect of position of maximum thickness	25(c)
Effect of camber	
Effect of aspect ratio	25(e)

## Evaluation of Buffet-Onset Measurement Techniques

Self-induced wing buffet is associated with the wing response to random excitation resulting from pressure fluctuations in separated flow from the wing. Separated-flow conditions on wind-tunnel models can be determined by a variety of techniques which include static force and moment measurements, such as inflections in the lift-curve slope; divergences in trailing-edge pressure; observations of the flow in the boundary layer; fluctuating wake pressure studies; and wing-root bending-gage measurements. All these methods have been utilized in the past with varying degrees of success to determine the conditions at which buffet onset occurs.

Since buffeting is a dynamic phenomenon, the fluctuating-root bending-gage technique appeared at the outset to be one of the most direct and simple methods for determining buffet onset in that it readily provides an integration of the oscillations occurring on the entire wing panel. Past research (ref. 7) has indicated that the wing-root bendinggage technique can be a reasonably effective method for predicting flight buffet-onset boundaries from wind-tunnel results. Insofar as the development of a particular configuration for good high-lift characteristics is concerned, the information provided by the wing-root bending gage is certainly recognized as being inadequate to determine where separation occurs and needs to be supplemented by other information, such as extensive pressure-distribution information and possibly, boundary-layer flow observations. There are further shortcomings in regard to the interpretation of the bending-gage results under certain conditions where the buffet-onset lift coefficient approaches zero. Usually this phenomenon occurs at conditions where the Mach number is high and the thicknessinduced flow field is substantial (for instance, a wing with low sweep and high thicknessto-chord ratio). Under these conditions, self-induced buffeting may occur where separation exists on the wing at all lift coefficients. At the higher Mach numbers, which obviously are of particular interest in this type of study, this situation is complicated by a rise in the "noise," or wind-tunnel turbulence level. (Tunnel "noise" is manifested in the bending-gage results as an increase in output of the gage with Mach number which is insensitive to changes in model attitude.) Under conditions such as this, that is, low lift coefficient for buffet onset and substantially high levels of tunnel turbulence (for example, see the case for a Mach number of 0.883 in fig. 4(g)), the uncertainty exists as to whether

the wing-bending-gage output at the low lift coefficient is due to separation on the wing or due to the wind-tunnel turbulence. In cases such as this, where a well-defined "plateau," or base level, in the bending-gage results and a pronounced divergence are not established as the model attitude is increased, additional aid is required to interpret the results with any degree of certainty. In the present study, the buffet-onset characteristics of these more "complicated" cases were interpreted with the aid of the static-force data. Classically, erratic variations in the axial-force coefficient with angle of attack suggest separation on the wing of a wind-tunnel model. "Erratic" variations in this discussion are assumed to be departures of the experimental results from the theoretical variations of axial-force coefficient with angle of attack. (An indication of separation could also be obtained by evaluating the experimental axial-force variations with the square of the angle of attack. A linear variation of axial-force coefficient with the square of the angle of attack would suggest that the airflow is attached to the wing, and departures from this linear variation would indicate that the flow over the wing has separated.)

The basic results determined for the wing 1 configuration will be discussed to illustrate the process used in the determination of the buffet characteristics presented in this paper. In figure 4, the static longitudinal aerodynamic characteristics and wingbending-gage moment  $M_{\mathrm{WS}\mathrm{g}}$  exhibited by the wing 1 configuration are presented as functions of angle of attack  $\alpha$  or lift coefficient  $C_{1}$ . The solid symbols shown on each of the presentations represent the buffet-onset points which were determined, primarily, from the wing-bending-gage results. In reviewing the bending-gage results (fig. 4(g)), it will be noted that at the lower Mach numbers the rms signal of the wing bending-gage output  $M_{WSg}$  is essentially invariant with  $C_{I}$  until some well-defined break takes place. At the lower Mach numbers the condition at which the divergence occurs is obvious, and the determination of the buffet-onset points requires very little interpretation. As the Mach number is increased, the zero-lift level of the rms moment output is increasing before the buffeting occurs as a result of the increase in the tunnel turbulence level. At the highest Mach numbers, the results indicate a gradual rise in the bending-gage intensity prior to the abrupt rise. For example, in the Mach 0.88 case, the bending-gage output appears to have increased between a lift coefficient of about 0 to 0.15; however, there is a definite "break" in the curve at a lift coefficient of about 0.45. In this region of uncertainty  $C_{I} = 0.15$  to 0.45, the wing possibly experiences a low-intensity, or intermittent, buffeting. Interpretation of this particular case is difficult and the exact lift coefficient at which buffet onset occurs cannot be definitely established from this information alone. For this case, a better indication of the point of buffet onset can be obtained from the axial-force results presented in figure 4(b). The theoretical axial-force curves (indicated by the dashed lines) were developed from the equation

$$C_{A} = s \left[ C_{L_{\alpha}} - \left( C_{L_{\alpha}} \right)^{2} \frac{\partial C_{D,i}}{\partial C_{L}^{2}} \right] \sin^{2} \alpha + \left( C_{A} \right)_{\alpha=0}$$

which was derived from information contained in references 2 and 8 and the experimental axial-force coefficients at zero angle of attack  $(C_A)_{\alpha=0}$ . The  $C_{L_{\alpha}}$  and  ${}^{\partial}C_{D,i}/{}^{\partial}C_L^2$  terms were calculated by a modified Multhopp lifting-surface theory developed in reference 9.

It will be noted from the axial-force results (fig. 4(b)) for Mach numbers of 0.82 and below, that the point at which the experimental data depart from the theoretical variations is in good agreement with the buffet-onset points, which are obvious from the bending-gage results (fig. 4(g)). These data suggest the correspondence between the deviation in the axial-force variations and the onset of buffeting. A rational explanation exists if separation in the boundary layer is presumed to cause each of these phenomenon. Acceptance of this argument leads to a very convenient method of complementing the wingbending-gage results in analyzing buffet-onset characteristics.

Again, comparison of both the axial-force results (fig. 4(b)) and the bending-gage data (fig. 4(g)) shows that in the lower Mach number range there is a pronounced reversal of the experimental axial-force slopes which correlates with an abrupt divergence in the wing bending-gage output. At a Mach number of 0.88, where the interpretation of the bending-gage results becomes more difficult, the experimental axial-force results indicate a noticeable departure from the theoretical curves at an angle of attack of about  $1^{0}$ which corresponds to the slight variation in the wing-bending-gage results at a lift coefficient of about 0.05. These results lead to the conclusion that separation did exist at the lower attitudes and that the gradual rise evidenced in the bending-gage output resulted from a low-intensity excitation (buffeting) of the wing panel. It should be emphasized here that this 'conservative' approach has been taken in the analysis of all of the buffetonset characteristics shown herein. (Although not included in the data presentations, the preliminary investigation previously mentioned indicated that at a Mach number of about 0.94 the wing 1 configuration exhibited buffeting at all lift coefficients.) The pronounced increase in buffet intensity noted for the Mach 0.88 condition at a lift coefficient of 0.45  $(\alpha = 4^{\circ})$  corresponds to the attitude at which the slope reverses in the experimental axial-force variation. The significance of this apparent onset of low-intensity buffeting is not fully understood at this point, but it could be conjectured that in the high-subsonic transonic region where a transition from the classic subsonic separation to a shockinduced separation takes place, two different types of buffeting phenomena might occur at one Mach number. The low-intensity buffeting might possibly be indicative of the development of a shock-induced separation, whereas the pronounced increase in buffet

intensity could be associated with the type of subsonic separation and buffeting exhibited at the lower subsonic Mach numbers. Additional studies, possibly visual flow observations, might be of assistance in the understanding of these suspected low-intensity and high-intensity "boundaries."

Interpretation of the bending-gage results obtained at the higher subsonic Mach numbers is not always as difficult as the Mach 0.88 condition for wing 1 just discussed. As an illustration, the rms output of the wing gages in figure 8(g) for a Mach number of about 0.93 can readily be interpreted. The pronounced rise in the bending-gage output at low attitudes suggests that there is well-defined separation on the relatively thick wing 5 configuration and that the airfoil buffets at a very low lift coefficient, probably at a lift coefficient of zero.

Although the axial force appears to be a useful aid in determination of buffet-onset characteristics in selected cases of uncertainty, this paper does not intend to suggest that the wing bending gage is not useful, or required, in the analysis of buffet-onset characteristics. Erratic axial-force characteristics (i.e., departures of the experimental axial force from the theoretical trend) may be caused by the formation of a shock system which is of insufficient strength to separate the boundary layer; therefore, care must be taken when interpreting the axial-force variations. Self-induced buffeting, however, is not possible without separation.

All the static-force and moment characteristics were examined in conjunction with the bending-gage results to determine whether any additional correlations could be established. In general, for the uncambered series of wings, the break in the lift-curve slope, which is commonly used to predict buffet onset, appeared to indicate optimistic predictions, particularly in the low-subsonic Mach number range. However, for the cambered wings, which develop considerably higher buffet-free lift coefficients, a fair correlation appeared to exist between the breaks in the lift-curve and pitching-moment slopes and the wing-bending-gage divergences. (For example, see fig. 15.) The possibility of using the divergences in the rolling-moment curves as an indication of buffet onset was examined and the trends indicated were found to be inconsistent; therefore, a satisfactory correlation with the wing-bending-gage results could not be established. This approach was not expected to offer a dependable indication of buffet onset since the rolling-moment divergences at zero angle of sideslip would be dependent upon asymmetric separation characteristics.

#### Wing-Geometry Effects on Buffet Onset

The effects of the various wing parameters which were evaluated are illustrated at comparable Mach numbers in the comparison plots contained in figures 18 to 24. Figure 23 shows that the application of transition grit did not significantly affect the lift

coefficient for buffet onset of the wing 8 configuration. Sizable changes are evident, however, in the buffet intensity and static longitudinal characteristics for several Mach numbers. The bending-gage results shown in figure 24 at Mach numbers above 0.75 indicate that the addition of transition grit had a significant effect on the buffet-onset characteristics of the more highly cambered airfoil, wing 9. It is not conclusive from this brief study, but the effect of transition grit on buffet-onset characteristics appears to be dependent to some extent on the amount of camber in the airfoil sections. In addition, the contents of figure 24 indicate that the forebody-shape variations considered in this study did not significantly affect the buffet-onset characteristics of the wings. However, at the higher Mach numbers the results suggest that the shape of the forebody did affect the level of buffet intensity.

Summaries of the buffet characteristics and several static longitudinal parameters for the wings which were considered in this investigation are presented in figure 25. Several relationships evident in the variations of these parameters with Mach number are interesting when it is recalled that buffeting is a phenomenon which occurs in separated flow. There is a strong resemblance between the comparative buffet-onset trends and the variations of the maximum lift-drag ratios. At a given Mach number, the wing developing the highest maximum L/D and lift coefficient for maximum L/D generally displays the highest lift coefficient for buffet onset. It will be noted that, in general, when there is a divergence in the  $C_{\rm m_{CL}}$  trend, a reduction in  $C_{\rm L_Q}$ , a marked increase in  $(C_A)_{\rm max}$ , and large reductions in  $(L/D)_{\rm max}$ , the buffeting occurs at very low lift coefficient.

in  $(C_A)_{\alpha=0}$ , and large reductions in  $(L/D)_{max}$ , the buffeting occurs at very low lift coefficients. (For instance, see the results for airfoil section 63A010 in fig. 25(b).)

In summary, the buffet-onset characteristics determined in this investigation have indicated that for the wing variations which were considered, the lower sweep, high-aspect-ratio, moderately thick, cambered airfoils with rounded leading edges should display higher buffet-free lift coefficients at low subsonic Mach numbers. In the high-subsonic regime, the results suggest that within the range of variables studied, increase in sweepback and reductions in thickness ratio, aspect ratio, and camber should favorably affect buffet-onset characteristics.

## CONCLUDING REMARKS

A wind-tunnel investigation has been conducted in the Langley high-speed 7- by 10-foot tunnel to determine the buffet and static aerodynamic characteristics of a systematic wing series at Mach numbers ranging from 0.23 to 0.94. The results have indicated that for a given Mach number, the wings which display superior aerodynamic efficiency characteristics generally display the highest buffet-free lift coefficient. The

characteristics exhibited by the wings which were considered have indicated that correlations can be made between the onset of buffeting and selected divergences in the static aerodynamic characteristics. Axial force has been found to be the most sensitive static component to the onset of buffeting.

Langley Research Center,

National Aeronautics and Space Administration, Langley Station, Hampton, Va., February 16, 1970.

#### REFERENCES

- 1. Mechtly, E. A.: The International System of Units Physical Constants and Conversion Factors. NASA SP-7012, 1964.
- 2. Henderson, William P.: Studies of Various Factors Affecting Drag Due to Lift at Subsonic Speeds. NASA TN D-3584, 1966.
- 3. Davis, Don D., Jr.; and Huston, Wilber B.: The Use of Wind Tunnels To Predict Flight Buffet Loads. NACA RM L57D25, 1957.
- 4. Braslow, Albert L.; Hicks, Raymond M.; and Harris, Roy V., Jr.: Use of Grit-Type Boundary-Layer-Transition Trips on Wind-Tunnel Models. NASA TN D-3579, 1966.
- 5. Gillis, Clarence L.; Polhamus, Edward C.; and Gray, Joseph L., Jr.: Charts for Determining Jet-Boundary Corrections for Complete Models in the 7- by 10-Foot Closed Rectangular Wind Tunnels. NACA WR L-123, 1945. (Formerly NACA ARR L5G31.)
- 6. Herriot, John G.: Blockage Corrections for Three-Dimensional-Flow Closed-Throat Wind Tunnels, With Consideration of the Effects of Compressibility. NACA Rep. 995, 1950. (Supersedes NACA RM A7B28.)
- 7. Mabey, D. G.: Comparison of Seven Wing Buffet Boundaries Measured in Wind Tunnels and in Flight. C.P. No. 840, Brit. A.R.C., 1966.
- 8. Polhamus, Edward C.: A Concept of the Vortex Lift of Sharp-Edge Delta Wings Based on a Leading-Edge-Suction Analogy. NASA TN D-3767, 1966.
- 9. Lamar, John E.: A Modified Multhopp Approach for Predicting Lifting Pressures and Camber Shape for Composite Planforms in Subsonic Flow. NASA TN D-4427, 1968.

TABLE I.- MODEL CHARACTERISTICS

Fuselage dimensions: length, 48.80 in. (123.95 cm); maximum diameter, 4.90 in. (12.45 cm); base diameter, 3.08 in. (7.82 cm)

Wing	Airfoil section	$\Lambda_{\mathrm{c}/4},\deg$	c <sub>t</sub> , in. (cm)	c <sub>r</sub> , in. (cm)	c, in.	b, in. (cm)	$\left \begin{array}{c} s, \text{ ft}^2\\ \left(\text{m}^2\right) \end{array}\right $	A	FS from L.E. of c <sub>r</sub> , in. (cm)
1	NACA 63A008	25	3.43 (8.71)	8.57 (21.8)	6.38 (16.2)	36.00 (91.4)	1.50 (0.139)	6	19.27 (48.95)
2	NACA 63A008	35	3.43 (8.71)	8.57 (21.8)	6.38 (16.2)	36.00 (91.4)	1.50 (0.139)	6	18.87 (47.93)
3	NACA 63A008	45	3.43 (8.71)	8.57 (21.8)	6.38 (16.2)	36.00 (91.4)	1.50 (0.139)	6	18.34 (46.58)
4	NACA 63A006	35	3.43 (8.71)	8.57 (21.8)	6.38 (16.2)	36.00 (91.4)	1.50 (0.139)	6	18.87 (47.93)
5	NACA 63A010	35	3.43 (8.71)	8.57 (21.8)	6.38 (16.2)	36.00 (91.4)	1.50 (0.139)	6	18.87 (47.93)
6	NACA 64A008	35	3.43 (8.71)	8.57 (21.8)	6.38 (16.2)	36.00 (91.4)	1.50 (0.139)	6	18.87 (47.93)
7	NACA 65A008	35	3.43 (8.71)	8.57 (21.8)	6.38 (16.2)	36.00 (91.4)	1.50 (0.139)	6	18.87 (47.93)
8	NACA 63A208	35	3.43 (8.71)	8.57 (21.8)	6.38 (16.2)	36.00 (91.4)	1.50 (0.139)	6	18.87 (47.93)
9	NACA 63A408	35	3.43 (8.71)	8.57 (21.8)	6.38 (16.2)	36.00 (91.4)	1.50 (0.139)	6	18.87 (47.93)
10	NACA 63A008	35	4.20 (10.7)	10.50 (26.7)	7.80 (19.8)	29.39 (74.7)	1.50 (0.139)	4	18.80 (47.75)
11	NACA 63A008	35	3.76 (9.55)	9.39 (23.9)	6.98 (17.7)	32.86 (83.5)	1.50 (0.139)	5	18.84 (47.85)

TABLE II. - RUN SCHEDULE

Run	Wing	Nose	Mach number	Transition grit								
		Te	st 768									
23 24 25 26 27 28	4	Round	0.940 .870 .811 .758 .707 .503	On								
Test 778												
1 2 3 4 5	9	Round	0.933 .863 .808 .753 .702	Off								
6 7 8 9 10		Pointed	.498 .292 .933 .863 .807									
11 12 13 14 15	8	Round	.753 .702 .498 .292 .833	On								
16 17 18 19 20			.863 .807 .754 .702 .498									
21 22 23 24 25			.292 .807 .753 .702 .498	Off								
26 27 28 29 30	7		.293 .932 .863 .932 .863	On								
31 32 33 34 35			.807 .754 .702 .498 .292									
36 37 38 39 40	5     		.933 .864 .806 .754 .702									

TABLE II.- RUN SCHEDULE - Continued

Run	Wing	Nose	Mach number	Transition grit
		Test 778	B - Continued	
41 42 43 44 45	5 5 6	Round	0.493 .293 .933 .864 .806	On
46 47 48 49 50	10		.755 .702 .293 .497 .933	
51 52 53 54 55			.864 .807 .755 .703 .293	
56 57 58 59 60	11		.498 .932 .863 .807 .754	
61 62			.702 .293	
64 65	11 9	Round	.497 .883	On
66 67 68 69 70			.823 .770 .718 .666 .225	
71 72 73 74 75	1		.455 .883 .823 .770 .718	
76 77 78 79 80	3 		.665 .225 .456 .883 .821	
81 82 83 84 85		•	.769 .717 .665 .225 .455	

16

TABLE II.- RUN SCHEDULE - Concluded

Run	Wing	Nose	Mach number	Transition grit						
Test 778 - Concluded										
86 87 88 89 90 91 92	2	Round	0.883 .770 .717 .665 .822 .456 .225	On						

#### TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS

The symbols used in the tabulated data are defined as follows:

MACH Mach number

Q free-stream dynamic pressure,  $lb/ft^2$  (1  $lb/ft^2 = 47.88 N/m^2$ )

BETA angle of sideslip, deg

ALPHA angle of attack, deg

Body axis:

CNF normal-force coefficient

CAF axial-force coefficient

CLB rolling-moment coefficient

CNB yawing-moment coefficient

CSF side-force coefficient

CAB + CAC chamber axial-force coefficient

Stability axis:

CL lift coefficient

CD drag coefficient

CPM pitching-moment coefficient

CLS rolling-moment coefficient

CNS yawing-moment coefficient

L/D lift-to-drag ratio

CDB + CDC chamber drag coefficient

PB-1 integrated rms output (M<sub>WSg</sub> on plotted presentations) from wing

bending gage, in. lb (1 in. lb = 0.113 m-N)

## TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST=	768 RUN=	23								
							BODY PRESS.COEFF				
PUINT	MACH	Ų	BETA	ALPHA	LNF	CAF	CLR	CNB	CSF	CAB	· CAC
538	0.936	737.243	-0.01	-1.07	-0.1591	0.0162	-0.0011	0.0007	0.0002	0.0031	0.0031
_539	0.939	739.626	-0.01	0.12	-0.0203	0.0174	-0.0006	0.0006	0.0004	0.0031	0.0031
540	0.940	740.409	-0.00	1.40	0.1237	0.0167	-0.300C	0.3005	-0.0006	0.0031	0.0031
541	0.939	740.015	-0.01	2.58	0.2595	0.0143	-0.3003	0.0905	0.0004	0.0031	0.0031
542	0.939	739.685	-0.61	3.82	0.3906	0.0115	-0.0004	0.0005	0.0003	0.0031	0.0031
543	0.940	740.258	-0.01	5.00	6.5100	0.0099	-0.0009	0.0005	0.0006	0.0031	0.0030
544	0.940	740.261	-0.01	6.22	3.6173	0.0085	-0.0C1C	0.0005	0.0003	0.0030	0.0030
545	0.943	742.844	-0.01	7.41	0.7169_	0.0087	0.0005	0.0004_	0.0007	0.0030	0.0030
546	0.941	741.527	-0.01	8.50	U.7051	0.0076	0.0025	0.0005	0.0046	0.0030	0.0029
547	0.937	738.187	-0.01	C.08	-0.0244	0.6170	-0.0001	0.0006	-0.0001	0.0031	0.0031
553	0.943	742.632	-0.01	0.12	-6.0226	0.0176	-0.0008	0.0007	0.0005	0.0032	0.0031
554	0.938	738.403	-0.00	-1.10	-J.1561	0.0161	-0.0006	0.0006	-0.0012	0.0031	0.0031
555	0.937	737.594	-0.01	6.07	-v.0285	0.0174	-0.0004	0.0006	0.0002	0.0031	0.0031

	TEST=	768 RUN=	23									
					STA	ABILITY AXIS	COEFFICIENT		STAB.PRESS.COEFF			
POINT	MACH	ų	BETA	ALPHA	CL	LU	CPM	CLS	CNS	L/D	CDB	CDC
538	0.936	737.243	-0.01	-1.07	-3.1588	0.0191	0.0139	-0.0011	0.0007	-8.306	0.0031	0.0031
539	0.939	739.626	-0.01	0.12	-5.3263	0.0174	0.0083	-0.0006	0.0006	-1.515	0.0031	0.0031
540	0.940	740.409	-0.00	1.40	0.1233	0.0197	0.0003	0.0000	0.0005	6.244	0.0031	0.0031
541	0.939	740.015	-0.01	2.58	<b>6.2586</b>	J.0260	-3.3143	-0.0003	0.0005	9.963	0.0031	0.0031
_542_	0.939	739.685	-0.01	3.82	0.3889	0.0374	-0.0312	-0.0003	0.0005	10.390	0.0031	0.0031
543	0.940	740.258	-0.01	5.00	0.5072	0.0543	-3.0454	-0.0008	0.0005	9.338	0.0030	0.0033
544	0.940	740.261	-0.01	6.22	J.0127	0.0753	-C.J480	-0.0010	0.0006	8.136	0.0030	0.0030
_545	0.943	742.844	-0.C1	7.41	J.7098	0.1011	-0.0567	0.0005	0.0004	7.019	0.0030	0.0030
546	0.941	741.527	-0.01	8.56	3.7752	0.1244	-0.0286	0.0026	0.0002	6.231	0.0029	0.0029
547	0.937	738.187	-0.01	0.08	-0.0244	0.0170	0.0074	-0.0001	0.0006	-1.436	0.0031	0.0031
553	_0.943	742.632	-0.01	0.12	-3.0226	0.0175	0.0381	-0.0038	0.0007	-1.290	0.0032	0.0031
554	0.938	738.403	-6.00	-1.10	-0.1558	0.3191	0.0147	-0.0006	0.0006	-8.170	0.0031	0.0031
555	0.937	737.594	-6.01	0.07	-0.3286	0.0174	0.0087	-0.0004	0.0006	-1.641	0.0031	0.0031

## TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST=	768 RUN=	24									
						BUDY AX	IS COEFFICIE!	NTS		BODY PRESS-CUEFF		
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLR	CNB	CSF	CAB	CAC	
556	0.868	682.237	-0.00	-1.10	-0.1338	0.0143	-0.0006	0.0006	-0.0011	0.0027	0.0026	
557	0.867	681.598	-0.01	0.04	-0.0256	0.0162	-0.3002	0.0006	0.0000	0.0027	0.0026	
558	0.867	681.609	-0.00	1.22	0.0859	0.0152	-0.0002	0.0006	-0.0005	0.0027	0.0026	
559	0.870	683.969	-0.00	2.42	0.2073	0.0108	-0.0003	0.006	-0.0000	0.0027	0,0027	
560	0.869	683.617	-0.01	3.67	0.3367	0.0040	-0.0003	0.0006	0.0004	0.0026	0.0027	
561	0.868	681.985	-0.01	4.88	0.4735	-0.0024	C.0000	0.0066	0.0007	0.0026	0.0026	
562	0.869	683.473	-0.01	6.13	0.6102	-0.0051	0.0008	0.0007	0.0007	0.0026	0.0026	
563	0.869	683.367	0.00	7.29	0.6558	0.0013	-0.0057	0.0003	0.0011	0.0026	0.0026	
564	0.871	685.057	0.00	8.44	0.7129	0.0053	-0.3054	-0.0003	0.0012	0.0025	0.0025	
565	0.870	683.813	-0.00	9.53	0.7367	0.0082	-0.0017	0.0001	0.0012	0.0025	0.0025	
56.0	0.871	684.883	-0.00	10.58	_0.7569	0.0119	-0.0004	0.0003	0.0005	0.0025	0.0025	
567	0.872	685.419	-0.00	11.71	0.7872	0.0141	-0.0000	0.0003	0.0008	0.0025	0.0024	
568	0.873	686.564	-0.00	12.78	0.8293	0.0156	-0.0005	0.0064	0.0008	0.0024	0.0024	
569	0.873	686.544	-0.01	13.91	0.8650	0.0156	-0.0002	0.0004	0.0012	0.0024	0.0024	
570	0.869	682.879	-0.00	16.17	0.9581	0.0160	0.0002	0.0004	0.0010	0.0022	0.0023	
571	0.876	688 - 805	-0.00	18.28	1.0295	0.0151	0.0003	0.0005	0.0003	0.0021	0.0020	
572	C.877	690.100	-0.00	19.35	1.0796	0.0146	0.0003 _	0.0005	0.0001	0.0019	0.0019	

	TEST=	768 RUN=	24			• •	-					-	
					STA	BILITY AXIS	COEFFICIENTS	i		STAB.PRESS.COEFF			
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	CDC	
556	0.868	682.237	-0.00	-1.10	-0.1335	0.0168	0.0034	-0.0006	0.0006	-7.935	0.0027	0.0026	
_557_	0.867	681.598	-0.01	0.04	-0.0256	0.0162	0.0069	-0.0002	0.0006_	-1.579	0.0027	0.0025	
558	0.867	681.609	-C.00	1.22	0.0855	0.0171	0.0096	-0.0002	0.0007	5.014	0.0027	0.0026	
559	0.870	683.969	-0.00	2.42	0.2067	0.0196	0.0121	-0.0002	0.0006	10.563	0.0027	0.0027	
560	0.869	683.617	-0.01	3.67	0.3357	0.0250	0.0138	-0.0003	0.0006	13.128	0.0026	0.0026	
561	0.868	681.985	-0.01	4.88	0.4719	0.0379	3.0076	0.0001	0.0006	12.454	0.0026	0.0026	
562	0.869	683.473	-0.01	6.13	0.6072	0.0601	-0.0014	0.0039	0.0006	10.104	0.0026	0.0026	
563	0.869	683.367	0.00	7.29	0.0504	0.0845	0.0371	-0.0057	0.0004	7.696	0.0026	0.0025	
564	0.871	685.057	0.00	8.44	0.7044	0.1098	0.0551	-0.0054	0.0005	6.416	0.0025	0.0025	
565	0.870	683.813	-0.00	9.53	0.7252	0.1301	0.0808	-0.0017	0.0004	5.573	0.0025	0.0025	
_566	0.871	684.883	-0.00	10.58	0.7419	0.1506	0.0963	-0.0003	0.0004	4.926	0.0025	0.0024	
567	0.872	685.419	-0.00	11.71	0.7680	0.1736	0.1070	0.0000	0.0003	4.425	0.0024	0.0024	
568	0.873	686.564	-0.00	12.78	少•8053	0.1986	0.1152	-0.0004	0.0005	4.055	0.0024	0.0023	
569	0.873	686.544	-0.01	13.91	0.8358	0.2232	0.1271	-0.0001	0.0004	3.745	0.0023	0.0023	
570	0.869	682.879	-0.00	16.17	0.9158	0.2821	0.1437	0.0003	0.0003	3.246	0.0021	0.0022	
571	0.876	688.805	-0.00	18.28	0.9729	0.3372	0.1463	0.0005	0.0004	2.885	0.0020	0.0019	
_572_	0.877	690.100	-0.00	19.35	1.5138	0.3715	0.1469	0.0004	0.0003	2.729	0.0018	0.0018	

## TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST=	768 RUN=	25								
	1631-	700 1011				BUDY AX	S CUEFFICIE	NTS		BODY PRESS.C	0EFF
POINT	MACH	0	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
573	0.812	632.386	-0.01	-1.07	-0.1249	0.0139	-0.0007	0.0006	0.0011	0.0024	0.0024
574	0.810		-0.01	0.05	-0.0198	C.0160	0.0005	0.0006	0.0003	0.0024	0.0024
575	0.811	631.332	-0.01	1.21	0.0800	0.0150	-0.0004	0.0006	0.0008	0.0024	0.0024
576	0.810	630.841	-0.01	2.37	0.1901	0.0109	0.0001	0.0006	0.0009	0.0024	0.0024
577	0.810	630.937	-0.01	3.53	0.2926	0.0047_	0.0002	0.0006	0.0013	0.0024	0.0024
578	0.811	631.151	-0.0C	4.70	0.4050	-0.0026	0.0002	0.0005	0.0007	0.0024	0.0024
579	0.810	630.237	-0.01	5 • 96	0.5225	-0.0087	C.3003	0.0007	0.0011	0.0024	0.0023
580	0.811	631.411	-0.00	7.16	<u> </u>	<u>-c.0070</u>	0.0004_	0.0002	0.0020	0.0023	0.0023
581	0.811	631.726	-0.00	8.26	0.6657	-0.0611	-0.0012	0.0001	0.0017	0.0023	0.0023
582	0.812	631.975	-0.0C	9.37	0.7012	0.0050	-û.0004	0.0002	0.0014	0.0023	0.0023
583	0.811	631.566	-0.00	10.46	0.7297	0.0087	0.0001	0.0003	0.0015_	0.0023	0.0022
584	0.814	633.761	-0.00	11.58	0.7744	0.0118	0.0002	0.3004	0.0007	0.0023	0.0022
585	0.813	633.008	-0.00	12.67	0.8066	0.0132	0.3302	0.0003	0.0013	0.0022	0.0022
586	0.813	633.661	-0.00	13.78	0.8317	0.0145	-0.0001	0.0004	0.0012	0.0022	0.0022
587	0.815	634.699	-0.01	15.99	0.9022	0.0154	0.3000	0.0004	0.0015	0.3621	0.0021
588	0.815	634.905	-0.01	18.08	0.9722	0.0151	0.0001	0.0005	0.0010	0.0019	0.0019
589	0.815	634.901	-0.00	20.19	1.Ú571	0.0147	_ C.0004 .	0.0007	-0.0010	0.0016	0.0017
590	0.819	638.564	-0.00	22.24	1.1421	0.0128	0.3004	0.3064	-0.0004	0.0012	0.0012
591	0.820	639.864	-0.00	23.24	1.1767	0.0116	-0.0002	0.0006	-0.0035	0.0009	0.0009
592	0.812	631.631	-0.00	0.08	-0.0239	0.0159	0.000	0.0207	0.0001	0.0024	0.0024
593	0.810	630.215	-0.01	0.09	-0.0216	0.0160	-0.0005	0.0006	0.0003	0.0024	0.0024

	TEST=	768' RUN=	25									
					514	ABILITY AXIS	COEFFICIENTS	5		STA	B.PRESS.COEFF	
POINT	MACH	Q_	BETA	ALPHA	LL	CD	CPM	CLS	CNS	L/D	CDB	CDC
573	0.812	632.386	-0.01	-1.07	-0.1246	0.0163	0.0019	-0.0007	0.0006	-7.655	0.0024	0.0024
574	0.810	630.827	-0.01	0.05	-J.ú198	0.0159	0.0070	-0.0005	0.0006	-1.242	0.0024	0.0024
575	0.811	631.332	-0.01	1.21	0.0796	0.0167	0.0115	-0.0004	0.0006	4.769	0.0024	0.0024
576	0.810	630.841	-0.01	2.37	0.1895	0.0188	0.0152	0.0001	0.0006	10.105	0.0024	0.0024
577	0.810	630.937	-0.01	3.53	0.2918	J.0227	C.U194	0.0003	0.0006	12.843	C.0024	0.0024
578	0.811	631.151	-0.00	4.70	0.4039	0.0306	0.0240	0.0003	0.0004	13.190	0.0024	0.0024
579	0.810	630.237	-0.01	5.96	J.5205	0.0456	0.0278	0.0004	0.0006	11.415	0.0024	0.0023
580	0.811	631.411	-0.00	7.16	0.6102	0.0696	0.0460	-0.0004	0.0002	8.773	C.0023	0.0023
581	0.811	631.726	-0.00	8.26	J.6589	0.0946	0.0741	-0.0012	C.0003	6.968	0.0023	0.0023
582	0.812	631.975	-0.00	9.37	0.6911	0.1191	C.3964	-0.0004	0.0003	5.803	0.0023	0.0023
583	0.811	631.566	-0.00	10.46	J.7160	0.1410	0.1121	C.0001	0.0003	5.079	C.0022	0.0022
584	0.814	633.761	-0.00	11.58	0.7563	0.1670	0.1281	0.0002	0.0004	4.528	0.0022	0.0022
585	0.813	633.008	-0.00	12.67	J.7841	0.1898	0.1429	0.0003	0.0003	4.131	0.0022	0.0022
586	0.813	633.661	-0.00	13.78	0.8043	0.2122	0.1515	-0.0000	0.0004	3.790	0.0021	0.0021
587	0.815	634.699	-0.01	15.99	J.8631	0.2634	0.1645	0.0002	0.0004	3.276	0.0020	0.0020
588	0.815	634.905	-0.01	18.08	0.9195	0.3162	0.1708	0.0002	0.0004	2.908	0.0018	0.0018
589	0.815	634.901	-0.00	20.19	J.9871	ٕ3786	0.1734	0.0007	0.0005	2.607	0.0015	0.0016
590	0.819	638.564	-0.00	22.24	1.0523	0.4440	0.1823	0.0005	0.0003	2.370	0.0011	0.0011
591	0.820	639.864	-0.00	23.24	1.0712	0.4725	C.1873	0.0001	0.0007	2.267	0.0009	0.0008
592	0.812	631.631	-0.00	0.08	-0.0239	0.0159	0.0072	0.0000	0.0007	-1.504	0.0024	0.0024
593	0.810	630.215	-0.01	0.09	-U.0216	0.0159	0.0068	-0.0205	0.0006	-1.357	0.0024	0.0024

## TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST=	768 RUN=	26									
					STA	RILITY AXIS	CUEFFICIENTS	S		STA	B.PRESS.COEFF	
POINT	MACH	Q	BETA	ALPHA	CL	CU	CPM	CLS	CNS	L/D	CDB	CDC
594	0.758	580.514	-0.01	-1.06	-0.1218	0.0165	0.0007	-0.0004	0.0007	-7.393	0.0023	0.0023
595	0.757	579.478	-0.01	0.05	-0.0234	0.0161	0.0067	-0.0004	0.0007	-1.451	0.0023	0.0023
596	0.759	582.091	-0.01	1.19	0.0751	0.0169	0.0127	-0.0001	0.0006	4.440	0.0023	0.0023
597	0.758	580.612	-0.00	2.33	0.1729	0.0187	0.0165	-0.0001	0.0006	9.258	0.0023	0.0023
598	0.760	582.345	-0.00	3.48	3.2764	0.0223	0.0223	-0.0001	0.0005	12.377	0.0023	0.0023
599	0.756	579.343	-0.00	4.65	0.3718	0.0292	0.0279	0.0001	0.0005	12.723	0.0023	0.0023
600	0.758	580.395	-0.09	5.80	0.4728	0.0460	0.0350	0.0000	0.0002	10.283	0.0023	0.0022
601	0.757	580.212	-0.00	6.97	0.5475	0.0689	0.0571	-0.0001	0.0002	_7.947_	0.0022	0.0022
602	0.758	580.561	-0.00	8.14	0.6025	0.0917	0.0814	-0.0003	0.0003	6.568	0.0022	0.0022
603	0.758	580.815	-0.00	9.23	0.6528	0.1134	0.1030	0.0000	0.0003	5.757	0.0022	0.0022
604	0.760	582.581	-0.00	10.35	0.6938	0.1359	C.1214	0.0000	0.0003	5.106	0.0022	0.0021
605	0.763	585.415	-0.00	11.49	0.7268	0.1590	0.1360	0.0000	0.0003	4.570	0.0021	0.0021
606	0.759	582.124	-0.00	12.55	0.7686	0.1840	6.1507	0.0002	0.0001	4.176	0.0021	0.0021
607	0.761	584.002	-0.00	13.71	0.7913	0.2070	0.1607	0.0001	0.0002	3.822	0.0020	0.0020
614	0.759	581.454	-0.01	0.09	-0.0208	0.0160	7700.0	-0.0010	0.0006	-1.299	0.0023	0.0023
615	0.759	582.039	-0.00	15.87	0.8473	0.2563	0.1762	-0.0031	0.0004	3.307	0.0020	0.0020
616	0.762	584.247	-0.00	17.94	0.8995	0.3069	0.1837	0.0000	0.0006	2.931_	0.0018	0.0018
617	0.765	586.855	-0.00	20.01	0.9509	0.3624	C.1867	0.0011	0.0000	2.624	0.0015	0.0014
618	0.762	584.399	-0.00	22.01	1.0006	0.4188	0.1896	0.0006	-0.0005	2.389	0.0011	0.0011
619	0.764	586.168	0.00	23.98	1.0663	0.4860	0.2060	-0.0001	0.0005	2.194	0.0007	0.0007
620	0.758	579.860	-0.0C	0.09	-J.0224	0.0161	0.0068	-0.0005	0.0006	-1.393	0.0023	0.0023

	TEST=	768 RUN=	26								
	_					RNDA VX I	S CUEFFICIE	NTS		BODY PRESS.C	UEFF
POINT	MACH	Q	BETA	ALPHA	CNF	LAF	CLR	CNB	CSF	CAB	CAC
594	0.758	580.514	-0.01	-1.06	-0.1221	0.0142	-0.0004	0.0007	0.0008	0.0023	0.0023
595	0.757	579,478	-0.01	0.05	0.0233	0.0161	-0.0004	0.0007	0.0002	0.0023	0.0023
596	0.759	582.091	-0.01	1.19	0.6754	0.0153	-0.0001	0.0006	0.0006	0.0023	0.0023
597	0.758	580.612	-0.00	2.33	0.1735	0.0116	-0.0001	0.0006	0.0001	0.0023	0.0023
_598	_0.760	582.345	-0.00	3.48	0.2772	0.0055		0.0005	0.0007	0,0023	0.0023
599	0.756	579.343	-0.00	4.65	0.3729	-0.0010	0.0001	0.0005	0.0012	0.0023	0.0023
600	0.758	580.395	-0.00	5.80	0.4751	-0.0020	0.0000	0.0002	0.0005	0.0023	0.0022
601	0.757	580,212		6.97	0,5518	0.0020	0.0001	0.0002	0.0009	0.0023	0.0022
602	0.758	580.561	-0.00	8.14	J.6094	0.0055	-0.0003	0.0003	0.0015	0.0022	0.0022
603	0.758	580.815	-0.00	9.23	0.6025	0.0072	-0.0000	0.0003	0.0016	0.0022	0.0022
604_	0.760	582.581	-0.00	10.35	0.7069	0.0090	0.0000	0_00003	0.0009	0.0022	0.0022
605	0.763	585.415	-0.00	11.49	0.7440	0.0111	-0.0000	0.0003	0.0003	0.0021	0.0021
606	0.759	582.124	-0.00	12.55	0.7902	0.0126	0.0002	0.0002	0.0007	0.0021	0.0021
607	0.761_	_584.002	-0.00	13.71	0.8178	0.0136	c•0000	0.0002	0.0005	0.0021	0.0021
614	0.759	581.454	-0.61	0.09	-0.0208	0.0161	-0.0010	0.0006	0.0007	0.0023	0.0023
615	0.759	582.039	-0.00	15.87	0.8851	0.0149	-0.0002	0.0003	0.0012	0.0321	0.0021
016	0.762	584.247	-0.00	17.94	0.9503	0.0149	0.000 <u>1</u>	_0.0006	-0.0006	0.0019	0.0019
617	0.765	586.855	-0.00	20.01	1.0175	0.0151	0.0010	0.0004	0.0005	0.0016	0.0015
618	0.762	584.399	-0.60	22.01	1.0846	0.0133	0.0007	-0.0003	0.0027	0.0012	0.0012
619	_0.764		0.00	23 <u>.</u> 98_	1.1718	0.0108	0.0003	0.0004	0.0033	0.0008	0.0008
620	. 0.758	579.860	-0.00	0.09	-0.0223	0.0161	-0.0005	0.0006	0.0003	0.0023	0.0023

## TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST=	768 RUN=	27								
	_					BUUY AK.	IS CUEFFICIEN	T5		PODA byE22.	CUEFF
TAIDS	MALH	Ų	BETA	ALPHA	LNE	LAF	LLS	LINS	C2F	CAb	CAC
621	0.706	527.974	-0.61	-1.03	-0.1142	U.J145	-0.0068	0.6.67	O.C∩11	0.0122	0.0022
622	0.700	528.663	-0.00	0.09	-J.u213	0.0162	_0.0005 .	C.0006	0.0003	0.0522	0.0022
623	0.706	527.823	-0.00	1.17	0.0710	0.0150	-5.0003	0.0005	-0.0005	0.3022	0.0022
624	0.707	528.837	-0.00	2.30	6.1006	C.u121	-0.5002	0.0005	0.0002	0.3022	0.0022
625	0.707	529.395	-6.06	3.40	0.2015	C.0065	-5.0003	0.5065	0.0011	€.0022	0.0022
626	0.706	527.953	-0.00	4.58	J.30lo	0.0001	J.9053	0.0004	0.0014	0.0022	C.0022
627	0.706	528.541	-0.00	5.76	L.4544	-0.6315	-0.0002	0.0001	0.0011	0.0022	0.0022
628	0.700	528.284	-0.00	6.37	6.5319	0.0032	01?12 <u>_</u>	0.0003	J. D∈11	0.0022	0.0021
629	0.707	529.590	-0.00	8.06	J.0014	0.0055	-0.3029	0.0003	0.0005	J.J.22	0.0021
630	0.707	529.269	-0.00	10.23	c.0963	0.Ji81	0.0000	€.3003	0.0003	0.3321	0.0021
631	0.706	528.239	-0.00	11.37	J.7333	0.0099	0.0000	0.0002	0.3010	0.0021	0.0021
632	0.708	529.732	-0.60	13.59	0.8083	0.0127	-0.0001	0.0002	0.0000	0.0025	0.0020
633	0.709	531.009	-0.00	15.79	J. 8772	U.J141	-0.0002	<b>∂.</b> ⊌?⊌2	-0.3007	0.0020	0.0020
634	0.709	530.953	-0.00	17.81	0.4014	0.0144	-0.0001	0.0003	0.0000	0.0019	0.0019
635	0.709	531.392	-0.00	19.83	0.9059	5.0158	0.0005	0.0003	J.C009	0.0015	0.0016
636	0.711	533.287	-0.00	21.82	1.0510	C.J139	0.0002	0.0005	J.0005	0.0012	C.0012
637	0.710	531.553	-0.00	23.80	1.1661	0.0113	-6.0662	0.6067	-0.0016	0.0008	0.0007
638	0.700	527.853	-0.00	0.09	-0.0231	0.0163	-0.0002	0.0005	0.0001	0.0022	C.0022

	TEST=	768 RUN=	.27									
			*		5 <u>[ A</u>	OILITY AXIS	LUETFILLENIS			STAB	•PKLSS•CUEFF	
PUINT	MALH	u	BETA	ALPHA	UL TO THE	ری	CPM	CLS	CNS	L/u	CDB	CDC
621	0.706	527.974	-0.01	-1.03	-0.1139	0.3165	6.5567	-3.0008	0.0007	-0.895	J.0022	0.0022
622	0.706	528.003	-0.00	0.09	-3.5214	0.0102	0.0079	-0.00.05	0.0006	-1.321	0.0022	0.0022
623	0.706	527.823	-0.00	1.17	J.J712	€.0170	0.0127	-0.0003	0.0005	4.162	0.0022	0.0022
624	0.707	528.837	-0.00	2.30	0.1054	0.0168	C.0185	-0.30:2	0.3635	8.801	0.0022	0.0022
625	0.707	529.395	-0.00	3.40	0.2004	0.0222	0.0236	-6.0000	0.0005	11.719	0.0022	0.0022
626	0.706	527.953	-0.0C	4.58	ا ۵۵ و د ر	J.0202	J.0305	0.0€03	0.0004	12.417	0.0022	0.0022
627	0.706	528.541	-0.00	5.76	0.4023	J.0441	3.0360	-0.0002	0.6301	10.266	0.0022	0.0022
628	0.706	528 - 284	-0.00	b. 87	0.5277	J.J068	J.3568	-3.3011	3.3304	7.902	3.0022	0.0021
629	0.707	529.590	-0.GC	შ•მხ	J.6037	0.0906	0.0747	-6.3028	0.0007	0.634	5.0021	0.0021
630	0.707	529.269	-0.00	10.23	3.0779	3.1307	t.1231	0.0301	0.0003	5.188	0.0021	0.0023
631	0.706	528.239	-0.00	11.37	J.7170	J.15+2	0.1390	0.3001	0.0002	4.649	0.0020	0.0020
632	0.708	529.732	-0.00	13.59	7327	J.2022	0.1652	-0.3000	″ ∂.∂(∂2	3.870	0.0020	0.0020
633	0.709	531.009	-0.00	15.79	0.8403	0.2522	0.1030	-0.0001	0.0003	3.332	0.0019	0.0019
	0.709	530.953		17.81	0.0105	3.3005	0.1918	3.0000	0.0003	2.957	0.0016	0.0018
634		531.392	-0.00	19.83	5.9221	- دو4وء	0.1827	0.0005	- 0.0001	2.640	2.0015	0.0015
635	0.709	533.287	-0.00	21.82	0.9705	0.4036	0.1902	3.0034	0.0004	2.405	0.0311	0.0011
636	0.711		-0.00	23.80	1.0075	0.4506	3.2018	6.6071	0.0007	2.206	0.0007	0.0006
637	0.710	531.553 527.853	-0.00	0.49	-0.0231	0.0103	3.0361	-0.0002	0.0005	-1.420	0.0022	0.3022
630	0.706											

# TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST=	768 RUN=	28								
						ZUUDY AXI	S CUEFFICIE	NTS		BUDY PRESS.C	OEFF
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CINB	CSF	CAB	CAC
639	0.503	314.968	-0.00	-0.93	-0.0991	0.0160	-0.3036	0.0304	0.0009	0.0020	0.0020
640		314.351	0OC	0.10	-0.0189	0.0174	_0.0006	0.0003	0.0004	0.0020	0.0020
641	0.502	313.646	-0.00	1.13	0.0638	0.0168	-0.0003	0.0002	-0.0005	0.0020	0.0020
642	0.502	313.298	-0.00	2.20	0.1445	0.0139	-0.0003	0.0003	-0.0310	0.0020	0.0020
_643	0.502	. 313.744	0.00	3.34	0.2326	0.0091	0.2003	C.0002	-0.0021	0.0020	0.0020
644	0.502	313.751	-0.00	4.37	0.3054	0.0032	-0.0003	-0.0000	0.0002	0.0020	0.0020
645	0.502	313.698	0.00	5.44	0.3916	0.0003	-0.0000	-0.0001	-0.0007	0.0020	0.0020
- 646	0. 502	313.772	0.00	6.59	0.4846	<u>0.</u> 0318	0.3002	0.6302	-0.0016	0.3019	0.0019
647	0.502	313.848	-0.00	7.65	0.5521	0.0038	0.0005	0.0001	-0.0003	0.0019	0.0019
648	0.502	313.309	0.00	8.78	0.6094	0.0044	0.0004	0.0001	-0.0011	0.3619	0.0019
649	0.502	_313.300	0.0C	9.83	0.0016	0.0050	-C.3002	-0.0000	-0.0014	0.0019	0.0019
650	0.502	313.397	0.00	10.96	0.7213	0.0054	-0.0030	0.0001	-0.0019	0.0018	0.0019
651	0.502	314.115	0.00	12.00	3.7730	0.0064	-0.0049	-0.0001	-0.0031	C.C018	0.0018
652	0.502	313.607	0.00	13.15	0.8210	0.0075	-0.3055	0,0001		0.3017	0.0017
653	0.502	313.808	0.00	15.30	U.8704	U.C103	-0.5061	-0.0002	-0.0032	0.3017	0.0017
654	0.504	316.050	. 0.00	17.30	0.9263	0.0120	-0.3004	0.0001	-0.0029	0.0016	
655	0.503	315.039	0.00	19.31	0.9834	0.0143	-0.0364	0.0001	-0.0029	0.3015	0.0016
656	0.503	314.624	0.00	21.26	1.0164	0.0154	0.0000	0.0003	-0.0034		0.0015
657	0.502	313.304	-0.00	23.15	1.0495	0.0130	-0.0000	0.0007	-0.0035	0.0012	0.0012
658	0.502		0.00	0.14	-0.0185	0.3179	-0.0004	0.0007		0.0008	0.0008
					J. 0103		-0.0004	Ç•Ç30Z	0.0021	0.0050	0.0020

	TEST =	768 RUN=	28									
•					214	ABILITY AXIS	CUEFFIC LENTS	S		STA	B.PRESS.COEFF	
POINT	MACH	Q	BETA	ALPHA	(L	CO	CPM	LLS	CNS	L/D	CDR	CDC
639	0.503	314.968	-0.00	-0.93	-0.0988	0.0176	-0.0005	-0.0006	0.0004	-5.699	0.0020	0.0020
_640_	0.503	314.351	-c.oo	0.10	-0.0189	0.0174	0.0385	-0.0006	0.0003	-1.C90	0.0020	0.0023
641	0.502	313.646	-0.00	1.13	0.0634	0.0180	0.0150	-0.0003	0.0002	3.516	0.0020	0.0020
642	0.502	313.298	-0.00	2.20	0.1439	J.0195	0.0201	-0.0003	0.0003	7.390	0.0020	0.0020
643_	0.502	313.744	0.00	3.34	J.2316	0.0227	3.0272	0.0003	0.0002	10.225	0.0020	0.0020
644	0.502	313.751	-0.00	4.37	J.3043	0.0264	0.0340	-0.0003	0.0000	11.524	0.0020	0.0020
645	0.502	313.698	0.00	5.44	J.3898	0.0374	0.0430	-0.0000	-0.3001	10.428	0.0020	0.0020
646	0.502	313.772	0.00	6.59	0.4812	0.0574	0.0526	C.0003	0.0002	8.384	3.0019	0.0019
.647	0.502	313.848	-0.00	7.65	0.5467	0.0773	0.0694	0.0005	0.0000	7.075	0.0019	0.0019
648	0.502	313.309	0.00	8.78	3.6316	J.0974	0.0917	0.86.4	0.0000	0.175	0.0019	0.0018
649	0.502	313.300	0.00	9.83	0.0511	0.1179	0.1160	-0.0002	0.0000	5.521	0.0018	0.0018
650	0.502	313.397	0.00	10.96	0.7071	0.1424	C.1293	-0.0029	0.0006	4.965	0.0018	0.0018
651	0.502	314.115	0.00	12.00	6.7548	0.1670	0.1429	-0.0048	0.0010	4.520	0.0017	0.0017
652	0.502	313.607	0.00	13.15	J.7978	0.1942	0.1016	-0.0054	0.0014	4.109	0.0017	0.0017
653	0.502	313.808	0.00	15.30	0.8308	0.2396	0.1974	-6.0002	-C.JOO1	3.493	0.0016	0.0016
654	0.504	316.050	0.00	17.30	8068.0	0.2869	0.2145	-0.0004	0.0002	3.C70	0.0016	0.0015
655	0.503	315.039	0.00	19.31	0.9233	0.3388	0.2129	-0.0003	0.0003	2.725	0.0014	0.0014
656	0.503	314.624	0.00	21.26	2.9416	0.3829	0.2044	0.0001	0.0003	2.459	0.0011	0.0011
657	0.502	313.304	-0.00	23.15	0.9596	J.4250	C.2594	0.0001	0.0007	2.258	0.0008	0.0008
658	0.502	313.818	0.00	0.14	-0.0105	0.0179	0.3372	-0.0004	0.0002	-1.035	0.0020	0.0020

## TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	1			6.1.5.VV						
							IS COEFFICIEN				PRESS-COEF	
POINT	MACH	ú	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		AB	CAC
152	.934	740.423	00	.48	•2762	.0334	.0015	•0003	.0007			.0000
153	•933	739.665	00	1.56	.3723	.0340	.0029	•0001	.0008			.0000
154	•932	738.819	00	2.75	•4555	.0332	.0338	0001	.0014			.0000
155	•932	739.171	00	3.89	•5520	.0316	•0042	0002	.0015	•0		.0000
156	.935	741.123	00	5.05	•6341	•0294	.0036	0003	.0016	•0	063 (	.0000
157	.935	741-633	00	6.21	•7256	•0256	•0022	0002	.0023	•0	062 (	.0000
158	.935	741.853	00	7.41	.8082	•0228	.0001	0003	.0018	•0	062 (	.0000
159	.936	742.142	00	8.57	.8849	.0192	0026	0003	.0025	•0	061	.0000
160	•938	743.666	00	9.75	•9758	.0177	0035	0003	.0030	• 0	059 (	• 0000
161	.939	744.434	00	10.92	1.0432	.0144	0051	0002	.0020	•0	058 (	.0000
	TEST= 7	78 KUN=	1		07.10					CT.A.D.	<b>DOESE COS</b>	
							COEFFICIENTS				PRESS . COE	
POINT	MACH	ú	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
152	.934	740.428	00	• 48	. 2759	.0357	1515	.0015	.0003	7.739	•0062	33.8823
153	.933	739.665	00	1.56	.3712	• 0441	1451	.0029	0000	8.417	.0063	38.4627
154	•932	738.819	00	2.75	• 4534	• 0550	1367	.0038	0003	8.244	•0062	44.4235
155	•932	739.171	00	3.89	<ul><li>5486</li></ul>	.0689	1332	•0042	0005	7.959	.0062	46.1800
156	•935	741.123	00	5.05	•6291	.0851	1343	•003₺	0006	7.392	•0062	50.3211
157	•935	741.633	00	6.21	.7186	.1040	1319	•0022	0005	6.909	.0062	62.4935
158	•935	741.853	00	7.41	<b>.</b> 7985	.1257	1346	.0001	0003	6.301	.0061	95.8736
159	.936	742.142	00	8.57	.8722	.1509	1261	0026	.0001	5.779	.0060	115.7645
160	• 938	743.666	00	9.75	.9587	.182 <b>7</b>	1326	0035	.0003	5.247	•0058	150.2119
161	.939	744.434	00	10.92	1.0216	-2118	1272	0050	.0008	4.823	.0057	158.8708

TEST= 778 RUN= 2

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	1271= 1	18 KUN=	2									
						BODY AX	IS COEFFICIEN	ITS		BODY	PRESS.COE	FF
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
174	.863	682.369	00	• 47	•2967	•0202	.0017	.0004	•0008		0054	0.0000
175	-862	681.710	01	1.69	•4170	.0184	.0017	•0004	.0013		0054	0.0000
176	.8o3	682.428	00	2.81	•5235	.0168	•0027	.0002	.0020	•	0054	0.0000
177	. 864	683.866	00	4.05	.6146	.0138	•0047	.0001	•0020	•	0054	0.0000
178	- 863	682.635	00	5.17	•7038	.0098	•0056	0001	•002 <b>7</b>		0053	0.0000
179	.863	683.244	00	6.32	•7786	•0048	.0057	0001	.0030		0053	0.0000
180	- 862	681.772	00	7.44	<ul><li>8453</li></ul>	•0005	•0050	0001	•0028	•	0052	0.0000
181	- 863	682.839	01	8.60	<b>.</b> 8790	0018	•0036	.0001	•0030	•	0052	0.0000
182	-863	683.198	00	9.74	•9370	0020	.0039	0001	.0019	•	0051	0.0000
183	- 867	680.037	00	10.86	•9664	0018	0028	0004	.0027	•	0052	0.0000
185	•868	686.924	00	11.98	•9870	0006	0009	0006	.0033		0052	0.0000
186	-866	685.168	00	12.99	•9846	.0015	.0036	0005	.0038		0051	0.0000
187	•869	688.151	00	14.09	•9734	•0063	.0001	.0001	.0013	•	0051	0.0000
188	.869	688.435	00	15.15	1.0043	.0077	.0000	0001	.0010	•	0049	0.0000
189	-868	686.978	00	16.33	1.0508	.0083	0002	•0002	.0008	•	0047	0.0000
191	<b>.</b> 8 <b>7</b> 2	689.984	00	18.50	1.1158	.0073	.0007	0000	.0024	•	0045	0.0000
	TEST= 7	78 RUN=	2			,						
DOINT	MACH	0	0671				COEFFICIENTS				.PRESS.CDE	
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
174	-863	682.369	00	•47	• 2965	.0226	1308	.0017	.0004	13.125	•0054	16.8910
175	.862	681.710	01	1.69	•4163	.0307	1335	.0017	.0004	13.559	.0054	17.0666
176 177	• 863	682.428	00	2.81	•5220	•0425	1295	•0027	-0001	12.278	.0054	27.6705
	• 864 843	683.866	00	4.05	•6121	.0572	1269	•0046	0003	10.705	•0054	40.2195
178 179	• 863	682.635	00	5.17	.7001	•0731	1205	•0056	0006	9.577	• 0053	48.6897
180	•863 •862	683.244 681.772	00 00	6.32	• 7734	•0905	1103	•0057	0007	8.544	.0053	66.5092
181	.863	682.839	01	7.44 8.60	.8381	•1099	0944	•0050	0008	7.623	• 0052	107.6696
182	.863	683.198	00	9.74	.8694	• 1296	0670	•0036	0005	6.709	.0051	179.5767
183	.867	686.037			.9238	•1565	0437	•0038	0007	5.903	•0050	220.9885
185	-868	686.924	00 00	10.86	• 9494	.1803	0201	0028	•0002	5.266	.0051	300.4239
186	•856	685.168	00	11.98 12.99	• 9656	- 2042	-0129	0011	0004	4.729	.0051	201.4120
187	.869	638.151		14.09	•9591 •9426	• 2228	.0358	.0034	0013	4.304	.0049	166.7767
188	.869	688.435	00	15.15	•9426	• 2430 2430	•0512	•0001	• 0000	3.879	.0049	134.5880
189	-868	686.978	00	16.33	1.0061	•2699 •3035	•0576	0000	0001	3.584	• 0048	145.5057
191	-872	689.984		18.50	1.0559		.0657	0001	•0002	3.315	.0045	146.5712
.,.	•0.2	5074704		10.50	1.0009	.3610	•0803	.0006	0002	2.925	•0042	146.3202

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	3									_
							IS COEFFICIEN				PRESS.COEF	
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CL8	CNB	CSF		CAB	CAC
192	• 805	630.597	01	.33	• 2 <b>7</b> 05	.0178	.0016	•0005	.0017			0.0000
193	.806	631.524	01	1.54	•3865	.0138	.0013	•0005	.0025			0.0000
194	.808	632.958	01	2.71	•5002	.0071	.0011	<b>-</b> 0004	.0022			0.000
195	.807	632.163	01	3.90	•6226	0008	.0007	.0002	.0031	•	0050 (	.0000
196	-805	629.908	00	5.13	•7200	0101	-0006	0001	.0026	•	0050 (	.0000
197	.807	632.049	00	6.26	.8183	0144	.0018	0005	.0043	•	0049 (	.0000
198	.837	631.865	00	7.40	.8652	0189	0008	0004	.0035	•	0049 (	0.0000
199	.806	630.818	00	8.53	.9142	0211	0015	0004	.0040	•	0049 (	.0000
200	.809	633.715	00	9.68	•9646	0172	0302	0002	.0032	•	0049 (	.0000
201	.807	632.373	00	10.72	.9866	0143	.0042	0002	.0040		0048 (	.0000
202	.839	634.209	00	11.87	.9875	0100	.0106	0006	.0057		0047 (	.0000
203	118.	635.706	01	12.86	1.0054	0027	.0154	0002	.0051		0047 (	.0000
204	.810	634.798	00	13.97	.9622	.0024	.0005	0001	.0032		0047	.0000
205	.810	634.708	00	16.15	1.0084	.0047	.0010	0002	.0032		0047 (	.0000
206	-811	636.043	01	18.29	1.0761	.0047	.0016	0003	.0052		0041 (	.0000
	TEST= 7	78 RUN=	3									_
					STABL		COEFFICIENTS				.PRESS.CDE	
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
192	<b>.</b> 805	630.597	01	•33	•2703	.0194	1163	.0016	.0005	13.946	.0050	14.0800
193	.806	631.524	01	1.54	.3860	.0241	1164	.0013	.0004	15.999	•0050	13.3772
194	.808	632.958	01	2.71	• 4993	.0308	1186	.0011	.0004	16.234	.0050	15.3098
195	.807	632.163	01	3.90	•6212	.0415	1164	.0007	.0002	14.955	•0050	15.8117
196	.835	629.908	00	5.13	•7180	.0543	1136	•0006	0002	13.218	• 0050	23.1529
197	.807	632.049	00	6.26	<ul><li>8150</li></ul>	.0750	1041	.0017	0007	10.870	•0049	44.9254
198	.807	631.865	00	7.40	•8604	.0928	0815	0009	0003	9.276	.0048	90.4776
199	.836	630.818	00	8.53	•9072	.1147	0477	0015	0002	7.911	•0048	124.7361
200	.809	633.715	00	9.68	•9537	.1453	0260	0003	0002	6.565	.0048	260.8944
201	.837	632.373	00	10.72	• 9721	.1695	.0047	•0041	0010	5.735	.0047	238.3061
202	.809	634.209	00	11.87	-9684	.1933	.0224	•0102	0027	5.011	.0046	146.4472
203	.811	635.706	01	12.86	.9808	.2212	•0420	•0149	0037	4.434	.0046	174.6825
204	.810	634.798	00	13.97	•9331	.2345	.0725	•0005	0002	3.979	.0046	120.2822
205	.810	634.708	00	16.15	.9673	.2851	.0926	.0009	0005	3.393	•0045	114.8233
206	.811	636.043	01	18.29	1.0203	. 3422	.1073	.0015	0008	2.982	.0039	109.5528
200	•011	23000.3										

TEST= 778 RUN= 4

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	4									
						BODY AX	IS COEFFICIEN	ats.		BODY	PRESS.COEF	F
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
285	.752	578.353	00	.44	.2522	.0172	.0016	•0005	.0004			.0000
286	.753	579.566	00	1.65	.3626	.0133	.0013	.0005	.0001			0.0000
287	.753	579.495	00	2.79	.4615	.0066	.0008	.0004	.0013			0.0000
288	.752	578.544	00	3.99	•5636	0028	.0008	.0003	.0019			.0000
289	.753	579.257	00	5.15	•6590	0137	•0021	.0005	.0002			0.000
290	.754	580.443	01	6.32	.7506	0254	.0022	•0004	.0019			0.0000
291	.755	581.024	00	7.48	.8442	0345	.0006	0003	.0026			0.0000
292	.755	581.509	00	8-63	.8977	0365	.0001	0004	•0032			0.0000
293	.755	581.565	00	9.74	.9378	0321	.0007	•0003	.0015			0.0000
294	.754	580.246	00	10.82	.9527	0269	•0000	0002	.0014			0.0000
295	.753	579.576	00	11.89	.9633	0183	•0042	0001	.0031			0.0000
296	.755	581.132	00	12.94	.9544	0104	.0003	.0003	.0021			0.0000
297	.757	582.980	00	13.98	.9645	0046	.0007	0000	.0021			0.0000
298	.757	583.130	00	16.17	1.0004	.0007	.0010	0002	.0027			0.0000
299	.757	583.829	00	18.31	1.0592	.0010	.0014	•0000				
300	759	584.903	00		1.1207	.0043	.0014		.0027			0.0000
301	.758	584.645	01		1.1883			0002	.0039			0.0000
302	.760	585.838	00			•0040	•0009	.0000	.0035			0.0000
303	.752	578.814	00	.39	1.2666 .2619	•0022	•0009	0002	.0038			0.0000
303	•172	210.014	00	• 39	• 5019	.0167	•0015	-0005	.0005	•	0047 (	0.0000
	TEST= 7	78 RUN=	4									
					STAB	LITTY AXIS	COEFFICIENTS			STAR	PRESS-COEF	: <b>c</b>
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
285	.752	578.353	00	.44	.2521	.0191	1066	.0016	• 0005	13.205	.0047	9.3867
286	.753	579.566	00	1.65	.3621	.0237	1055	.0013	.0004	15.272	.0047	10.0894
287	.753	579.495	00	2.79	.4607	.0291	1047	.0008	.0003	15.846	.0047	11.2690
288	.752	578.544	00	3.99	• 5624	.0364	1016	•0008	-0003	15.450	.0047	11.6706
289	.753	579.257	00	5.15	•6576	.0455	0952	.0021	.0003	14.453	.0047	14.9584
290	.754	580.443	01	6.32	• 7489	•0573	0852	•0022	•0001	13.059	.0047	14.8580
291	.755	581.024	00	7.48	-8415	.0758	0773	.0006	0003	11.109	.0047	28.1098
292	.755	581.509	00	8.63	8930	•0986	0487	.0001	0004	9.054	• 0045	88.8462
293	.755	581.565	00	9.74	•9297	.1270	0118	.0007	•0002	7.319	•0045	
294	.754	580.246	00	10.82	9408	.1524	•0129	0000	0002	6.172		210.5705
295	.753	579.576	00	11.89	• 9464	• 1806	.0387	-004L	0002 0009		-0044	184.9708
296	.755	581.132	00	12.94	•9325	-2036	.0663			5.240	•0044	152.0927
297	.757	582.980	00	13.98	.9370	• 2285		•0003	•0002	4.581	• 0043	150.8378
298	757	583.130	00	16.17	.9606	•2793	• 0860 1054	.0007	0002	4.100	•0043	105.9127
299	757	583.829	00	18.31			•1056	•0009	0004	3.439	• 0042	104.4068
300	759	584.903	00	20.35	1.0053 1.0492	-3338	•1235	.0013	0004	3.012	.0038	94.1167
301	.758	584.645	01	22.50	1.0492	-3938	•1258	•0009	0005	2.664	.0032	107.1676
302	.760	585.838				• 4584	•1338	.0009	0003	2.392	.0024	117.8351
303	.752	578.814	00 00	24.55	1.1511	•5284	•1521	.0007	0006	2.179	.0017	136.0939
203	•172	>10.014	00	• 39	.2618	.0185	1082	.0015	•0005	14.169	•0047	10.2651

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

TEST= 778 RUN= 5 Q6/19/67.						IXA YOOB	S COEFFICIEN		BODY PRESS-COEFF		
POINT	MACH	0	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
325	.702	526.501	0L	.43	2389	.0165	0014	•0006	.0018	• 0046	0000
-326	.702	526.565	01	1.51	.3457	.0129	.0015	.0006	-0012	•0046	0000
327	700	524.808	= •.0 0	2.69	- 4409	.0065	0012	.0005	0010_	•0046	0000
328	.701	525.522	00	3.82	•5302	0029	0012	•0004	.0004	-0046	0000
329	-702	526.714		4.88	.6184	0128	.0019	• 3005	.0019	<b>-</b> 0046	0000
330	•702	527.154	00	6.05	•7008	0249	•0023	•0005	• 0008	0045	0000
331		526.644	00	7.16	.7710	0379	.0018	•0005	•000 <u>7</u>	•0045	0000
332	702	527.275	00_	8.33	.8669	0436	0006	-,0006	0034	.0045	000
333	.703	528.098	•00	9.37	. 8812	0356	0040	0009	,0038	• 0044	0000
334	704	529.011	00	10.47	•9097	-,0298	-,0022	0002	.0025	.0044	0000
335	.701	526.559	01	11.55	.9297		00005	0005	.0020	.0044	0000
336	.703	528,505	00	12.64	•9526	0161	.0021	• 2004	.0011	.0043	0000
_337	.701	526.489	00	13.73	.9610	0110	.0012	0001	•0027	.0043	0000
338	.705	529.883	00	15.87	•9989		0011	0002	•0021	0042	0000
339	702	526.905	01	17.98	1.0335	0018	.0013	.0000	. 0041	.0040	0000
340	.702	527,431	00	20.07	1.0926	.0019	.0010	.0002	•0026	<u>.</u> 0034	,0000
341	-706	530.581	00	22.07	1,1530	0034_	-0013	0001	•0033	•0028	0000
342	7.02	526.671	00	-18	. 2480	.0164	.0019	•0005	.0014	.0045	-,000
343	701	525.412	01	- 14	.2413	.0163	.0011	•0006	.0020	.0045	0000
344	• 702	526.427	01	.15	.2434	.0164	.0015	.0006	.0017	.0045	0000

	TEST= 7	75 1711:12	ל										
			-		STAR	TLITY AXIS	COFFFICIENTS		STAB.PRESS.COEFF				
POINT	MACH	87.7	4r [4	ALPHA	CL	_ CD	CPM	CLS	CN5	L/D	CDB	PB-1	
325	.702	526.501	^]	.43	73R7	~ .01⊣3	1040	.0014	.0015	13.072	.0046	7-0149	
326	• 702	476.444	11	1.51	• 3452	• 11220	<b>-</b> .n985	• 9015	.0005	15.662	.0046	-7-5545	
327	• 700	524,305	<b>⊸.</b> ე∩	2,69	.4411	.11272	-,0972	.0012	.0004	16.204	.0046	_8.2447.	
328 329	.701	7/7,527	20	3.42	.5292	• 1325	0951	.0013	•0003	16.273	• 0046	8-4330	
329	.702	524.714	<b></b> 11	4.22	.6172	.4349	np43	.0019	.0003	15.475	.0046	_8_4079	
330	.702	527.154	µ n	6.15	.4445	.04 +1	<b>~</b> •∩735	.0024	.0002	14.236	.0045	9.9639	
331	.702	727.544	00	7.16	. 7697	1586	1659	.001A	.0003	13.143	.0045	10.4659	
332	.702	521.212	10	ઘ ુર	. H640	·4425	<b>~.</b> ∧5∩3	0007	0005	10.478	.0045	56,9720	
333	•703	524.144	• 0.0	9.37	.4752	•10H3	0049	0041	0003	8.085	•0044	103.2774	
334	.704	524.011	<b>-</b> , 1 1	10.47		.1361	.024]	0022	.0002	6.612	.0043	119,2145	
335	.701	524.554	41	11.55	•4153	.1643	•n508	• 0006	.0004	5.570	.0043	127.2458	
336	.703	524.515	<b>-</b> • ↑ ∩	12.54	.4330	.1927	• 073B	.0022	0000	4.841	.0042	125.7400	
337	•701	474.44	00	13.73	.4362	.2173	. 1957	.0017	0004	4.307	.0041	100.1402	
338	.705	571.243	00	15.37	.4618	.2697	.1161	.0010	0005	3.566	.0040	94.8697	
339	.702	526, 1. 5	-, 1]	17.30	<b>,</b> 9H36	.3173	.1331	.0012	0004	3.100	.0038	88.0933	
340	.702	527.441	<b>-</b> 0 1	20.07	1.0256	3766	.1362	•001n	non2	2.723	.0032	92.6109	
341	.706	ን 3 7 • 5 ላ [	01	22.07	1.0672	.4364	.1371	.0011	<b>-</b> .nou6	2.446	.0026	106.1637	
342	.702	525.571	33	.14	.2490	. 1177	1030	.0019	.0005	14.443	.0045	8.1067	
343	•701	525.412	- 11	.14	.2412	-1169	1nn9	•0011	•0006	14.247	•0045	8.1067	
344	.702	526.427	01	.15	.2433	• 01 ነው	1027	.0015	.0006	14.312	.0045	7.3663	

## TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	6			4004 144	5 605F51615W			2024	20000 0000	-
							S COEFFICIEN				PRESS.COEF	
POINT	MACH	4	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
358	•497	310.221	00	.22	-2125	.0167	.0018	.0005	0001			0.0000
359	•498	311.021	00	1.29	.3073	.0137	.0014	.0005	0004			.0000
360	.497	309.871	00	2.34	.3822	.0081	-0011	.0004	0005			-0000
361	•448	311.025	00	3.43	.4728	.0006	.0012	.0004	0011			.0000
362	<b>-</b> 496	309.790	•00	4 = 47	•5301	0080	•0016	.0003	0019			•0000
363	.497	310.331	•00	5.56	.6137	0183	.0015	.0004	0025			.0000
364	•496	309.717	•00	6.62	.6741	0309	.0012	.0003	0027			0000
365	•497	310.341	•00	6.63	.6841	0305	.0016	.0003	0031			.0000
366	•497	310.039	•00	7.71	•7578	0437	•0006	•0004	0029			0.000
367	-478	311.752	•00	8.83	.8129	0469	.0003	0005	0008			0.0000
368	.501	314.882	•00	9.92	.8726	0414	0004	0004	.0009			0.0000
369	•530	313.633	•00	11.02	.8974	0336	.0009	0002	0013			0.0000
370	.530	313.722	•00	12.07	•9297	0266	.0019	0001	0009			0.000
371	•500	313.493	.00	13.21	•9469	0219	.0013	0002	0011			0.000
372	.499	311.974	•00	15.38	1.0078	0139	•0015	0001	0002			0.000
373	•498	310.788	•00	17.48	1.0536	0092	•0009	0001	0005	•		0.0000
374	<b>.</b> 5J0	313.259	•00	19.54	1.1024	0052	.0013	.0002	0015	•		0.000
375	.504	317.007	.00	21.60	1.1608	0011	•0012	0002	•0004	•	0027	0.0000
377	.497	309.590	.00	•25	-2164	.0171	.0013	•0004	0019	•	.0041	0.0000
	TEST= 7	78 RUN=	6		CTAN	TIETU ANTO	COESELCIENTO			5740		
00.14.7				A 1 D 1 1 A			COEFFICIENTS	G. 5	cus.		.PRESS.COE	
PUINT	MACH	Ţ	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
358	MACH -497	ų 310.221	BETA 00	-22	CL •2124	CD •0175	CPM -•0926	-0019	.0005	L/D 12.137	CDB -0041	PB-1 4.4047
358 359	MACH •497 •498	310.221 311.021	BETA 00 00	•22 1•29	CL •2124 •3069	CD •0175 •0206	CPM 0926 0845	.0019 .0015	.0005 .0005	L/D 12.137 14.900	.0041 .0041	PB-1 4.4047 4.5929
358 359 360	MACH •497 •498 •497	310.221 311.021 309.871	BETA 00 00 00	•22 1•29 2•34	CL •2124 •3069 •3815	CD •0175 •0206 •0237	CPM 0926 0845 0836	.0019 .0015 .0012	.0005 .0005 .0004	L/D 12.137 14.900 16.109	CDB •0041 •0041 •0041	PB-1 4.4047 4.5929 4.2792
358 359 360 361	MACH •497 •498 •497 •498	310.221 311.021 309.871 311.025	BETA 00 00 00	.22 1.29 2.34 3.43	CL •2124 •3069 •3815 •4719	CD •0175 •0206 •0237 •0289	CPM 0926 0845 0836 0759	.0019 .0015 .0012 .0012	.0005 .0005 .0004 .0003	L/D 12.137 14.900 16.109 16.313	CDB •0041 •0041 •0041	PB-1 4.4047 4.5929 4.2792 4.7059
358 359 360 361 362	MACH •497 •498 •497 •498	310.221 311.021 309.871 311.025 309.790	BETA 00 00 00 00	•22 1•29 2•34 3•43 4•47	CL •2124 •3069 •3815 •4719 •5291	CD .0175 .0206 .0237 .0289 .0333	CPM 0926 0845 0836 0759 0689	.0019 .0015 .0012 .0012 .0016	.0005 .0005 .0004 .0003	L/D 12.137 14.900 16.109 16.313 15.869	CDB •0041 •0041 •0041 •0041 •0040	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282
358 359 360 361 362 363	MACH •497 •498 •497 •498 •496	310.221 311.021 309.871 311.025 309.790 310.331	BETA 00 00 00 00 00	.22 1.29 2.34 3.43 4.47 5.56	CL •2124 •3069 •3815 •4719 •5291 •6126	CD •0175 •0206 •0237 •0289 •0333 •0412	CPM 0926 0845 0836 0759 0689 0596	.0019 .0015 .0012 .0012 .0016	.0005 .0005 .0004 .0003 .0002	L/D 12.137 14.900 16.109 16.313 15.869 14.854	COB •0041 •0041 •0041 •0041 •0040	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172
358 359 360 361 362 363 364	MACH •497 •498 •497 •498 •496 •497	310.221 311.021 309.871 311.025 309.790 310.331 309.717	BETA 00 00 00 00 00 00	.22 1.29 2.34 3.43 4.47 5.56 6.62	CL •2124 •3069 •3815 •4719 •5291 •6126 •6731	CD •0175 •0206 •0237 •0289 •0333 •0412 •0470	CPM 0926 0845 0836 0759 0689 0596 0546	.0019 .0015 .0012 .0012 .0016 .0015	.0005 .0005 .0004 .0003 .0002 .0003	L/D 12.137 14.900 16.109 16.313 15.869 14.854 14.312	CDB .0041 .0041 .0041 .0041 .0040 .0040	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172 4.4298
358 359 360 361 362 363 364 365	MACH • 497 • 498 • 497 • 498 • 496 • 497	310.221 311.021 309.871 311.025 309.790 310.331 309.717 310.341	BETA 00 00 00 00 00 00 00	.22 1.29 2.34 3.43 4.47 5.56 6.62 6.63	CL • 21 24 • 30 69 • 38 15 • 47 19 • 52 91 • 61 26 • 67 31 • 68 31	CD .0175 .0206 .0237 .0289 .0333 .0412 .0470	CPM 0926 0845 0836 0759 0689 0546 0532	.0019 .0015 .0012 .0012 .0016 .0015 .0012	.0005 .0005 .0004 .0003 .0002 .0003 .0001	L/D 12.137 14.900 16.109 16.313 15.869 14.854 14.312 14.032	COB .0041 .0041 .0041 .0041 .0040 .0040 .0040	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172 4.4298 4.5176
358 359 360 361 362 363 364 365 366	MACH •497 •498 •497 •498 •496 •497 •497	310.221 311.021 309.871 311.025 309.790 310.331 309.717 310.341 310.089	BETA 00 00 00 00 00 00 00 	.22 1.29 2.34 3.43 4.47 5.56 6.62 6.63 7.71	CL •2124 •3069 •3815 •4719 •5291 •6126 •6731 •6831 •7568	CD •0175 •0206 •0237 •0289 •0333 •0412 •0470 •0487 •0584	CPM 0926 0845 0836 0759 0689 0596 0546 0532 0398	.0019 .0015 .0012 .0012 .0016 .0015 .0017	.0005 .0005 .0004 .0003 .0002 .0003 .0001	L/D 12.137 14.900 16.109 16.313 15.869 14.854 14.312 14.032 12.951	COB .0041 .0041 .0041 .0040 .0040 .0040 .0040 .0040	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172 4.4278 4.5176 5.2706
358 359 360 361 362 363 364 365 366 367	MACH •497 •498 •496 •497 •496 •497 •496 •497	310.221 311.021 309.871 311.025 309.790 310.331 309.717 310.341 310.089	BETA 00 00 00 00 00 00 00 	.22 1.29 2.34 3.43 4.47 5.56 6.62 6.63 7.71 8.83	CL •2124 •3069 •3815 •4719 •5291 •6126 •6731 •6831 •7568 •8104	CD .0175 .0206 .0237 .0289 .0333 .0412 .0470 .0487 .0584	CPM0926084508360759068905960546053203980303	.0019 .0015 .0012 .0012 .0016 .0015 .0012 .0017	.0005 .0005 .0004 .0003 .0002 .0003 .0001 .0001	L/D 12.137 14.900 16.109 16.313 15.869 14.854 14.312 14.032 12.951 10.327	COB .0041 .0041 .0041 .0040 .0040 .0040 .0040 .0040 .0040	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172 4.4298 4.5176 5.2706
358 359 360 361 362 363 364 365 366 367 368	MACH •497 •498 •497 •496 •497 •496 •497 •498 •501	310-221 311-021 309-871 311-025 309-790 310-331 309-717 310-341 310-089 311-752 314-882	BETA00000000000000	.22 1.29 2.34 3.43 4.47 5.56 6.62 6.63 7.71 8.83 9.92	CL 2124 3069 3815 4719 5291 6126 6731 6831 7568 8104 8667	CD .0175 .0206 .0237 .0289 .0333 .0412 .0470 .0487 .0584 .0785	CPM 0926 0845 0836 0759 0689 0546 0532 0398 0303	.0019 .0015 .0012 .0016 .0015 .0012 .0017 .0006 .0002	.0005 .0005 .0004 .0003 .0002 .0003 .0001 .0001 .0003 0005	L/D 12.137 14.990 16.109 16.313 15.869 14.854 14.312 14.032 12.951 10.327 7.914	COB .0041 .0041 .0041 .0040 .0040 .0040 .0040 .0040	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172 4.4298 4.5176 5.2706 25.2235 70.5248
358 359 360 361 362 363 364 365 366 367 368 369	MACH	310.221 311.021 309.871 311.025 309.790 310.331 309.717 310.341 310.089 311.752 314.882 313.683	BETA00000000000000	.22 1.29 2.34 3.43 4.47 5.56 6.62 6.63 7.71 8.83 9.92 11.02	CL 2124 3069 3815 4719 5291 6126 6731 6831 7568 8104 8667 8873	CD .0175 .0206 .0237 .0289 .0333 .0412 .0470 .0487 .0584 .0785 .1095 .1386	CPM 0926 0836 0759 0689 0546 0532 0398 0302 0352	.0019 .0015 .0012 .0012 .0016 .0015 .0017 .0006 .0002 0004	.0005 .0005 .0004 .0003 .0002 .0003 .0001 .0001 .0003 0005	L/D 12.137 14.900 16.109 16.313 15.869 14.854 14.312 14.032 12.951 10.327 7.914 6.404	COB .0041 .0041 .0041 .0040 .0040 .0040 .0040 .0040 .0039	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172 4.4298 4.5176 5.2706 25.2235 70.5248 90.6031
358 359 360 361 362 363 364 365 366 367 368 369 370	MACH .497 .498 .497 .498 .497 .496 .497 .498 .501 .500	310-221 311-021 309-871 311-025 309-790 310-331 309-717 310-341 310-089 311-752 314-882 313-683 313-722	BETA00000000000000	.22 1.29 2.34 3.43 4.47 5.56 6.62 6.63 7.71 8.83 9.92 11.02 12.07	CL 2124 3069 3815 4719 5291 6126 6731 6831 7568 8104 8667 8873	CD .0175 .0206 .0237 .0289 .0333 .0412 .0470 .0487 .0584 .0785 .1095 .1386 .1684	CPM 0926 0845 0836 0759 0689 0546 0532 0398 0303 0002 0352 0365	.0019 .0015 .0012 .0012 .0016 .0015 .0017 .0006 .0002	.0005 .0005 .0004 .0003 .0002 .0003 .0001 .0001 .0003 0005	L/D 12.137 14.900 16.109 16.313 15.869 14.854 14.312 14.032 12.951 10.327 7.914 6.404 5.432	COB .0041 .0041 .0041 .0040 .0040 .0040 .0040 .0040 .0039 .0039 .0038	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172 4.4298 4.5176 5.2706 25.2235 70.5248 90.6031 91.3560
358 359 360 361 362 363 364 365 366 367 368 369 370 371	MACH •497 •498 •497 •498 •497 •497 •497 •498 •501 •500 •500	310-221 311-021 309-871 311-025 309-790 310-331 309-717 310-341 310-089 311-752 314-882 313-683 313-722 313-493	BETA00000000000000	.22 1.29 2.34 3.43 4.47 5.56 6.62 6.63 7.71 8.83 9.92 11.02 12.07 13.21	CL 2124 3069 3815 4719 5291 6126 6731 6831 7568 8104 8667 8873 9147	CD .0175 .0206 .0237 .0289 .0333 .0412 .0470 .0487 .0584 .0785 .1095 .1386 .1684 .1951	CPM 0926 0845 0836 0759 0689 0596 0532 0398 0303 0002 0352 0665 0893	.0019 .0015 .0012 .0016 .0015 .0017 .0006 .0002 0004 .0009	.0005 .0005 .0004 .0003 .0002 .0003 .0001 .0003 0005 0003	L/D 12.137 14.900 16.109 16.313 15.869 14.854 14.312 14.032 12.951 10.327 7.914 6.404 5.432 4.751	COB .0041 .0041 .0041 .0040 .0040 .0040 .0040 .0040 .0039 .0039 .0038	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172 4.4298 4.5176 5.2706 25.2235 70.5248 90.6031 91.3560 88.8462
358 359 360 361 362 363 364 365 366 367 368 369 370 371	MACH •497 •498 •497 •498 •497 •497 •497 •498 •501 •500 •500 •500	310-221 311-021 309-871 311-025 309-790 310-331 309-717 310-341 310-089 311-52 314-882 313-683 313-722 313-93 311-974	BETA00000000000000	.22 1.29 2.34 3.43 4.47 5.56 6.62 6.63 7.71 8.83 9.92 11.02 12.07 13.21	CL 2124 3069 3815 4719 5291 6126 6731 6831 7568 8104 8667 8873 9147 9269 9755	CD .0175 .0206 .0237 .0289 .0333 .0412 .0470 .0487 .0584 .0785 .1095 .1386 .1095 .1386 .1084	CPM 0926 0845 0836 0759 0689 0546 0532 0398 0303 0002 0352 0893 1273	.0019 .0015 .0012 .0012 .0016 .0015 .0012 .0017 .0006 .0002 -0004 .0009 .0019	.0005 .0005 .0004 .0003 .0002 .0003 .0001 .0001 .0003 0005 0003 0005 0005	L/D 12.137 14.900 16.109 16.313 15.869 14.854 14.312 14.032 12.951 10.327 7.914 6.404 5.432 4.751 3.843	COB .0041 .0041 .0041 .0040 .0040 .0040 .0040 .0039 .0039 .0038 .0038	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172 4.4298 4.5176 5.2706 25.2235 70.5248 90.6031 91.3560 88.8462 92.6109
358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373	MACH 497 498 497 498 496 497 497 498 500 500 510 498	310.221 311.021 309.871 311.025 309.790 310.331 309.717 310.341 310.089 311.752 314.882 313.683 313.722 313.493 311.974	BETA00000000000000	.22 1.29 2.34 3.43 4.47 5.56 6.62 6.63 7.71 8.83 9.92 11.02 12.07 13.21 15.38 17.48	CL 2124 3069 3815 4719 5291 6126 6731 6831 7568 8104 8667 8873 9147 9269 9755 1.0077	CD .0175 .0206 .0237 .0289 .0333 .0412 .0470 .0487 .0584 .0785 .1095 .1386 .1684 .1951 .2538 .3078	CPM 0926 0845 0836 0759 0689 0546 0532 0398 0302 0302 0352 0465 0893 1273 1493	.0019 .0015 .0012 .0012 .0016 .0015 .0017 .0006 .0002 0004 .0009 .0019 .0019	.0005 .0005 .0004 .0003 .0002 .0003 .0001 .0001 .0003 0005 0005 0005 0005	L/D 12.137 14.900 16.109 16.313 15.869 14.854 14.312 14.032 12.951 10.327 7.914 6.404 5.432 4.751 3.843	COB .0041 .0041 .0041 .0040 .0040 .0040 .0040 .0039 .0039 .0038 .0037 .0035	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172 4.4298 4.5176 5.2706 25.2235 70.5248 90.6031 91.3560 88.8462 92.6109 86.3364
358 359 360 361 362 363 364 365 366 367 368 370 371 372 373	MACH .497 .498 .497 .498 .497 .497 .497 .498 .500 .500 .500 .499 .499 .500	310-221 311-021 309-871 311-025 309-790 310-331 309-717 310-341 310-089 311-752 314-882 313-683 313-722 313-493 311-778 310-788	BETA00000000000000	.22 1.29 2.34 3.43 4.47 5.56 6.62 6.63 7.71 8.83 9.92 11.02 12.07 13.21 15.38 17.48 19.54	CL 2124 3069 3815 4719 5291 6126 6731 6831 7568 8104 8667 8873 9147 9269 9755 1.0077	CD .0175 .0206 .0237 .0289 .0333 .0412 .0470 .0487 .0584 .0785 .1095 .1386 .1084 .1951 .2538 .3078	CPM 0926 0845 0836 0759 0689 0546 0532 0398 0303 0002 0352 0465 0893 1273 1493 1646	.0019 .0015 .0012 .0012 .0016 .0015 .0017 .0006 .0002 0004 .0009 .0019 .0013	.0005 .0005 .0004 .0003 .0002 .0003 .0001 .0003 0005 0005 0005 0005 0005	L/D 12.137 14.900 16.109 16.313 15.869 14.854 14.312 14.032 12.951 10.327 7.914 6.404 5.432 4.751 3.843 3.274 2.860	COB .0041 .0041 .0041 .0040 .0040 .0040 .0040 .0039 .0039 .0038 .0037 .0035	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172 4.4298 4.5176 5.2706 25.2235 70.5248 90.6031 91.3560 88.8462 92.6109 86.3364
358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373	MACH 497 498 497 498 496 497 497 498 500 500 510 498	310.221 311.021 309.871 311.025 309.790 310.331 309.717 310.341 310.089 311.752 314.882 313.683 313.722 313.493 311.974	BETA00000000000000	.22 1.29 2.34 3.43 4.47 5.56 6.62 6.63 7.71 8.83 9.92 11.02 12.07 13.21 15.38 17.48	CL 2124 3069 3815 4719 5291 6126 6731 6831 7568 8104 8667 8873 9147 9269 9755 1.0077	CD .0175 .0206 .0237 .0289 .0333 .0412 .0470 .0487 .0584 .0785 .1095 .1386 .1684 .1951 .2538 .3078	CPM 0926 0845 0836 0759 0689 0546 0532 0398 0302 0302 0352 0465 0893 1273 1493	.0019 .0015 .0012 .0012 .0016 .0015 .0017 .0006 .0002 0004 .0009 .0019 .0019	.0005 .0005 .0004 .0003 .0002 .0003 .0001 .0001 .0003 0005 0005 0005 0005	L/D 12.137 14.900 16.109 16.313 15.869 14.854 14.312 14.032 12.951 10.327 7.914 6.404 5.432 4.751 3.843	COB .0041 .0041 .0041 .0040 .0040 .0040 .0040 .0039 .0039 .0038 .0037 .0035	PB-1 4.4047 4.5929 4.2792 4.7059 4.0282 4.4172 4.4298 4.5176 5.2706 25.2235 70.5248 90.6031 91.3560 88.8462 92.6109 86.3364

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	7											
							BODY AXIS CJEFFICIENTS				BODY PRESS.COEFF			
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNR	CSF		CAB	CAC		
378	-242	119.300	.00	.17	.2105	.0185	.0020	0000	0065	•		0.0000		
379	-292	119.204	•00	1.16	-3116	.0164	.0020	.0003	0072	•	0038	0.0000		
380	.272	119.301	•00	2.19	.3580	.0111	•0015	.0000	0070	•	0038	0.0000		
381	-292	119.304	• 00	4.19	•5196	0035	.0018	.0001	0084	•	0038	0.0000		
382	.270	117.959	.00	6.31	•6298	0230	.0013	0000	0089	•	0037	0.0000		
383	.292	119.418	•00	8.36	<b>. 7</b> 662	0477	.0006	0009	0094	•	0037	0.0000		
384	.290	117.988	•00	9.42	.8243	0533	.0301	0023	0033	•	0038	0.0000		
385	.291	118.894	•00	10.49	.8934	0515	0017	0020	0026	•	0036	0.0000		
386	-292	119.612	.00	11.57	• 9065	0421	0011	0020	0041	•	0036	0.0000		
387	<ul><li>290</li></ul>	118.402	•00	12.69	.9718	0369	0011	0014	0054	•	0036	0.0000		
388	.291	119.159	-00	14.83	1.0001	0254	.0005	0039	0081	•	0034	0.0000		
389	.291	119.152	.00	16.90	1.0726	0165	.0004	0002	0094	•	0031	0.0000		
390	.292	119.718	.00	18.96	1.1210	0117	.0304	0000	0103	•	0030	0.0000		
391	. 291	118.926	•00	20.94	1.1641	0077	.0009	.0000	0111	•	0026	0.0000		
392	-291	119.012	•00	• 22	.2073	.0194	.0320	0000	0065		0039	0.0000		
	TEST= 7	78 RUN=	7											
						STABILITY AXIS COEFFICIENTS					STAB.PRESS.COEFF			
POINT	MACH	Ų	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1		
378	.292	119.300	.00	• 17	• 2164	.0192	0805	.0020	0000	11.293	.0038	1.3929		
379	.292	119.204	.00	1.16	•3112	.0227	0705	•0020	.0002	13.707	.0038	1.5310		
98F	-292	119.301	.00	2.19	• 3573	• 0248	0692	•0015	0000	14.421	.0038	1.5812		
381	.242	119.304	•00	4.19	•5185	.0345	0592	.0018	0001	15.041	.0038	1.5812		
382	.290	117.959	•00	6.31	<ul><li>6285</li></ul>	.0463	0457	-0013	0002	13.563	.0037	1.3051		
383	•292	119.418	.00	8.36	• 7650	.0643	0222	•0004	0009	11.907	.0037	2.5098		
384	.290	117.988	.00	9.42	.8219	.0823	0170	0003	0023	9.985	.0037	13.7286		
385	· 29 1	118.894	•00	10.49	.8878	.1121	.0019	0021	0017	7.918	.0035	28.4235		
386	•292	119.612	•00	11.57	<ul><li>8965</li></ul>	.1405	.0351	0014	0017	6.382	.0035	40.0313		
387	•290	118.402	.00	12.69	• 9561	. 1776	.0729	0014	0011	5.384	•0035	42-1019		
388	.291	119.159	.00	14.83	• 9733	-2314	.1168	•0002	0010	4.206	.0032	46.0548		
389	.291	119.152	•00	16.90	1.0311	.2961	.1515	•0004	0003	3.483	•0030	48.5642		
390	-292	119.718	.00	18.96	1.0640	.3531	.1763	•0004	0002	3.014	.0028	43.1682		
391	-291	118.926	.00	20.94	1.0899	. 4089	-1837	•0003	0003	2.666	.0024	38.5251		
392	.291	119.012	.00	• 22	.2072	.0202	0818	•0020	0000	10.246	•0039	1.6816		

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

BODY AXIS COEFFICIENTS BI PUINT MACH U BETA ALPHA CNF CAF CLB CNB CSF 412	ODY PRESS.COEFF CAB CAC .0064 0.0000 .0064 0.0000
	.0064 0.0000 .0064 0.0000
412	.0064 0.0000
413 .934 737.33000 1.55 .3635 .03290002 .0000 .0004	
414 •932 735•95200 2•64 •4501 •03290021 •0000 •0005	.0063 0.0000
415 .933 736.99600 3.80 .5434 .03110017 .0000 .0007	.0063 0.0000
416 .934 737.32900 4.94 .6261 .028600110001 .0017	.0063 0.0000
417 .934 737.86700 6.13 .7197 .025400290002 .0019	.0062 0.0000
418	.0062 0.0000
419 .938 740.34600 8.49 .8799 .019100440004 .0023	.0062 0.0000
420 .937 739.734 .00 9.67 .9533 .015700520005 .0026	•0060 0•0000
421 .936 738.716 .00 10.82 1.0243 .012400580006 .0026	•0058 0•0000
422 .933 736.07100 .29 .2700 .0329 .0013 .0001 .0007	.0063 0.0000
TEST= 778 RUN= 8 STABILLTY AXIS COEFFICIENTS	STAB.PRESS.COEFF
POINT MACH Q BETA ALPHA CL CD CPM CLS CNS 1/D	COB PB-1
412 .932 735.78400 .39 .2746 .03401512 .0015 .0001 8.076	
413 .934 737.33000 1.55 .3625 .042714490001 .0000 8.481	
414 .932 735.95200 2.64 .4481 .053613800021 .0001 8.357	
415 .933 736.99600 3.80 .5401 .067013810017 .0001 8.059	
416 •934 737-32900 4.94 •6213 •082413560011 •0000 7.538	
417 .934 737.86700 6.13 .7129 .102213690029 .0001 6.977	
418 •936 738•965 -•00 7•30 •7940 •1244 -•1373 -•0046 •0004 6•383	
419 .938 740.34600 8.49 .8674 .148813180044 .0002 5.829	
420 •937 739•734 •00 9.67 •9371 •1757 -12710052 •0003 5.333	
421 •936 738-716 •00 10-82 1.0037 •204512070058 •0005 4.909	
422 .933 736.07100 .29 .2698 .03431499 .0013 .0001 7.865	

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 KUN=	9										
						BUDY AXIS CUEFFICIENTS					BODY PRESS.COEFF		
POINT	MACH	Q .	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC	
436	• გი∠	078.828	00	-31	.3106	.0196	.0019	.0002	•0007			0.0000	
437	-862	670.497	00	1.47	•4265	.0183	.0022	.0002	.0010			0.0000	
438	-862	678.638	00	2.63	•5268	-0163	.0003	•0000	•0009			0.0000	
439	.803	679.494	00	3.81	•6190	.0136	0002	0001	•0009			0.0000	
440	.802	678.554	-00	4.95	•7074	.0086	0011	0005	.0013			0.0000	
441	.864	080 <b>.</b> 510	00	6.11	.7875	.0061	0018	0007	•0034			0.0000	
442	-864	580 <b>.</b> 187	00	7.28	.8442	.0013	.0023	0006	.0032			0.000	
443	.804	68U• <b>4</b> 62	• 00	8.39	.8960	0032	0025	0006	•0025			0.000	
444	•8o5	680.834	00	9.53	.9310	0016	.0043	0003	•0029			0.0000	
445	-864	080.340	-00	10.62	•9632	0019	0027	0007	.0031			0.000	
446	-805	681.306	•00	11.76	.9846	0008	0024	0006	•0030			0.0000	
447	-867	682.913	•00	12.77	•9716	.0010	0036	0001	.0002			0.0000	
448	.866	002.320	• 00	13.90	.9887	•0028	0012	0003	.0010			0.0000	
449	•87U	685.333	00	16.16	1.0446	.0072	0003	.0001	0003			0.000	
450	.872	687. <b>-</b> 271	•00	18.31	1.1111	.0076	0010	0004	0001			0.0000	
451	.863	679.730	00	1.51	•4336	.0192	.0011	.0001	.0008	•	0055	0.000	
	TEST= 7	78 KUN=	9										
						ILITY AXIS	STAB.PRESS.COEFF			FF			
PUINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	P8-1	
436	.862	678.828	00	-31	.3105	•0213	1344	.0019	•0002	14.557	.0055	18.8862	
437	<ul><li>862</li></ul>	678.497	00	1.47	• 4259	• 0292	1375	.0022	.0001	14.590	.0054	17.4431	
438	•8o2	618.638	00	2.63	• 5255	•0404	1344	.0003	0000	12.995	• 0054	28.8627	
439	.863	679.494	00	3.81	.6167	• 0547	1331	0002	0001	11.265	.0053	34.2588	
440	.862	678.554	•00	4.95	.7041	• 0696	1303	0012	0004	10.110	.0053	53.7093	
441	.804	680.510	00	6.11	. 7824	•0899	1240	0018	0005	8.707	.0053	116.2028	
442	.864	080.187	00	7.28	. 8372	·1082	1008	.0023	0009	7.737	.0052	139.7947	
443	.864	680 <b>-</b> 462	-00	8.39	• 8868	.1276	0864	0026	0002	6.949	•0052	182.4610	
444	-865	680.834	00	9.53	•9184	• L525	0563	.0042	0010	6.020	.0050	190.9943	
445	.804	680.340	-00	10.62	.9471	·1750	0303	0028	0002	5-392	•0050	307.9533	
446	-805	081.306	- 00	11.76	. 9641	.1999	0040	0025	0001	4.824	.0049	203-6708	
447	. 007	082.913	•00	12.77	•9474	.2157	.0233	0035	.0007	4.392	.0050	140.0472	
448	.866	682.326	.00	13.90	• 9590	• 2402	.0328	0013	•0000	3.993	.0048	132.5178	
449	.870	685.333	00	16.16	1.0013	.2975	.0367	0003	.0002	3.365	•0045	144.9413	
450	.872	687.271	.00	18.31	1.0525	•3563	.0405	0011	0001	2.954	.0042	148.7060	
451	-863	674.730	00	1.51	.4329	•0306	1389	.0011	.0000	14.137	•0055	18.1961	

TEST= 778 RUN= 10

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

						BUDY AXI	S COEFFICIEN	TS		BODY	PRESS.COLF	F
TOINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		AB	CAC
465	• 8U5	627.101	00	•25	.2740	.0170	.0019	.0002	.0015	• 0	051 0	.0000
466	.805	627.710	00	1.45	.3915	.0130	.0020	.0002	.0021	• 0	051 0	.0000
467	.807	628.790	00	2.59	•5044	.0063	.0019	•0002	.0017	• 0	050 0	•000ò
468	•ცე7	629.334	00	3.80	•6224	0019	.0010	.0001	.0019	.0	050 0	•0000
469	<b>.</b> 805	027.504	00	4.94	•7194	0109	.0006	0001	.0018	• 0	050 0	.0000
470	.836	628.348	•00	6.12	.8114	0157	.0000	0006	.0027	-0	049 0	•0000
471	.800	028.253	•00	7.27	.8660	0196	0024	0007	•0029	• 0	049 0	•0000
472	•878	630.144	00	8.37	•9002	0177	.0002	0005	•0029			•0000
473	•899	631.054	00	9.51	•9645	0154	.0008	0001	.0017			• 0000
474	.873	031.440	00	10.60	•9859	0139	.0024	0001	•0028			•0000
475	.807	629.904	•00	11.69	•9919	0112	<b>.</b> 0058	0012	.0060	• 0		.0000
476	• 80 8	630.372	00	12.74	1.0091	0052	.0150	0006	•0062			•0000
477	• 809	631.629	00	13.80	.9676	0007	0001	0002	•0032			.0000
478	.81 i	633.542	00	16.02	1.0096	.0039	.0008	0001	.0031			.0000
479	.810	032.303	00	18-16	1.0669	.0036	.0008	0003	.0037			•0000
480	<b>.</b> 805	627.667	01	-28	•2797	.0169	.0023	-0003	.0023	• (	0050 0	•0000
481	•870	628.664	01	-29	•28 <b>47</b>	.0169	.0020	.0002	•0025	• (	050 0	.0000
	TEST= 7	778 KUN=	10		CT AL	RILITY AVIC	COEFFICIENTS			CTAD	.PRESS.COEF	- <del>-</del>
PUINT	МАСН		BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
465	-805	627.707	00	•25	• 2739	.0182	1186	•0019	.0002	15.059	•0051	11.2188
466	-805	627.710	00	1.45	.3911	.0229	1215	•0020	•0001	17.070	•0050	13.4776
467	.837		00	2.59	•5036	.0291	1232	.0019	•0001	17.316	•0050	14.6070
468	.807		00	3.80	•6212	.0393	1245	•0010	•0000	15.796	•0050	15.4102
469	-835		00	4.94	.7177	.0511	1223	•0006	0001	14.037	.0049	23.6549
470	.806		•00	6.12	.8084	.0708	1126	0001	0006	11.412	.0049	61.2386
471	.806		•00	7.27	.8615	.0901	0907	0025	0003	9.561	-0048	95.3716
472	•808		00	8.37	.8932	.1136	0561	.0001	0005	7.860	.0048	117.2067
473	.809	631.054	00	9.51	. 9538	.1441	0415	.0008	0002	6.621	.0048	313.9768
474	.839	031.446	00	10.60	.9716	.1677	0175	•0024	0005	5.793	.0047	307.2003
475	.807		.00	11.69	.9736	.1901	.0058	•0054	0024	5.122	•0046	166.4002
476	•808		00	12.74	.9854	.2176	.0228	.0145	0039	4.529	•0046	166.7767
477	•809		00	13.80	• 9398	.2300	.0531	0001	0002	4.086	.0045	109.9295
478	.811		00	16.02	.9693	-2825	.0623	.0007	0003	3.432	.0043	120.4707
479	.810		00	18.16	1.0127	.3360	•0755	•0006	0005	3.014	.0039	101.2707
480	-835	027.667	01	•28	• 2796	.0183	1193	.0023	.0003	15,258	•0050	12.5490
481	• d\) b	028-664	01	•29	• 2846	.0184	1192	.0021	.0002	15.504	.0050	12.1223

	TEST= 7	78 KUN= .	11			вару ах	IS COEFFICIEN	its		8008	Y PRESS.COEF	F
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
495	• 753	577.408	00	.21	-2592	.0164	.0020	•0002	.0014			.0000
496	.754	578.452	00	1.35	.3620	.0125	.0017	•0002	.0011			.0000
					•4684	•0060	.0015	•0002	.0008			.0000
497	725	579.734	00	2.47	.5702	0037	.0015	.0002	•0004			.0000
498	.752	577.042	00	3.63								.0000
499	•755	o 79 • 756	00	4.81	•6694	0150	.0024	•0002	.0002			.0000
500	•754	578.683	00	5.94	.7635	0265	.001d	0001	.0013			
501	• 754	<b>578.824</b>	•00	7.12	.8499	0348	.0002	0003	.0008			.0000
502	•754	579.113	00	8.22	.8820	0318	.0040	•0003	.0012			.0000
503	•755	579.331	00	9.34	.9371	0310	0013	0002	.0012			.0000
504	.750	580.356	.00	10.40	• 94 L 8	0245	.0038	0003	.0010			.0000
505	.754	579.148	00	11.49	•9664	0182	.0061	0002	.0019			.0000
506	•755	580.152	00	12.58	.9951	0114	.0109	0003	.0019			.0000
507	.755	579.445	00	13.65	<b>.</b> 9608	0062	0003	0004	.0027			.0000
508	.750	581.033	00	15.83	.9954	.0008	.0009	0003	و 0023		.0043 (	.0000
509	.760	584.122	00	17.96	1.0485	.0013	.0012	0005	•0026		.0041	.0000
510	.759	583.837	00	20.04	1.1074	.0047	.0009	0003	.0028		.0035 (	.0000
511	. 759	583.536	00	22.09	1.1624	.0052	.0004	0003	.0019			.0000
512	.753	570.008	00	•21	.2591	.0163	.0024	.0002	.0010			.0000
	TEST= 7	778 KUN=	11		6A.T.2	11 1 TV A V T C	COEFFICIENTS			CTA	B.PRESS.COE	re
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS			
495	.753	577.408	00	.21	• 2591	• 0174	1118			L/D	CDB	P8-1
496	.754	578.452	00	1.35	.3616	•0210	1118	.0020	.0002 .0002	14.902	•0048	9.5121
								.0017		17.210	•0048	9.4117
497	.755	579.734	00	2.47	.4677	• 0261	1117	.0015	.0001	17-900	•0049	10.3404
498	•752 •755	577.042	00	3.63	.5693	•0324	1106	.0014	.0000	17-545	•0048	11.5702
499		579.756	00	4.81	.6683	.0411	1067	•0025	•0000	16.263	.0048	15-6862
500	.754	578.683	00	5.94	.7621	•0526	0988	.0018	0002	14.478	.0047	15.7615
501	•754	578.824	•00	7.12	.8476	•0708	0899	•0002	0003	11.966	•0047	31.7490
502	• 754	579.113	00	8.22	.8774	• 0946	0505	.0040	0003	9.278	•0046	87.9678
503	• 755	579.331	00	9.34	•9297	•1214	0272	0013	.0000	7.659	•0046	265.4121
504	.756	5 80 - 356	.00	10.40	.9308	. 1459	0008	.0036	0010	6.379	•0045	136.2825
505												
	.754	579.148	00	11.49	•9506	•1746	.0181	•0060	0015	5.444	• 0044	163.7649
506	•754 •755	580.152	00	12.58	.9737	·2057	.0349	.0106	0027	4.734	•0044	152.4708
507	•754 •755 •755	580.152 579.445	00 00	12.58 13.65	.9737 .9351	•2057 •220 <b>7</b>	.0349 .0667	-0106 0004	0027 0003	4•734 4•237	•0044 •0043	152.4708 98.2589
	•754 •755 •755 •756	580.152 579.445 581.033	00 00 00	12.58 13.65 15.83	.9737 .9351 .9575	•2057 •2207 •2723	.0349	.0106	0027	4.734	•0044	152.4708
507	•754 •755 •755	580.152 579.445	00 00	12.58 13.65	.9737 .9351	•2057 •220 <b>7</b>	.0349 .0667	-0106 0004	0027 0003	4•734 4•237	•0044 •0043	152.4708 98.2589
507 508	•754 •755 •755 •756	580.152 579.445 581.033	00 00 00	12.58 13.65 15.83	.9737 .9351 .9575	•2057 •2207 •2723	.0349 .0667 .0790	.0105 0004 .0008	0027 0003 0005	4•734 4•237 3•516	•0044 •0043 •0041	152.4708 98.2589 99.7648
507 508 509	.754 .755 .755 .756	580.152 579.445 581.033 584.122	00 00 00	12.58 13.65 15.83 17.96	.9737 .9351 .9575 .9970	•2057 •2207 •2723 •3246	.0349 .0667 .0790 .0912	.0105 0004 .0008 .0010	0027 0003 0005 0008	4.734 4.237 3.516 3.071	.0044 .0043 .0041 .0039	152.4708 98.2589 99.7648 89.6001

	IESI≈ 7	78 RUN= 1	12								
						RODA WXI	S CUEFFICIEN	TS		BODY PRESS.	COEFF
POINT	MACH	a	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
528	.702	525.865	~.00	-15	-2487	.0159	.0020	.0003	.0013	-0046	0.0000
529	.702	525.783	00	1.20	.3404	.0126'	.0017	.0003	.0012	.0046	0.0000
530	.701	524.767	00	2.36	•4462	.0061	-0015	-0002	.0008	• 0046	0.0000
531	.702	526-491	00	3.51	•5386	0031	.0014	•0002	•0004	•0046	0.0000
532	.702	526.421	00	4.62	•6240	0137	.0021	•0002	•0005	• 0046	0.0000
533	•702	526.532	00	5.75	.7045	0252	•0023	.0003	0003	•0046	0.0000
534	.702	525.949	00	6.92	.7947	0385	.0019	.0003	.0009	• 0045	0.0000
535	.702	526.197	00	8.04	.8618	0420	-0017	.0001	.0003	•0045	0.0000
536	.702	526.380	•00	9.11	.8766	0352	0031	0010	.0020	• 0044	0.0000
537	.704	528.239	•00	10.20	.8972	0273	0045	0010	.0037	•0044	0.0000
538	.703	527.444	00	11.33	•9492	0225	.0037	0001	•0010	.0043	0.0000
539	.703	527.414	00	12.39	.9577	0165	.0047	0003	•0022	.0043	0.0000
540	.704	528.160	•00	13.51	.9628	0109	•0002	0004	.0015	•0043	0.0000
541	.703	527.145	00	15-69	1.0006	0036	.0008	0002	.0017	.0042	0.0000
542	.704	528.555	00	17.81	1.0537	0015	.0012	0003	.0021	.0039	0.0000
543	.705	529.580	00	19.85	1.0881	•0026	-0012	0002	•0020	.0034	0.0000
544	.705	529.772	00	21.88	1.1345	.0043	•0005	0002	.0012	•0027	0.0000
545	.701	525.400	00	-15	•2488	.0160	.0018	•0002	.0015	.0046	0.0000

	1F21= 1	/8 KUN=	12									
					STAE	SILITY AXIS	CUEFFICIENTS			STAB	.PRESS.COEF	F
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
528	.702	525.865	00	•15	• 2486	.0166	1047	.0020	.0003	14.975	.0046	7.8055
529	.702	525.783	00	1.20	. 3400	.0197	1048	.0017	.0002	17.220	-0046	7.1780
530	.731	524.767	00	2.36	• 4456	.0245	1037	.0016	.0001	18.200	.0046	8.1318
531	•702	526.491	00	3.51	•5378	.0299	1017	-0014	.0001	18.006	•0046	8.7090
532	.702	526.421	00	4.62	•6230	.0366	0923	.0021	.0001	17.007	.0046	8.8345
533	.702	526.532	00	5.75	• 7035	.0455	0843	.0023	•0000	15.449	.0046	10.7670
534	.702	525.949	00	6.92	• 7936	.0575	0792	.0019	.0001	13.795	.0045	10.9176
535	.702	526.197	00	8.04	<ul><li>8592</li></ul>	.0790	0622	.0017	0001	10.879	.0045	54.9642
536	•702	526.380	.00	9.11	-8711	.1040	0196	0033	0005	8.378	.0044	92.6109
537	• 704	528.239	.00	10.20	.8879	.1321	.0129	0046	0002	6.720	.0043	108.4225
538	.703	527.444	00	11.33	• 9351	• 1644	.0302	•0036	0009	5.690	•0043	133.5203
539	<b>.7</b> 03	527.414	00	12.39	• 9389	-1894	.0523	•0045	0013	4.958	.0042	111.9362
540	-704	528.160	•00	13.51	•9388	.2142	•0740	.0001	0004	4.382	.0042	93.6148
541	.703	527.145	00	15.69	<b>9642</b>	·2671	•0928	1000	0004	3.610	.0040	93.3638
542	.704	528.555	00	17.81	1.0037	• 3208	.1040	.0011	0006	3.128	.0038	86.3364
543	• 705	529.580	00	19.85	1.0225	.3719	.0990	.0011	0007	2.750	.0032	89.5991
544	•735	529.772	00	21.88	1.0512	<b>.</b> 4267	•0937	-0004	0004	2.464	•0025	105.4108
545	-701	525.400	00	-15	• 2487	.0167	1048	-0018	•0002	14.892	• 0046	7.8557

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	13									
						BODY AX	IS COEFFICIEN			BODY	PRESS.COE	FF
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
558	. 499	311.782	00	-14	.2190	•0153	.0021	.0003	.0020		0041	0.0000
559	.498	311.165	00	1.17	• 3076	.0128	.0019	.0004	.0016		.0041	0.0000
560	•478	311.166	00	2.25	.3807	.0073	.0012	.0003	.0019		0041	0.0000
561	.498	311.078	00	3.31	.4693	0002	.0012	.0002	.0013		0041	0.0000
562	.498	310.553	00	4.38	•5329	0090	.0019	.0004	.0003			0.0000
563	.498	310.561	00	5.45	•6060	0194	•0012	.0003	.0003			0.0000
564	•497	310.128	00	6.55	•6734	0321	.0012	.0003	0001			0.0000
565	.497	309.613	00	7.63	.7444	0451	.0005	.0002	0001			0.0000
566	.497	310.397	•00	8.74	.8106	0482	.0000	0006	.0020			0.0000
567	478	310.601	•00	9.81	.8702	0434	0006	0006	.0016			0.0000
568	.497	310.110	00	10.93	.8897	0350	.0010	0002	.0015			0.0000
569	.500	313.250	00	11.99	.9206	0280	.0019	0001	.0019			0.0000
570	.490	308.496	.00	13.13	.9482	0233	.0015	0004	.0017			0.0000
571	.491	309.993	•00	15.30	1.0076	0149	.0012	0001	.0007			0.0000
		311.283	00	17.39	1.0388	0100	.0016	0003	•0020			0.0000
572	•498			19.45	1.0388	0056	.0012	0001	.0018			0.0000
573	.499	312.249	00	21.51	1.1355	0015	.0006	0001	.0001			0.0000
574	.499	312.230	•00		•2199	.0159	.0021	•0002	0003			0.0000
575	-498	310.727	00	•26				.0002	0003			0.0000
576	•498	311.346	00	<b>.</b> 20	-2229	.0160	.0019	¥000 <del>4</del>	0002	•	14004	0.0000
	TESI= /	78 KUN=	13									
							CULFFICIENTS				.PRESS.COE	FF
POINT	MACH	ų.	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
558	.499	311.782	00	.14	.2190	.0159	0926	.0021	• 0003	13.816	.0041	4.5929
559	• 49°	311.165	00	1.17	.3073	.0191	0885	•0020	.0003	16.112	.0041	4.2667
560	-49 b	311.166	00	2.25	.3802	.0222	0872	.0012	• 0002	17.136	.0041	4.4423
561	.498	311.078	00	3.31	- 4085	•0269	0829	.0013	.0001	17.443	.0041	4.4298
562	•448	310.553	00	4.38	.5320	.0317	0776	.0019	.0002	16.785	.0041	4.0659
563	. 498	310.501	00	5.45	.6051	.0383	0697	.0013	.0002	15.818	.0040	4.3545
564	•497	310.128	00	6.55	.6726	.0450	0652	.0012	.0002	14.962	.0040	4.2416
565	.497	309.613	00	7.63	.7438	.0541	0535	.0005	.0002	13.738	.0040	4.8816
566	.497	310.397	•00	8.74	.8144	.0764	0425	0001	0006	10.662	.0039	24.0313
567	498	310.601	•00	9.81	.8649	.1054	0151	~.0007	0005	8.202	.0039	62.4935
568	.497	310.110	00	10.93	.8802	. 1344	.0176	.0010	0004	6.552	.0038	84.0776
569	.500	313.250	00	11.99	.9063	.1638	.0482	.0019	+.0005	5.533	.0037	80.9404
570	496	300.490		13.13	.9288	•1927	.0691	.0014	0007	4.819	.0037	87.0894
571	.497	309.993		15.30	.9759	-2515	.1034	.0012	0005	3.880	.0035	90.7285
572	498	311.283		17.39	.9943	.3010	.1211	.0015	0008	3.303	.0033	80.3130
573	•499	312.249		19.45	1.0320	•3585	.1319	.0011	0005	2.879	.0030	77.8032
574	•479	312.236		21.51	1.0570	•4149	.1243	.0005	0003	2.548	•0024	81.6933
575	•477 •498	310.727	00	•26	.2199	.0169	0930	.0021	•0002	13.024	.0041	4.3420
576	•498	311.346	00	•20	• 2229	.0168	0910	.0021	•0004	13.285	-0041	4.3043
210	• 770	7110740	- • 00	• 20	• 6667	• 0100		40017	* 0007	130203	•0071	T+3UT3

TEST= 778 RUN= 13

	TEST= 7	78 RUN=	14									
							S COEFFICIEN			BODY	PRESS.CQE	FF
PCINT	MACH	ú	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
591	•292	119.872	00	•16	-2148	.0144	.0020	.0005	0005			0.0000
592	-292	119.197	00	1.16	-3118	.0119	.0026	•0004	0016	•	0038	0.0000
593	-292	119.873	00	2.16	•3563	.0073	.0021	•0005	0014			0.0000
594	-292	114.199	•00	3.20	•4441	.0007	.0021	•0004	0018	•	0038	0.0000
595	.291	119.102	.00	4.18	-5107	0083	.0018	.0001	0020	•	0038	0.0000
596	• 291	119.107	•00	5.26	•5864	0168	.0020	•0004	0028		0039	0.0000
597	•291	119.109	•00	6.31	•6330	0278	.0011	.0001	0024		0039	0.0000
598	•291	119.113	.00	7.33	.7101	0405	.0008	0001	0027		0037	0.0000
599	.292	119.217	.00	8.41	.7579	0523	.0008	0004	0030		0037	0.0000
600	-292	119.238	00	9.43	.8341	0572	•0001	0016	.0091		0037	0.0000
601	.242	119.270	•00	10.51	-8815	0565	0015	0024	.0038		0036	0.0000
602	• 291	118.639	.00	11.57	•9231	0470	0011	0017	.0083		0036	0.0000
603	-292	114.454	00	12.70	•9440	0413	0009	0012	.0072		0035	0.0000
604	. 292	119.445	00	14.86	1.0075	0294	.0009	0006	.0041		0034	0.0000
605	. 242	119.629	00	16.95	1.0690	0206	-0011	0004	.0028		0031	0.0000
606	.243	120.140	00	20.97	1.1619	0114	.0008	0001	.0018		0026	0.0000
607	-294	120.977	.00	9.49	-8415	0578	0004	0016	.0034		0037	0.0000
	TEST= 7	7ø RUN=	14		C**A0		205551015070					
SOLLE	14 4 6 1 1		N (** *				COEFFICIENTS				.PRESS.COE	
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	P8-1
591	• 292	119.872	00	-10	.2147	•0150	0837	.0020	.0005	14.349	•0038	1.4557
592	-292	119.197	00	1.16	-3115	.0183	0775	.0026	.0003	17.062	•0038	1.5310
593	• 292	119.873	00	2.16	.3558	.0207	0758	•0022	.0004	17.207	.0038	1.4933
594	-242	119.199	.00	3.20,	• 4433	.0255	0742	•0021	•0002	17.387	.0038	1.4306
595	. 291	119.102	•00	4.18	•5100	.0289	0708	.0018	.0000	17.627	.0038	1.2925
596	- 241	119.107	•00	5.26	. 5854	.0370	0594	•0020	.0002	15.822	.0038	1.3553
597	• 29 1	119.109	•00	6.31	.6322	.0419	0546	.0011	0000	15.072	•0038	1.4055
598	.211	119.113	•00	7.33	. 7095	.0504	0460	.0008	0002	14.064	.0037	1.3553
599	-242	119-217	• 00	8.41	. 7574	.0591	0406	.0007	0005	12.810	.0037	2.3341
600	• 242	114.538	00	9.43	.8323	•0802	0322	0002	0016	10.382	•0037	14.3059
601	- 292	119.270	•00	10.51	.8770	.1053	0165	0019	0021	8.330	.0035	26.7921
602	- 291	118.639	•00	11.57	.9138	-1391	.0190	0014	0015	6.570	.0035	39.7176
603	• 29 2	119.454	00	12.70	.9299	. 1673	.0459	0011	0010	5.559	.0034	42.5411
604	• 292	119.445	00	14.86	.9813	•2299	•0933	.0007	0008	4.268 °	.0032	46.1176
605	-242	119.629	00	16.95	1.0286	• 2920	•1232	•0009	0007	3.523	.0030	44.3607
606	-293	120.180	00	20.97	1.0891	•4051	-1484	.0007	0004	2.688	.0024	36.5803
6Ù7	•244	150.411	•00	9.49	. 8395	.0817	0330	0007	0015	10.271	•0036	13.9294

	TEST= 7	78 KUN=	15									
						BODY AX	IS COEFFICIE	NTS		BODY	PRESS-COE	FF
PUINT	MACH	ú	BETA		CNF	CAF	CLB	CNB	CSF		CAB	CAC
639	•929	731.612	00		.1404	.0213	.0005	•0004	0000		0063	0.0000
640	-931	733.140	00	1.31	-2598	.0239	0000	•0004	0008	•	0063	0.0000
641	•953	734.777	00	2.48	•3570	.0256	0015	•0005	0000	•	0063	0.000
642	.932	733.893	00	3.68	•4583	•0246	0013	•0004	0008	•	0064	0.0000
643	•933	735.033	00	4.87	•5502	•0232	0010	.0003	.0005	•	0066	0.0000
644	.931	733.275	00	6.07	•6502	.0209	.0008	•0006	0006		<b>ს</b> 066	0.0000
645	.934	735.610	00	7.30	•7512	•0200	0003	.0003	.0010		0068	0.0000
646	•935	736.425	00	8.51	•8354	.0185	.0029	.0004	.0006	•	006 <b>7</b>	0.0000
647	.930	737.282	00		•9139	•0169	.0027	•0003	.0002	_	0060	0.0000
648	-940	740.064	00		•9839	.0168	.0027	.0001	0001		0058	0.0000
649	.933	734.629	00	.16	•1354	.0207	•0006	-0004	.0001		0063	0.0000
	TEST= 7	78 RUN=	15		STAR	ILITY AXIS	COEFFICIENTS			STAR	.PRESS.COE	cc
POINT	MACH	ن ن	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
639	.929	/31.612	00	-11	- 1404	.0216	0766	•0005	• 0004	6.514	• 0063	15.9385
640	.931	733.140	00	1.31	. 2592	.0299	0858	0000	.0004	8.682	•0063	19.3714
641	.933	734.777	00	2.48	. 3555	.0410	0850	0015	•0006	8.679	•0063	24.3369
642	-932	733.893	00	3.68	•4558	.0540	0830	0012	•0005	8.434	•0064	27.5859
643	.933	735.033	00	4-87	• 5462	.0698	0805	0010	.0004	7.823	•0065	42.7888
644	•931	733.275	00	6.07	• 6444	.0896	0789	.0008	•0005	7.194	.0066	61.1794
645	•934	735.610	00	7.30	• 7426	.1154	0847	0002	.0003	6.437	• 0068	113.0418
646	•935	730.425	00	8.51	.8234	.1419	0775	.0029	0000	5.801	.0067	133.1490
647	•936	737.282	00	9.71	. 8982	.1709	0710	.0028	0001	5.256	•0059	166.7428
648	•940	740.064	00	10.85	• 9636	-2018	0727	•0026	0004	4.775	.0057	199.8461
649	.933	734.629	00	-10	.1353	.0211	0802	•0006	•0004	6.412	.0063	17.6550

TEST= 778 RUN= 16

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

							IS COEFFICIE <sup>1</sup>	NTS		BOOY	PRESS-COE	F
PUINT	MACH	ú	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
663	-863	677.534	01	•02	•1583	.0174	.0013	.0005	.0009		.0055	0.0000
664	- 865	679.244	01	1.19	<b>.</b> 2490	.0152	.0010	.0005	.0017		.0054	0.0000
665	<ul><li>864</li></ul>	678.719	01	2.40	.3787	.0111	.0008	.0004	.0014			0.0000
666	- 863	677.791	00	3.62	•5093	.0065	.0011	-0004	.0009			0.0000
667	.863	678-173	01	4.79	.0147	.0029	.0012	.0004	.0014			0.0000
668	-862	677.355	00	5.97	.7024	,0008	0011	0002	.0017			0.0000
669	-864	679.087	00	7.17	<b>.7</b> 768	.0001	0023	.0003	.0008		.005 <b>3</b>	0.0000
670	-865	079.413	00	8.29	.8128	.0026	0013	.0002	.0007		.0052	0.0000
671	-866	680.517	01	9.42	.8396	.0058	.0024	.0007	.0006		.0051	0.0000
672	-865	679.244	01	10.49	.8606	.0070	.0052	.0010	.0004			0.0000
673	- 863	677.616	01	3.63	.5112	.0043	.0013	.0003	.0017			0.0000
	TEST= 7	78 RUN=	16									
		_					COEFFICIENTS			STAR	.PRESS.COE	F
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
663	-863	677.534	01	•02	•1289	.0174	0572	.0013	• 0005	7.408	•0055	11.0099
664	-805	679.244	01	1.19	. 2487	.0204	0602	.0010	.0005	12,191	0054	15.3992
665	•864 •863	678.719 677.791	01	2.40	•3779	.0269	0642	.0008	.0003	14.048	•0054	20.0458
666 667	-863	078.173	00 01	3.62	.5080	.0387	0756	.0011	.0003	13.127	.0053	20.3523
668	- 862	677.355	00	4.79 5.97	•6125	.0542	0779	.0012	.0003	11.301	•0053	27.0955
669	.864	679.087	00	7.17	•6987 •7710	.0739	0678	0011	0001	9.455	•0053	63.3863
670	-865	679.413	00	8.29	• 8042	.0971	0465	0023	•0006	7.940	•0052	71.1103
671	.866	680.517	01	9.42	.8276	.1199	0036	0013	.0004	6.707	•0052	73.9302
672	.865	679.244	01	10.49	•8453	-1431	.0280 .0526	-0024	-0003	5.783	•0050	99.6781
673	.863	677.616	01	3.63	• 5099	.1635 <b>.0366</b>	0736	.0052 .0013	.0000 .0002	5.170	•0050	105.5632
	-005		401	3433	• ,0 ,,	• 0.000	- 6 0 1 3 0	•0013	• 0002	13.923	0053	20.9653

CAF

BODY AXIS COEFFICIENTS

CLB

CNB

CSF

BODY PRESS.COEFF

CAC

CAB

POINT	MAGN	¥	DLIM	MEFTIA	CINI	CAI	GED	0,10	05.	•		0
687	.805	622.876	01	•02	.1152	•0168	-0014	•0006	.0008	.(		.0000
688	. BÙ 7	027.454	01	1.19	•2232	.0144	.0013	.0006	.0015		0051. 0	.0000
689	.805	625.957	01	2.36	.3379	•0091	.0013	.0006	.0021		0050 0	.0000
690	.807	628.039	01	3.53	•4512	•0008	.0017	•0005	.0011		0050 0	•0000
691	.800	020.323	01	4.73	•5632	0083	.0019	•0004	.0016		0.050 0	.0000
692	.800	027.030	00	5.96	•6925	0128	.0003	.0001	.0012		0049	•0000
693	.80B	628.823	00	7.14	.7602	0137	0010	.0000	.0013		0049	•0000
694	.800	027.185	01	8.24	•7841	0090	.0019	•0005	.0009		0048	.0000
695	.806	626.899	01	9.32	.8124	0051	.0044	.0011	.0012		0048	.0000
696	. 808	628.288	01	10.41	.8302	0009	.0021	•0006	.0014		0048 0	.0000
697	.810	030.654	01	11.51	.8421	•0054	.0009	•0005	.0007		0047	•0000
698	-80b	628.823	01	12.57	•8677	•0083	.0010	•0006	~0014		0047	-0000
699	.809	629.727	00	13.70	•856	•0109	.0006	•0006	.0002	•(	0047 0	.0000
700	.812	632.117	00	15.98	•9501	.0123	.0006	•0005	.0005	•(	0045 0	.0000
701	.814	634.420	01	18.12	1.0076	.0132	.0007	.0007	0001		0041 0	•0000
702	.807	627.222	01	•05	.1146	.0152	.0010	•0006	.0023	.(	0051 0	•0000
	TEST= 7	78 KUN=	17		STAR	LLITY AXIS CO	HEETCTHNTS			STAR	.PRESS.COEF	: <b>F</b>
TAZEN	MACH	ú	BETA	ALPHA	CL STAD	CD CD	CPM	CLS	CNS	L/D	CDB	PB-1
PUINT 687	•8J5	625.870	01	•02	•1152	.0168	0527	.0014	.0006	6.857	.0051	9.9800
688	.807	027.454	01	1.19	•2229	.0191	0512	.0013	.0006	11.670	•0050	10.6666
689	.801	625.957	01	2.36	.3374	.0230	0493	.0013	•0005	14.670	•0050	11.7701
690	.807	628.039	01	3.53	• 4504	.0230 .0286	0477	.0018	.0004	15.748	•0050	15.3501
691	.806	626.323	01	4.73	• 5621	•0200 •0382	0462	.0019	•0003	14.715	•0049	18.0965
692	.806	627.030	00	5.96	•6903	•0592	0483	.0003	-0000	11.660	.0049	32.4901
693	.608	028.823	00	7.14	. 7563	.0809	0208	0009	.0001	9.349	•0048	69.0261
694	.806	627.185	01	8.24	.7776	•1034	.0243	.0019	.0002	7.520	•0048	87.5402
695	.806	626.899	01	9.32	.8028	.1266	.0497	.0045	.0003	6.341	.0048	131.1264
696	-808	028.288	01	10.41	.8171	•1492	.0747	.0022	.0002	5.477	.0047	131.8620
697	.810	630.654	01	11.51	.8245	•1733	.0911	.0010	.0003	4.758	•0046	114.7586
648	.808	028.823	01	12.57	• 8456	.1969	.1037	.0011	.0003	4.295	•0046	101.5172
699	. 807	629.127	00	13.70	• 8584	2204		.0007	•0005	3.895	•0045	101.5172
700	.812	632.117	00	15.98	.9106	2734	-1341	.0007	.0003	3.331	•0043	92.8735
701	.814	634.420	01	18.12	.9541	•3259	.1389	.0009	.0004	2.928	.0039	95.6322
702	<b>.</b> 807	027.222	01	•05	• 1146	.0153	0526	.0010	.0006	7.467	.0051	9.2689

TEST= 778 RUN= 17

MACH

PUINT

BETA ALPHA

CNF

	1EST= 7	78 RUN=	18									
						BODY AXI	S COEFFICIENT	ΓS		BODY	PRESS.COEF	F
PUINT	MACH	J	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	(	CAB	CAC
716	•754	576.339	01	.03	.1025	.0164	.0011	.0005	.0012		0048	.0000
717	•753	575.816	00	1.14	-2046	.0143	.0010	.0006	.0007		00,48	0000
718	- 753	575.372	01	2.28	.305l	•0093	.0011	.0005	.0013		0049	.0000
719	- 754	576.427	01	3.45	•4090	.0017	.0020	.0007	.0012		0048	.0000
720	.754	577.049	01	4.59	.5003	0075	.0018	.0006	.0007		0048	0.0000
721	•755	517.861	00	5.77	•6132	0177	.0013	.0004	.0018		0048	.0000
722	. 755	578.204	00	6.95	.7138	0220	•0005	.0001	.0017		.0047	0.000
723	• 755	577.799	00	8.09	•7542	0185	0002	.0002	.0012		.0047	0.000
724	.755	577.584	00	9.18	.7909	0133	.0027	.0007	.0000		0046	0.000
725	•757	514.565	01	10.25	.8123	0067	.0017	.0006	.0013		0046	0.0000
726	• 754	576.653	00	11.35	.8300	0008	.0023	.0006	.0001		.0045 (	0.000
727	• 755	277.484	00	12.43	. 8492	.0032	.0011	.0005	.0007		0045	0.0000
728	.750	578.587	00	13.58	.8783	•0063	.0007	.0004	•0005		.0045	0.000
729	• 75 7	580.130	00	15.81	.9318	.0095	•0006	•0006	0002		.0043	0.000
730	• 759	281.540	00	17.93	.9863	.0112	.0010	.0007	.0002		.0041	0.000
731	•7 <b>&gt;</b> 8	580.437	00	20.02	1.0487	.0127	.0011	.0007	0014		.0035	0.000
732	• 75B	580.449	00	22.14	1.1199	•01.14	•0002	.0009	0036		.0027	0.0000
733	• 754	571.205	00	6.97	.7049	0238	.0004	.0001	.0019		.0047	0.000
	TEST= 7	70 RUN=	18		<b>67.</b> 4.3							
							COEFFICIENTS				.PRESS.COE	
POINT	МАСН	ú	BETA	ALPHA	CL	Çυ	CPM	CLS	CNS	L/D	CDB	PB-1
716	MACH -754	576.339	BETA 01	.03	CL •1024	ເນ .0165	CPM 0497	.0011	.0005	<b>L/D</b> 6.206	<b>CDB</b> •0048	PB-1 8∙6069
716 717	MACH •754 •753	576.339 575.816	BETA 01 00	.03 1.14	CL •1024 •2043	0165 .0183	CPM 0497 0471	.0011 .0010	.0005 .0006	L/D 6.206 11.164	.0048 .0048	PB-1 8.6069 8.4352
716 717 718	MACH • 754 • 753 • 753	576.339 575.846 575.372	BETA 01 00 01	.03 1.14 2.28	CL •1024 •2043 •3046	0165 .0183 .0214	CPM 0497 0471 0448	.0011 .0010 .0012	•0005 •0006 •0005	L/D 6.206 11.164 14.234	.0048 .0048 .0049	PB-1 8.6069 8.4352 9.2935
716 717 718 719	MACH • 754 • 753 • 753 • 754	576.339 575.816 575.372 576.427	BETA 01 00 01 01	.03 1.14 2.28 3.45	CL • 1024 • 2043 • 3046 • 4083	CU .0165 .0183 .0214 .0263	CPM 0497 0471 0448 0397	.0011 .0010 .0012 .0020	.0005 .0006 .0005 .0005	L/D 6.206 11.164 14.234 15.525	.0048 .0048 .0049 .0048	PB-1 8.6069 8.4352 9.2935 9.5632
716 717 718 719 720	MACH • 754 • 753 • 753 • 754 • 754	576.339 575.846 575.372 576.427 577.049	BETA 01 00 01 01	.03 1.14 2.28 3.45 4.59	CL • 1024 • 2043 • 3046 • 4083 • 5055	00 .0165 .0183 .0214 .0263 .0330	CPM 0497 0471 0448 0397 0339	.0011 .0010 .0012 .0020 .0018	.0005 .0006 .0005 .0005	L/O 6.206 11.164 14.234 15.525 15.318	.0048 .0048 .0049 .0048 .0048	PB-1 8.6069 8.4352 9.2935 9.5632 11.1571
716 717 718 719 720 721	MACH • 754 • 753 • 753 • 754 • 754 • 755	576.339 575.816 575.372 576.427 577.049 577.807	BETA 01 00 01 01 01	.03 1.14 2.28 3.45 4.59 5.77	CL • 1024 • 2043 • 3046 • 4083 • 5055 • 6121	.0165 .0183 .0214 .0263 .0330 .0442	CPM 0497 0471 0448 0397 0339 0306	.0011 .0010 .0012 .0020 .0018	.0005 .0006 .0005 .0005 .0005	L/D 6.206 11.164 14.234 15.525 15.318 13.848	.0048 .0048 .0049 .0048 .0048	P8-1 8.6069 8.4352 9.2935 9.5632 11.1571 13.4620
716 717 718 719 720 721 722	MACH • 754 • 753 • 753 • 754 • 755 • 755	576.339 575.816 575.372 576.427 577.049 577.867 578.204	BETA 01 00 01 01 00 00	.03 1.14 2.28 3.45 4.59 5.77 6.95	CL • 1024 • 2043 • 3046 • 4083 • 5055 • 6121 • 7115	.0165 .0183 .0214 .0263 .0330 .0442 .0646	CPM 0497 0471 0448 0397 0339 0306 0187	.0011 .0010 .0012 .0020 .0018 .0014	.0005 .0006 .0005 .0005 .0005 .0002	L/O 6.206 11.164 14.234 15.525 15.318 13.848 11.014	CDB •0048 •0049 •0048 •0048 •0048 •0047	P8-1 8.6069 8.4352 9.2935 9.5632 11.1571 13.4620 33.9613
716 717 718 719 720 721 722 723	MACH - 754 - 753 - 753 - 754 - 756 - 755 - 755	576.339 575.846 575.372 576.427 577.049 577.867 578.204 577.799	BETA 01 00 01 01 01 00 00	.03 1.14 2.28 3.45 4.59 5.77 6.95 8.09	CL 1024 2043 3046 4083 5055 6121 7115 7496	.0165 .0183 .0214 .0263 .0330 .0442 .0646	CPM 0497 0471 0448 0397 0339 0306 0187	.0011 .0010 .0012 .0020 .0018 .0014 .0005	.0005 .0006 .0005 .0005 .0005 .0002 .0000	L/O 6.206 11.164 14.234 15.525 15.318 13.848 11.014 8.547	CDB .0048 .0049 .0049 .0048 .0048 .0048 .0047	P8-1 8.6069 8.4352 9.2935 9.5632 11.1571 13.4620 33.9613 56.2752
716 717 718 719 720 721 722 723 724	MAUH • 754 • 753 • 753 • 754 • 755 • 755 • 755 • 755 • 755	576.339 575.846 575.372 576.427 577.049 577.867 578.204 577.779 577.534	BETA010001010100000	.03 1.14 2.28 3.45 4.59 5.77 6.95 8.09 9.18	CL 1024 2043 3046 4083 5055 6121 7115 7496 7833	CU .0165 .0183 .0214 .0263 .0330 .0442 .0646 .0877 .1130	CPM 0497 0471 0448 0397 0339 0306 0187 .0178	.0011 .0010 .0012 .0020 .0018 .0014 .0005 0002	.0005 .0006 .0005 .0005 .0005 .0002 .0000 .0003	6.206 11.164 14.234 15.525 15.318 13.848 11.014 8.547 6.932	CDB .0048 .0049 .0048 .0048 .0048 .0048 .0047 .0047	P8-1 8.6069 8.4352 9.2935 9.5632 11.1571 13.4620 33.9613 56.2752 74.7884
716 717 718 719 720 721 722 723 724 725	MACH - 754 - 753 - 754 - 754 - 755 - 755 - 755 - 757	576.339 575.816 575.372 576.427 577.049 577.807 578.204 577.749 577.544 579.505	BETA010001010100000	.03 1.14 2.28 3.45 4.59 5.77 6.95 8.09 9.18 10.25	CL 1024 2043 3046 4083 5055 6121 7115 7446 7833 8009	CU .0165 .0183 .0214 .0263 .0330 .0442 .0646 .0877 .1130 .1379	CPM 0497 0471 0448 0397 0339 0306 0187 .0178 .0496 .0756	.0011 .0010 .0012 .0020 .0018 .0014 .0005 0002 .0028	.0005 .0006 .0005 .0005 .0005 .0002 .0000 .0003	L/O 6.206 11.164 14.234 15.525 15.318 13.848 11.014 8.547 6.932 5.808	CDB .0048 .0049 .0048 .0048 .0048 .0047 .0047 .0046	P8-1 8.6069 8.4352 9.2935 9.5632 11.1571 13.4620 33.9613 56.2752 74.7884 92.8112
716 717 718 719 720 721 722 723 724 725 720	MACH - 754 - 753 - 753 - 754 - 755 - 755 - 755 - 757 - 757	576.339 575.816 575.372 576.427 577.049 577.807 578.204 577.799 577.534 579.505	BETA010001010100000	.03 1.14 2.28 3.45 4.59 5.77 6.95 8.09 9.18 10.25 11.35	CL 1024 2043 3046 4083 5055 6121 7115 7496 7833 8009 8143	CU .0165 .0183 .0214 .0263 .0330 .0442 .0646 .0877 .1130 .1379	CPM 0497 0471 0448 0397 0339 0306 0187 .0178 .0496 .0756	.0011 .0010 .0012 .0020 .0018 .0014 .0005 0002 .0028	.0005 .0006 .0005 .0005 .0005 .0002 .0000 .0003 .0003	6.206 11.164 14.234 15.525 15.318 13.848 11.014 8.547 6.932 5.808 5.008	CDB .0048 .0049 .0048 .0048 .0048 .0047 .0047 .0046 .0046	P8-1 8.6069 8.4352 9.2935 9.5632 11.1571 13.4620 33.9613 56.2752 74.7884 92.8112 106.4827
716 717 718 719 720 721 722 723 724 725 720	MACH - 704 - 703 - 704 - 754 - 705 - 700 - 700 - 705 - 707 - 704 - 705 - 707 - 707 - 707 - 707 - 707 - 707 - 707 - 707 - 707 - 708 -	576.339 575.816 575.372 576.427 577.049 577.867 578.204 577.799 577.564 579.505 570.053 571.484	BET A010001010000000	.03 1.14 2.28 3.45 4.59 5.77 6.95 8.09 9.18 10.25 11.35 12.43	CL 1024 2043 3046 4083 5055 6121 7115 7496 7833 8009 8143 8291	CU .0165 .0183 .0214 .0263 .0330 .0442 .0646 .0877 .1130 .1379 .1626 .1859	CPM 0497 0471 0448 0397 0339 0306 0187 .0178 .0496 .0756 .0974 1123	.0011 .0010 .0012 .0020 .0018 .0014 .0005 0002 .0028 .0018	.0005 .0006 .0005 .0005 .0005 .0002 .0003 .0003 .0003 .0003	6.206 11.164 14.234 15.525 15.318 13.848 11.014 8.547 6.932 5.808 5.008 4.460	CDB .0048 .0049 .0048 .0048 .0048 .0047 .0047 .0046 .0045	P8-1 8.6069 8.4352 9.2935 9.5632 11.1571 13.4620 33.9613 56.2752 74.7884 92.8112 106.4827 93.9770
716 717 718 719 720 721 722 723 724 725 726 727	MACH -754 -753 -754 -754 -755 -755 -755 -755 -757 -756 -757 -756	576.339 575.816 575.372 576.427 577.049 577.867 578.204 577.779 577.564 579.505 570.653 570.653	BET A010001010000000	.03 1.14 2.28 3.45 4.59 5.77 6.95 8.09 9.18 10.25 11.35 12.43 13.58	CL 1024 2043 3046 4083 5055 6121 7115 7496 7833 8009 8143 8291 8528	CU .0165 .0183 .0214 .0263 .0330 .0442 .0646 .0877 .1130 .1379 .1626 .1859 .2124	CPM 0497 0471 0448 0397 0339 0187 .0178 .0496 .0756 .0974 -1123	.0011 .0010 .0012 .0020 .0018 .0014 .0005 0002 .0028 .0018 .0024 .0012	.0005 .0006 .0005 .0005 .0005 .0002 .0000 .0003 .0003 .0003 .0002	6.206 11.164 14.234 15.525 15.318 13.848 11.014 8.547 6.932 5.808 5.008 4.460 4.015	CDB .0048 .0049 .0048 .0048 .0048 .0047 .0047 .0046 .0046 .0045	P8-1 8.6069 8.4352 9.2935 9.5632 11.1571 13.4620 33.9613 56.2752 74.7884 92.8112 106.4827 93.9770
716 717 718 719 720 721 722 723 724 725 720 727 727 728	MACH - 754 - 753 - 754 - 755 - 755 - 755 - 755 - 757 - 756 - 757 - 756 - 757 - 756 - 757 - 756 - 757	576.339 575.816 575.372 576.427 577.049 577.867 578.204 577.799 577.564 579.505 570.053 577.484 578.561 580.136	BET A010101010100000	.03 1.14 2.28 3.45 4.59 5.77 6.95 9.18 10.25 11.35 12.43 13.58	CL 1024 2043 3046 4083 5055 6121 7115 7496 7833 8009 8143 8291 8528 8946	CU .0165 .0183 .0214 .0263 .0330 .0442 .0646 .0877 .1130 .1379 .1626 .1859 .2124 .2631	CPM 0497 0471 0448 0397 0339 0306 0187 .0178 .0496 .0756 .0974 1123 .1261 1467	.0011 .0010 .0012 .0020 .0018 .0014 .0005 -0002 .0028 .0018 .0024 .0012	.0005 .0006 .0005 .0005 .0005 .0002 .0000 .0003 .0003 .0003 .0002 .0002	6.206 6.206 11.164 14.234 15.525 15.318 13.848 11.014 8.547 6.932 5.808 5.008 4.460 4.015 3.400	CDB .0048 .0049 .0048 .0048 .0048 .0047 .0047 .0046 .0045 .0045 .0045	P8-1 8.6069 8.4352 9.2935 9.5632 11.1571 13.4620 33.9613 56.2752 74.7884 92.8112 106.4827 93.9770 90.6666 79.8161
716 717 718 719 720 721 722 723 724 725 726 727 728 729 730	MACH - 754 - 753 - 754 - 755 - 755 - 755 - 755 - 755 - 757 - 757 - 757 - 757 - 757 - 757 - 757	576.339 575.816 575.372 576.427 577.049 577.867 578.204 577.799 577.564 579.505 570.053 577.484 578.507 580.136	BET A010101010000000	.03 1.14 2.28 3.45 4.59 5.77 6.95 8.09 9.18 10.25 11.35 12.43 13.58 13.58	CL 1024 2043 3046 4083 5055 6121 7115 7496 7833 8009 8143 8291 8528 8946	CU .0165 .0183 .0214 .0263 .0330 .0442 .0646 .0877 .11379 .1626 .1859 .2124 .2631 .3143	CPM 0497 0471 0448 0397 0339 0306 0187 .0178 .0496 .0756 .0974 .1123 .1261 .1467 .1539	.0011 .0010 .0012 .0020 .0018 .0014 .0005 0002 .0028 .0018 .0024 .0012 .0008	.0005 .0006 .0005 .0005 .0005 .0002 .0000 .0003 .0003 .0002 .0002 .0002	6.206 6.206 11.164 14.234 15.525 15.318 13.848 11.014 8.547 6.932 5.808 5.008 4.460 4.015 3.400 2.977	CDB .0048 .0049 .0048 .0048 .0048 .0047 .0047 .0046 .0045 .0045 .0045	P8-1 8.6069 8.4352 9.2935 9.5632 11.1571 13.4620 33.9613 56.2752 74.7884 92.8112 106.4827 93.9770 90.6666 79.8161 82.9425
716 717 718 719 720 721 722 723 724 725 726 727 728 729 730 731	MACH - 704 - 703 - 703 - 704 - 755 - 700 -	576.339 575.816 575.372 576.427 577.049 577.807 578.204 577.799 577.564 579.505 570.653 571.484 578.567 580.136	BET A010001010000000	.03 1.14 2.28 3.45 4.59 5.77 6.95 8.09 9.18 10.25 11.35 12.43 13.58 15.81 17.93 20.02	CL 1024 2043 3046 4083 5055 6121 7115 7496 7833 8009 8143 8291 8528 8946 9356	CU .0165 .0183 .0214 .0263 .0330 .0442 .0646 .0877 .1130 .1379 .1626 .1859 .2124 .2631 .3143	CPM 0497 0471 0448 0397 0339 0306 0187 .0178 .0496 .0756 .0974 .1123 .1261 .1467 .1539	.0011 .0010 .0012 .0020 .0018 .0014 .0005 0002 .0028 .0018 .0024 .0012 .0008 .0007	.0005 .0006 .0005 .0005 .0005 .0002 .0003 .0003 .0003 .0002 .0002 .0002	6.206 11.164 14.234 15.525 15.318 13.848 11.014 8.547 6.932 5.808 5.008 4.460 4.015 3.400 2.977 2.646	CDB .0048 .0049 .0048 .0048 .0047 .0047 .0046 .0045 .0045 .0045 .0043 .0041	P8-1 8.6069 8.4352 9.2935 9.5632 11.1571 13.4620 33.9613 56.2752 74.7884 92.8112 106.4827 93.9770 90.6666 79.8161 82.9425 91.2184
716 717 718 719 720 721 722 723 724 725 726 727 728 729 730	MACH - 754 - 753 - 754 - 755 - 755 - 755 - 755 - 755 - 757 - 757 - 757 - 757 - 757 - 757 - 757	576.339 575.816 575.372 576.427 577.049 577.867 578.204 577.799 577.564 579.505 570.053 577.484 578.507 580.136	BET A010101010000000	.03 1.14 2.28 3.45 4.59 5.77 6.95 8.09 9.18 10.25 11.35 12.43 13.58 13.58	CL 1024 2043 3046 4083 5055 6121 7115 7496 7833 8009 8143 8291 8528 8946	CU .0165 .0183 .0214 .0263 .0330 .0442 .0646 .0877 .11379 .1626 .1859 .2124 .2631 .3143	CPM 0497 0471 0448 0397 0339 0306 0187 .0178 .0496 .0756 .0974 .1123 .1261 .1467 .1539	.0011 .0010 .0012 .0020 .0018 .0014 .0005 0002 .0028 .0018 .0024 .0012 .0008	.0005 .0006 .0005 .0005 .0005 .0002 .0000 .0003 .0003 .0002 .0002 .0002	6.206 6.206 11.164 14.234 15.525 15.318 13.848 11.014 8.547 6.932 5.808 5.008 4.460 4.015 3.400 2.977	CDB .0048 .0049 .0048 .0048 .0048 .0047 .0047 .0046 .0045 .0045 .0045	P8-1 8.6069 8.4352 9.2935 9.5632 11.1571 13.4620 33.9613 56.2752 74.7884 92.8112 106.4827 93.9770 90.6666 79.8161 82.9425

	TEST= 7	78 RUN=	19									
						BODY AXI	S COEFFICIENT	S			PRESS.COE	
POINT	MACH	۵	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
747	.701	523.700	00	• 05	•0994	.0165	.0012	.0006	0002			0.0000
748	.702	524.803	00	1.10	-1914	.0147	.0011	.0006	0007		00/16	0.000
749	.701	523.789	00	2.23	.2926	•0097	.0006	.0006	.0005		00/16	0.0000
750	•702	524.098	00	3.38	.3877	.0026	.0016	.0006	0008		.0046	0.0000
751	.702	524.275	00	4.49	.4732	<del>-10060</del> 00	.0016	.0006	0001		.0046	0.0000
752	.702	524.383	00	5.61	•5673	0164	.0014	.0007	0005		<b>.</b> 0046	0.0000
753	.702	524.594	01	6.78	.6576	0206	•0029	.0014	0012		.0045	0.000
754	.702	524.342	01	7.90	.7148	0173	.0042	.0016	0020		.0045	0.0000
755	.704	520.700	01	9.03	.7546	0116	.0048	.0014	0024		•0045	0.0000
	.703	525.159	00	10.08	.7762	0040	.0024	.0007	0010		.0044	0.0000
756 757	.703	525.481	00	11.22	.8119	0013	.0018	.0007	0012		.0044	0.0000
	.704	526.194	00	12.31	.8449		.0015	•0006	0016			0.0000
758 750			00	13.41	-8645	.0011	.0013	.0005	0006			0.0000
759	.702	524.225		15.63	.9188	•0035	.0008	.0005	0010			0.0000
760	.704	526.007	00	17.77	.9676	.0073	.0007	•0006	0014		•0042	0.0000
761	.705	527.297	00		1.0442	•0093	•0007	•0009	0019		•0039	0.0000
762	-704	526.648	00	19.88		.0119	.0003	•0006	0031		•0034	0.0000
763	.705	527.451	00	21.93	1.1020	.0113 .0151	.0009	•0006	.0001			0.0000
764	.701	523.053	00	02	•0948		.0018	-0006	0007			0.0000
765	•699	520.944	00	02	•0982	.0154	.0018	•0000	0007	•	0034	0.0000
	1ESI= 7	78 KUN=	19							CT LO	22566 605	c.e.
						ILITY AXIS C					.PRESS.COE	
POINT	MACH	Ų	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
747	.701	523.706	00	•05	• 0994	.0166	0483	.0012	.0006	5.988	.0046	7.7732
748	.702	524.803	00	1.10	.1911	.0183	0444	.0011	.0006	10.443	.0046	7.2092
749	.701	523.789	00	2.23	. 2920	.0211	0405	1000	• 0005	13.839	•0046	7.4299
750	.702	524.098	00	3.38	. 3869	.0254	0355	.0016	.0005	15.232	.0046	7.3563
75 L	. 702	524.275	00	4.49	• 4723	•0310	0293	.0017	.0005	15.235	•0046	7.8712
752	.702	524.383	00	5.61	• 5664	.0391	0221	.0014	-0006	14.486	•0046	9.0728
753	.702	524.594	01	6.78	<ul><li>6550</li></ul>	•0573	0129	.0030	.0011	11.442	•0045	22.9269
754	•702	524.342	01	7.90	•7107	.0811	.0161	.0043	.0010	8.763	•0045	62.6506
755	.704	526.706	01	9.03	• 7474	.1069	•0448	.0049	-0007	6.992	.0044	67.3096
756	.733	525.159	00	10.08	.7653	.1320	.0779	•0025	.0003	5 <b>.7</b> 98	•0043	85.0872
757	د70.	525.481	00	11.22	.7971	.1566	•0983	.0019	-0003	5.090	.0043	90.8496
758	. 704	526.194	00	12.31	<ul><li>8257</li></ul>	.1812	.1168	.0016	.0002	4.557	.0042	89.3783
759	.702	524.225	00	13.41	.8407	.2039	.1323	.0014	•0002	4.123	.0042	84.3516
760	.704	526.007	00	15.63	.8834	.2545	.1537	.0009	.0002	3.471	.0040	78.5892
761	.705	527.297	00	17.77	•9193	•3040	.1634	•000B	.0004	3.024	•0038	77.4857
762	.704	526.648	00	19.88	•9785	.3662	• 1633	.0011	•0005	2.672	•0032	86.1906
763	.705	527.451	00	21.93	1.0186	.4221	.1665	-0006	• 0005	2.413 6.305	•0025	94.1599
764	.701	523.053	00	02	.0949	.0150 .0154	0481 0487	.0009 .0018	.0006 .0006	6.305 6.372	.0046 .0046	7.2827 7.2827

TEST= 778 RUN= 19

TEST= 778 RUN= 20

	TEST= 77	78 RUN≃ 2	0									
						BODY AX	IS COEFFICIENT	rs -		80	DY PRESS.COEF	=
POINT	MACH	Ú	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
779	.495	306.392	00	•03	.0848	.0168	.0009	.0007	.0000			.0000
780	•498	309.315	00	1.09	.1701	.0151	-0012	.0006	0008		•0041 O	.0000
781	.497	308.785	00	2.09	•2522	.0113	•0009	.0005	0011		-0041 0	.0000
782	•498	309.497	00	3.18	.3374	•0053	.0012	.0006	0018		-0041 0	.0000
783	.498	309.701	00	4-17	.4114	0020	.0012	.0004	.0000		-0047 0	.0000
784	.498	309.856	00	5.28	•4894	0120	.0014	.0006	0007		,0041 <b>0</b>	.0000
785	-498	309.159	00	6.37	•5723	0230	.0014	.0009	0013		.0041 0	•0000
786	•497	308.760	00	7.45	•6472	0292	.0018	.0022	0046		.0040 0	•0000
787	•497	308.867	00	8.55	.7108	0235	.0030	.0014	0042		.0040 0	•0000
788	-497	308.355	00	9.61	•7517	0171	•0028	.0011	0028		.0039	•0000
789	-497	308.992	00	10.72	.7861	0125	•0022	.0007	0032		.0038	.0000
790	.497	308.502	00	11.80	.8198	0094	.0019	.0004	0014		.0038	.0000
791	•500	311.689	.00	12.91	.8543	0064	.0011	.0002	0015		.0038	•0000
792	.498	309.435	.00	15.13	.9210	0015	.0008	.0004	0024		.0036 <b>0</b>	•0000
793	499	310.101	00	17.22	.9761	.0018	.0005	.0003	0006		0034 0	• 0000
794	.499	310.864	00	19.27	1.0269	.0018	.0003	.0003	0010		.0032	•0000
795	-498	309.058	00	21.28	1.0786	.0043	0001	.0006	0007		.0032 .0026 0	•0000
796	•497	308.779	00	02	.0880	.0173	.0009	.0005	.0000		.0041 0	.0000
						*0T12					*00-1T	
	TEST= 7	78 RUN=	20									
							COEFFICIENTS				AB.PRESS.COEF	
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	COB.	PB-1
779	•495	306.392	00	.03	• 0848	.0168	0434	.0009	• 0007	5.048	.0041	4.4994
780	•498	309.315	00	1.09	• 1697	•0183	0390	.0012	• 0006	9.273	.0041	4.5485
781	.497	308.785	00	2.09	• 2517	.0204	0341	.0009	•0005	12.338	.0041	4.5117
782	•498	309.497	00	3.18	•3367	.0240	0287	.0012	• 0006	14.029	.0041	4.3400
783	•498	309.761	00	4.17	<b>.</b> 4106	.0278	0233	.0012	.0003	14.770	.0041	4.0703
784	•498	309-856	00	5.28	• <b>4</b> 886	•0330	0175	.0014	.0005	14.806	.0040	4.2665
785	•498	309.159	00	6.37	•5715	.0406	0100	.0015	.0007	14.076	.0040	4.3891
786	•497	308.760	00	7.45	•6457	.0549	0020	.0021	.0020	11.761	•0040	10.3724
787	-497	308.867	00	8.55	• 7066	.0824	•0223	.0031	•0009	8.575	•0039	39.7850
788	•497	308.355	00	9.61	<b>.</b> 7443	.1087	• 0547	.0029	-0006	6.847	•0039	56.3978
789	•497	308.992	00	10.72	•7750	.1340	•0851	.0023	• 0003	5.784	•0038	67.4322
790	•497	308.562	00	11.80	.8047	.1584	.1087	.0019	0000	5.080	•0037	68.4130
791	•500	311.689	•00	12.91	<ul><li>8345</li></ul>	.1846	•1281	.0011	0000	4.521	•0037	74.0528
792	•498	309.435	.00	15.13	. 8899	•2389	<ul><li>1593</li></ul>	.0009	•0002	3.725	•0035	75.4015
793	•499	310.101	00	17.22	•9323	•2907	.1795	.0006	-0001	3.207	•0033	69.7617
794	.499	310.864	00	19.27	• 9686	•3430	.1928	.0004	.0002	2.824	•0030	66.9418
795	-498	309.058	00	21.28	1.0029	.3981	.1883	.0001	.0006	2.519	.0024	71.1103
796	•497	308.779	00	02	.0880	.0173	0439	.0009	•0005	5.087	.0041	4.5975

	TEST= 7	78 RUN=	21									
						BODY AXI	IS COEFFICIEN	ITS		BOD	Y PRESS.CO	EFF
TAIDS	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
810	-292	118.610	00	00	.0603	.0165	.0006	.0006	.0004		•0038	0.0000
811	-293	119.382	00	1.01	.1376	.0147	.0012	•0004	0007		.0038	0.0000
812	•292	119.286	00	2.00	•2151	.0116	.0014	.0006	0012		.0038	0.0000
813	•293	119.860	00	3.02	•3008	.0065	.0015	•0004	0019		.0038	0.0000
814	.294	120.543	00	4.03	•3600	.0006	.0019	.0006	0027		.0038	0.0000
815	. 243	114-864	•00	5.06	•435l	0090	.0015	•0004	0027		.0039	0.0000
816	• 243	119.678	•00	6.11	•5125	0186	.0014	.0006	0033		.0039	0.0000
817	•273	119.778	00	7.12	•5789	0304	.0014	.0012	0038		.0037	0.0000
818	•243	119.791	00	8.19	•6544	0373	•0002	.0027	0094			0.0000
819	.292	119.147	00	9.26	.7190	0343	.0057	•0040	0149		.0037 .0037	0.0000
820	•292	119.080	00	10.31	.7587	0317	.0086	-0041	0123		<b>.</b> 0036	0.0000
821	-291	118.437	00	11.42	.8013	0294	•0086	.0034	0132		<b>.</b> 0036	0.0000
822	• 29 L	118.476	•00	12.54	.8380	0240	.0068	.0018	0125		•0035	0.0000
823	•291	118.464	.00	14.67	•9074	0108	.0010	.0001	0090		.0034	0.0000
824	•292	119.116	.00	16.72	.9563	0058	.0008	0001	0097		.0031	0.0000
825	-243	119.781	•00	18.480	1.0320	0022	.0007	.0002	0048		.0031	0.0000
826		119.074	.00	20.83	1.0603	0010 0387	.0007	•0003	0050		.0026	0.0000
827	• 292	118.727	•00	8.21	.6416	0387	•0002	•0026	0153		•0037	0.0000
	TEST= 1	78 KUN=	21									
					STAB	ILITY AXIS C	DEFFICIENTS			STA	B.PRESS.CO	EFF
POINT	MACH	ú	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
810	.292	118.610	00	00	.0603	.0165	0460	.0006	•0006	3.655	.0038	1.8267
811	-293	119.382	00	1.01	.1373	.0171	0376	.0012	.0003	8.029	•0038	1.8145
812	.292	119.286	00	2.00	-2145	•0191	0365	.0014	• 0005	11.230	.0038	2.1823
813	.293	119.866	00	3.02	.3000	.0223	0306	.0016	.0003	13.457	•0038	1.8022
814	. 294	120.543	00	4.03	. 3652	<b>.</b> 0263	0235	.0020	.0004	13.886	•0038	2.1455
815	.243	119.869	.00	5.06	• 4342	.0294	0202	.0015	.0002	14.772	•0038	1.6919
816	- 293	119.678	•00	6.11	.5117	.0361	0122	.0015	•0005	14.175	•0038	1-6061
817	<b>.</b> 293	119.778	00	7.12	•5782	0415	0053	.0015	.0011	13.923	•0037	2.2558
818	د 29 •	119.791	00	8.19	•6532	•0563	.0026	.0006	•0026	11.602	•0037	7.4909
819	-292	119.147	00	9.26	.7154	.0817	.0157	.0063	.0030	8.756	•0037	20.4749
8∠0	-292	119.080	00	10.31	• 7524	.1046	.0438	•0092	•0025	7.193	•0035	28.2602
821	- 291	118.437	00	11.42	.7915	.1299	•0686	.0091	.0016	6.093	.0035	34.2678
822	- 291	118.476	•00	12.54	. 8236	-1584	•0965	.0071	•0003	5.199	.0034	40.0302
823	- 291	118.464	•00	14.67	.8809	.2193	•1450	.0010	0001	4.017	.0032	39.8463
824	- 292	119.110	•00	16.72	.9178	.2697	.1699	•0007	0004	3.403	•0030	36.9651
825	.293	119.781		18.80	•9 <b>7</b> 80	•3304	.1977	.0008	0000	2.960	.0028	33.5935
826	Acc. 1		r.c.	20 02	0017	07/2	1040	0000	0000	- (		22 7771
827	•292 •292	119.074	•00 •00	20.83 8.21	.9917 .6405	.3761 .0533	.2048 0030	.0008 .0006	.0000 .0025	2.637 12.023	.0036 .0037	33.7774 7.7115

						BODY AXI	S COEFFICIEN	TS		BUDY PRESS.	COEFF
TAIDS	MACH	ú	BETA	ALPHA	CNF	CAF	<b>C</b> LB	CNB	CSF	CAB	CAC
848	.807	626.795	00	.21	.1248	.0140	.001B	.0006	•0006	.0051	0.0000
849	•8J7	627.301	01	1.30	.2442	.0116	.0018	.0006	.0012	.0051	0.0000
850	.806	625.813	00	2.56	.3556	•0060	.0020	.0006	•0004	•0050	0.0000
851	.80s	627.914	01	3.69	.4612	0021	•0026	.0006	.0005	•0050	0.0000
852	.804	024.611	00	4.81	.5575	0103	.0020	.0002	.0004	•0050	0.0000
853	• 808	627.813	00	6.00	.6802	0146	0002	0002	.0016	.0049	0.0000
855	.830	626.056	01	8.26	.7837	0101	.0044	.0008	0001	•0048	0.0000
854	-879	627.635	00	7.15	.7466	0132	0009	.0001	.0011	.0049	0.0000
856	.807	627.383	01	9.35	.8208	0054	.0062	.0008	.0009	.0048	0.0000
857	.809	628.807	00	10.44	.8342	.0010	•0029	.0004	•0008	.0048	0.0000
858	. 808	628.310	00	11.53	.8418	•0044	•0009	.0003	•0009	.0047	0.0000
859	.810	621.714	00	12.58	.8614	•0080	•0012	.0004	•0002	.0047	0.0000
860	-810	629.468	00	13.73	.8882	•0102	•0009	.0004	-0000	.0047	0.0000
861	•898	628.828	00	14.81	.9119	.0085	•0006	.0005	0001	.0046	0.0000
862	.810	030.143	00	15.97	.9477	.0113	.0007	.0006	0006	•0045	0.0000
863	.811	030.835	00	18.13	1.0189	.0121	•0006	.0006	0011	.0041	0.0000
864	.812	631-143	.00	20.23	1.0832	-0124	•0005	.0006	0035	.0035	0.0000
865	.806	625.828	00	.07	.1289	•0122	.0021	.0006	-0004	•0050	0.0000
866	•900	625.904	01	•07	.1303	.0121	•0016	.0006	.0008	.0050	0.000
	TEST=	778 RUN=	22		STAB	ILITY AXIS (	CUEFFICIENTS			STAB.PRESS	.COEFF

	TEST= 7	78 RUN=	22									
					STAB	ILITY AXIS	CUEFFICIENTS			STAB.	.PRESS.COEF	F
POINT	MACH	O)	BETA	ALPHA	CL	CO	CPM	CLS	CNS	L/D	CDB	PB-1
848	• 8J7	526.795	00	.21	. 1248	.0145	0587	.0018	.0005	8 <b>.60</b> 7	•0051	9.3180
849	. 807	627.301	01	1.36	. 2439	.0174	0579	.0018	•0006	14.017	.0050	10.3233
850	.806	625.813	00	2.56	•3550	.0219	0550	.0021	•0005	16.210	.0050	11-7210
851	.808	627.974	01	3.69	• 4605	.0276	0508	.0026	.0004	16.685	.0050	16.4045
852	.804	024.611	00	4.81	•5566	•0366	0446	.0020	.0001	15.208	.0049	16.5517
853	.808	627.813	00	6.00	.6783	.0566	0430	0002	0002	16.984	.0049	26.4825
855	•8U6	620.050	01	8.26	.7774	.1025	.0202	.0045	.0001	7.584	.0048	176.3060
854	• 80 s	027.635	00	7.15	.7428	.0798	0133	0008	.0002	9.308	.0048	60.9342
856	.807	027.383	01	9.35	.8113	.1280	.0421	.0062	0002	6.338	•0048	249.7471
857	.809	628.807	00	10.44	.8207	.1520	.0680	.0029	0002	5.399	.0047	218-1149
858	808 <b>.</b>	628.316	00	11.53	- 8245	.1725	.0878	.0010	.0001	4.780	.0046	130.9425
859	.810	624.714	00	12.58	-8395	1955	.1010	.0013	.0001	4.294	•0046	105-1954
860	.810	624.468	00	13.73	.8610	•2206	.1124	.0010	.0002	3.903	•0045	101.8850
861	.809	628.828	00	14.81	.8794	.1235	.1235	.0007	.0004	3.645	•0046	95.2643
862	.810	030.143	00	15.97	• 9087	.2716	.1326	.0008	-0004	3.346	.0043	90.1149
863	.811	630.835	00	18.13	·9651	-3285	.1403	.0008	.0004	2.938	.0039	93.0574
864	.812	631.143	.00	20.23	1.0121	. 3861	.1367	.0007	.0004	2.621	•0035	107.9540
865	.806	625.828	00	.07	.1289	.0124	0591	.0021	.0006	10.416	•0050	9.4406
866	.800	625.904	01	.07	.1303	.0123	0582	.0016	.0006	10.587	•0050	9-4406

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

BODY AXIS COEFFICIENTS

BODY PRESS.COEFF

	•						IS COEFFICIEN	115		800	Y PRESS.COE	FF
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
883	.753	575.300	00	02	-1176	.0143	.0018	.0005	0006			0.0000
884	•754	575.821	00	1.13	.2255	.0118	.0017	.0006	0010		.0048	0.0000
885	.754	575.825	00	2.30	.3253	.0067	.0014	.0006	0001		.0049	0.0000
886	•753	574.946	00	3.43	-4165	0004	.0023	.0006	0004		.0048	0.0000
887	•755	576.701	00	4.58	.5169	0093	.0019	.0005	0006		•0048	0.0000
888	.753	574.748	00	5.76	<b>.</b> 6088	0187	.0016	•0003	.0003		•0048	0.0000
889	.753	574.932	00	6.94	.7097	0224	.0003	0001	.0007		.0047	0.0000
890	•755	576.794	00	8.06	.7606	0184	.0013	.0004	0002		.0047	0.0000
891	.755	577.030	00	9.19	• 1967	0131	.0040	.0008	0011		.0046	0.0000
892	.755	576.906	00	10.25	.8190	0068	•0025	.0004	0006			0.0000
893	-756	578.128	00	11.35	.8296	0	.0017	.0005	0005			0.0000
894	.755	577.625	00	12.44	-8571	.0034	.0011	.0004	0005		.0045	0.0000
895	.756	578.562	00	13.58	.8809	.0066	.0012	•0003	0011		•0045	0.0000
896	.756	578.499	00	15.82	•9288	.0088	.0007	•0005	0014			0.0000
897	.757	579.504	00	17.97	•9999	.0106	.0008	•0003	0008			0.0000
898	.759	581.210	•00	20.06	1.0555	.0127	.0010	.0005	0025			0.0000
899	9 خ7 •	580.843	•00	22.15	1.1273	.01.08	0000	.0007	0058			0.0000
900	.755	577.234	00	•04	.1190	.0128	.0016	•0005	0004		.0048	0.0000
	TEST= 7	18 RUN=	23			ILLIN AVIC	COEFFICIENTS			CTA	B.PRESS.COE	E <b>C</b>
			05.74	4 : D 4		CD CD	CPM	CLS	CNS	L/D	CDB	P8-1
POINT	MACH	Q	BETA	ALPHA	CL N. 7		0552	.0018	•0005			7.6015
883	.753	575.300	00	02	.1176	.0143	0525	.0018	•0006	8.224	•0048	8.1655
884	.754	575.821	00	1.13	•2253	.0163		.0014	•0005	13.822	•0048	8.6559
885	• 754	575.825	00	2.30	• 3249	•0198	0493 0386	.0023	.0004	16.409	•0049	9.8574
886	.753	574.946	00	3.43	•4159	.0246	0336	.0019	.0004	16.907 16.128	.0048 .0048	11.6720
887	.755	576.701	00	4.58	•5161 •6078	.0320	0280	.0017	.0001			13.7808
888	•753	574.748 574.932	00 00	5.76 6.94	• 7076	.0425 .0635	0154	.0003	0001	14.301 11.143	.0047 .0047	34.3904
889	•753	3/4-932			• 10.10	*0635				11.143	•0047	3703707
890											oolié	56.8883
	.755	576.794	00	8.06	.7561	.0884	.0184	.0014	.0002	8.553	•0046	56.8883 79.0796
891	.755 .755	576.794 577.030	00 00	8.06 9.19	.7561 .7891	.0884 .1142	.0184 .0481	.0014 .0040	.0002 .0001	8.553 6.910	.0046	79.0796
892	.755 .755 .755	576.794 577.030 576.906	00 00 00	8.06 9.19 10.25	.7561 .7891 .8077	.0884 .1142 .1390	.0184 .0481 .0727	.0014 .0040 .0026	.0002 .0001 0001	8.553 6.910 5.811	.0046 .0045	79.0796 96.1215
892 893	.755 .755 .755 .756	576.794 577.030 576.906 578.128	00 00 00	8.06 9.19 10.25 11.35	.7561 .7891 .8077 .8139	.0884 .1142 .1390 .1632	.0184 .0481 .0727 .0967	.0014 .0040 .0026 .0017	.0002 .0001 0001 .0001	8.553 6.910 5.811 4.987	.0046 .0045 .0044	79.0796 96.1215 92.9338
892 893 894	.755 .755 .755 .756 .755	576.794 577.030 576.906 578.128 577.625	00 00 00 00	8.06 9.19 10.25 11.35 12.44	.7561 .7891 .8077 .8139 .8368	.0884 .1142 .1390 .1632 .1879	.0184 .0481 .0727 .0967 .1125	.0014 .0040 .0026 .0017	.0002 .0001 0001 .0001	8.553 6.910 5.811 4.987 4.453	.0046 .0045 .0044 .0044	79.0796 96.1215 92.9338 89.3783
892 893 894 895	.755 .755 .755 .756 .755	576.794 577.030 576.906 578.128 577.625 578.562	00 00 00 00 00	8.06 9.19 10.25 11.35 12.44 13.58	.7561 .7891 .8077 .8139 .8368	.0884 .1142 .1390 .1632 .1879	.0184 .0481 .0721 .0967 .1125	.0014 .0040 .0026 .0017 .0011	.0002 .0001 0001 .0001 .0001	8.553 6.910 5.811 4.987 4.453 4.010	.0046 .0045 .0044 .0044	79.0796 96.1215 92.9338 89.3783 93.0574
892 893 894 895 896	.755 .755 .755 .756 .755 .756	576.794 577.030 576.906 578.128 577.625 578.562 578.499	00 00 00 00 00 00	8.06 9.19 10.25 11.35 12.44 13.58 15.82	.7561 .7891 .8077 .8139 .8368 .8553	.0884 .1142 .1390 .1632 .1879 .2133	.0184 .0481 .0727 .0967 .1125 .1257 .1451	.0014 .0040 .0026 .0017 .0011 .0013	.0002 .0001 0001 .0001 .0001 0000	8.553 6.910 5.811 4.987 4.453 4.010 3.406	.0046 .0045 .0044 .0044 .0043	79.0796 96.1215 92.9338 89.3783 93.0574 82.0230
892 893 894 895 896 897	.755 .755 .755 .756 .756 .756 .756 .756	576.794 577.030 576.906 578.128 577.625 578.562 578.499 579.504	00 00 00 00 00 00 00	8.06 9.19 10.25 11.35 12.44 13.58 15.82 17.97	.7561 .7891 .8077 .8139 .8368 .8553 .8918	.0884 .1142 .1390 .1632 .1879 .2133 .2618	.0184 .0481 .0727 .0967 .1125 .1257 .1451 .1541	.0014 .0040 .0026 .0017 .0011 .0013 .0008	.0002 .0001 0001 .0001 0000 .0003	8.553 6.910 5.811 4.987 4.453 4.010 3.406 2.976	.0046 .0045 .0044 .0044 .0043 .0041	79.0796 96.1215 92.9338 89.3783 93.0574 82.0230 81.8391
892 893 894 895 896 897 898	.755 .755 .755 .756 .756 .756 .756 .756	576.794 577.030 576.906 578.128 577.625 578.562 578.499 579.504 581.210	00 00 00 00 00 00 00	8.06 9.19 10.25 11.35 12.44 13.58 15.82 17.97 20.06	.7561 .7891 .8077 .8139 .8368 .8553 .8918	.0884 .1142 .1390 .1632 .1879 .2133 .2618 .3187	.0184 .0481 .0727 .0967 .1125 .1257 .1451 .1541	.0014 .0040 .0026 .0017 .0011 .0013 .0008 .0008	.0002 .0001 0001 .0001 .0000 0000 .0003 .0001	8.553 6.910 5.811 4.987 4.453 4.010 3.406 2.976 2.642	.0046 .0045 .0044 .0044 .0043 .0041 .0039	79.0796 96.1215 92.9338 89.3783 93.0574 82.0230 81.8391 99.3103
892 893 894 895 896 897	.755 .755 .755 .756 .756 .756 .756 .756	576.794 577.030 576.906 578.128 577.625 578.562 578.499 579.504	00 00 00 00 00 00 00	8.06 9.19 10.25 11.35 12.44 13.58 15.82 17.97	.7561 .7891 .8077 .8139 .8368 .8553 .8918	.0884 .1142 .1390 .1632 .1879 .2133 .2618	.0184 .0481 .0727 .0967 .1125 .1257 .1451	.0014 .0040 .0026 .0017 .0011 .0013 .0008	.0002 .0001 0001 .0001 0000 .0003	8.553 6.910 5.811 4.987 4.453 4.010 3.406 2.976	.0046 .0045 .0044 .0044 .0043 .0041	79.0796 96.1215 92.9338 89.3783 93.0574 82.0230 81.8391

TEST= 778 RUN= 23

	TEST= 7	•				BODY AXI	S COEFFICIENT	S		BODY PRESS.	COEFF
POINT	MACH	۵	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
914	.702	524.324	00	•03	.1152	.0144	.0017	.0007	0005	•0046	0.000
915	.702	523.938	00	1.10	.2117	.0122	.0011	•0006	0006	.0046	0.000
916	.701	522.929	00	2.25	.3095	.0075	.0018	•0007	0004	.0046	0.000
917	.701	522.938	00	3.36	.3980	.0008	•0026	•0006	0004	.0046	0.000
918	-702	523.667	00	4.47	•4804	0074	-0018	-0006	0003	•0046	0.000
919	.701	523.152	00	5.61	.5732	<b></b> 0175	.0016	•0007	0008	.0046	0.000
920	.701	523.444	00	6.79	.6634	0218	•0024	.0011	0021	.0045	0.000
921	.702	523.734	00	7.91	.7276	0196	.0015	.0007	0009	.0045	0.000
922	.701	523.380	00	9.01	.7540	0105	0006	•0002	0001	•0044	0.000
923	د 70ء	525.279	00	10.12	.7863	0052	.0041	.0007	0011	.0044	0.000
924	.702	524.507	00	11.22	.8186	0014	.0026	•0005	0019	.0043	0.000
925	.703	524.740	00	12.31	.8474	.0011	.0016	.0004	0003	•0043	0.000
926	.703	525.085	00	13.46	.8785	.0031	.0012	•0004	0005	•0043	0.000
927	.704	526.313	00	15.67	.9292	.0068	-0008	.0005	0010	.0042	0.000
928	•705	527.522	00	17.78	.9783	.0089	.0008	•0006	0015	•0039	0.000
929	.706	528.010	00	19.85	1.0333	.0118	.0012	•0006	0020	•0034	0.000
930	.707	529.005	00	21.96	1.0989	.0108	-0004	•0006	0031	.0027	0.000
931	.702	523.693	01	6.82	.6629	0238	.0023	.0011	0007	•0045	0.000

	TEST= 7	78 RUN= 2	24		CTAG	11 1 T V A V I C	COEFFICIENTS			BATS	.PRESS.COEF	=
					STAB							
POINT	MACH	Q	BETA	ALPHA	CL	€D	CPM	CLS	CNS	L/D	COB	PB-1
914	.702	524.324	00	• 03	.1152	.0145	0535	.0017	.0007	7.945	•0046	7.5154
915	.732	523.938	00	1.10	.2115	.0163	0483	.0011	.0006	12.975	.0046	7.2579
916	.701	522.929	00	2.25	.3090	.0196	0447	.0018	.0006	15.765	.0046	7.2334
917	.701	522.938	00	3.36	• 3974	.0241	0349	•0026	.0005	16.490	•0046	7.7851
918	.702	523.667	00	4-47	•4796	.0300	0272	•0018	.0005	15.987	•0046	8.4594
919	.701	523.152	00	5.61	• 5724	.0386	0209	.0017	.0006	14.829	•0046	8.6923
920	.701	523.444	00	6.79	.6616	.0568	0124	•0025	.0008	11.648	•0045	21.5170
921	.702	523.734	00	7.91	.7237	.0808	•0136	.0016	•0005	8.957	.0045	61.6698
922	.701	523.380	00	9.01	.7467	.1078	.0487	0006	.0003	6.927	•0044	82.3908
923	.703	525.279	00	10.12	•7755	.1330	.0727	.0042	0000	5.831	.0043	98.2069
924	•702	524.507	00	11.22	.8038	.1578	.0967	•0027	.0000	5.094	•0043	102.4368
925	• 703	524.746	00	12.31	• 8282	.1817	•1155	.0016	•0001	4.558	.0042	86.9885
926	.703	525.085	00	13.46	.8542	.2074	•1314	.0013	.0001	4.119	.0042	84.5977
927	-704	526.313	00	15.67	. 8935	•2575	•1525	•0009	.0003	3.470	.0040	80.0000
928	.705	527.522	00	17.78	• 9295	•3073	.1630	•0009	.0003	3.025	•0038	77.4253
929	.706	528.010	00	19.85	• 9685	.3621	•1586	.0013	•0002	2.675	.0032	93.2414
930	.707	529.005	00	21.96	1.0157	.4208	.1640	•0006	-0004	2.414	.0025	95.0804
931	.702	523.693	01	6.82	.6611	.0550	0125	• 0024	-0008	12.018	.0045	21.5170

.

:

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	25			HODY	AVIS COMPETCIEN	T.C		0.00	N DDECC COC	c c
					C.111		AXIS COEFFICIEN			801	DY PRESS.COE	
POINT	MACH	9	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
945	.498	309.310	00	.01	•0998	.0147	.0018	.0007	0007		.0041	0.0000
946	•498	309.930	00	1.07	-1854	.0128	•0022	•0006	0016		.0041	0.0000
947	•498	309.930	00	2.07	-2630	•0089	.0015	•0006	0015		.0041	0.0000
948	•490	310.113	00	3.15	.3411	.0032	.0021	•0006	0026		.0041	0.0000
949	-490	309.941	•00	4.17	.4148	0035	.0010	•0004	0022		.0041	0.0000
950	.499	310.656	•00	5.26	·4954	0132	.0009	•0004	0027		.0041	0.0000
951	•498	310.046	•00	6.34	•5749	0244	•0019	.0008	0041		-0041	0.0000
952	.478	310.088	00	7.42	.6516	0309	.0013	.0019	0042		.0040	0.0000
953	.498	309.657	•00	8.53	•7195	0273	.0009	.0005	0046		.0040	0.0000
954	.497	309.051	•00	9.59	•7730	0229	0042	0010	0010		.0039	0.0000
955	.499	310.415	00	10.70	.7937	0139	•0022	.0007	0033		.0038	0.0000
956	.498	309.807	.00	11.75	.8276	0106	.0016	.0004	0036		.0038	0.0000
957	.497	308.765	00	12.87	.8623	0078	.0011	.0004	0014		.0038	0.0000
958	.497	309.086	•00	15.10	.9259	0024	.0008	.0003	0023		•0036	0.0000
959	•500	312.248	.00	17.20	.9842	.0012	.0004	.0003	0029		.0034	0.0000
960	•499	310.524	•00	19.25	1.0359	•0040	.0007	.0005	0037		.0032	0.0000
961	499	310.675	.00	21.26	1.0848	.0040	•0006	•0006	0037		.0026	0.0000
962	•497	308.603	00	04	.1001	.0154	.0018	.0005	0007		.0041	0.0000
	TES1= 7	78 KUN=	25		STAH	11 TY AXI	S COEFFICIENTS			CT	AB.PRESS.COE	EE
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
945	.498	309.310	00	.01	•0998		0478	•0018	.0007			4.3891
946	•498	309.930	00	1.07	.1852	.0147	0421	•0022	.0006	6.789	-0041	4.6098
947	•498	309.930	00	2.07	. 2626	.0163	0362	.0015	•0005	11.362	-0041	4.3768
948	•498	310.113	00	3.15	. 3404	.0184	0261	.0021	•0005	14.272	.0041	4.7201
949	-498	309.941	•00	4.17	.4141	.0220	0193	•0010	.0003	15.473	.0041	
950	•499	310.656	•00	5.26	•4947	•0266	0141	.0010	•0004	15.568	.0041	4.6711
951	•49t	310.046	.00	6.34	• 5743	.0321	0082	•0020		15.411	•0040	4.6220
952	.498	310.088	00	7.42	• 6503	•0392	.0002	.0015	.0006	14.651	•0040	4.3033
953	•498	309.657	•00	8.53	•7159	•0536			-0017	12.132	.0040	9.7594
954	.497	309.051	•00			.0796	.0181	•0009	.0003	8.994	•0039	31.5705
				9.59	• 7663 7030	•1063	•0424	0043	0003	7.209	•0039	48.3060
955	.499	310-415	00	10.70	.7828	.1336	•0860	•0023	•0003	5.859	•0038	66.3288
956	• 498	309.807	-00	11.75	.8129	.1581	.1095	.0017	.0000	5.142	•0037	67.0644
957	•497	308.765	00	12.87	• 8429	.1845	.1279	.0012	.0001	4.569	•0037	70.8651
958	•497	309.086	•00	15.10	•8951	.2388	.1599	•0009	.0000	3.748	•0035	73.6850
959	.500	312.248	•00	17.20	• 9404	.2922	.1813	.0005	•0002	3.218	•0033	68.6582
960	.499	310.524	•00	19.25	.9772	•3 <sup>4</sup> 53	•1937	.0008	.0002	2.830	•0030	68.2904
961		310.675	•00	21.26	1 0003		1893	0000	0000	-	1	71 2222
962	•499 •497	308.603	00	04	1.0092 .1001	•3993	0465	.0008 .0018	.0003 .0005	2.527	.0024 .0041	71.2329 4.5117

	TEST= 7	78 xUN≃ 2	26									
						BODY AXI	S COEFFICIENT	rs		BODY	PRESS.COE	FF
POINT	MACH	Ų	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
978	.292	119.381	00	•04	.0802	.0146	•0015	•0002	0004		•0038	0.0000
979	. 293	119.478	00	1.02	.1476	.0134	.0016	.0004	0009		.0038	0.0000
980	.293	119.478	00	2.01	.2435	.0096	.0014	.0007	0014		•0038	0.0000
981	.293	119.479	00	3.02	.3113		•0015	•0004	0020		•0038	0.0000
982	.293	120.157	00	4.03	.3763	.0038	•0015	•0006	0025		.0038	0.0000
983	.294	120.160	00	5.04	.4525	0014	.0014	•0006	.0030			0.0000
984	• 294	120.162	00	6.11	•5199	0097	.0021	•0007	.0020		.0039	0.0000
985	.294	120.162	00	7.12	.5866	0198	•0014	.0013	0038		.0039	0.0000
		119.599	00	8.19	•6560	0311	.0013	.0023	0043		•0037	0.0000
986	.293		00	9.26	.7289	0385	•0033	•0023	0043		.0037	0.0000
987	.242	118.353			.7986	0390	•0086	.0038	0126		.0037	0.0000
988	.292	118.894	00	10.39		0334		•0036 •0034	0125		.0036	0.0000
989	-591	118.342	00	11.46	.8120	0314	-0091		0067		.0036	
990	-29L	118-287	00	12.52	.8679	0258	•0068	•0020			.0035	0.0000
991	. 292	119.047	00	14.73	.9118	0123	•0015	•0004	.0027		•0034	0.0000
952	.293	119.799	00	16.79	.9687	0071	•0008	•0002	.0022			0.0000
993	-293	119.882	00	18.80	1.0405	0029	.0011	•0004	.0008		.0030	0.0000
994	. 293	119.959	00		1.0804	•0004	•0006	-0005	.0008		.0026	0.0000
995	.292	118.923	00	8.21	•6496	0393	.0009	•0023	0040		.0037	0.0000
	TEST= 7	78 KUN=	26		натг	. 212A VTIII	COEFFICIENTS			A T Z	B.PRESS.CO	c <b>c</b> c
TALUS	MACH	J.	BETA	ALPHA	CL	C)	CPM	CLS	CNS	L/D	CDB	
978	.292	119.381	00	•04	.0802		0465	•0015	• 0002		.0038	PB-1
979	.293	119.478	00	1.02	.1474	.0146	0485 0425	.0017	• 0003	5.493	.0038	1.7409 1.8390
980	.293	119.478	00	2.01	.2430	.0160				9.213	.0038	
	.293	119.479			.3106	.0181	0318 0277	.0014	•0006	13.425	.0038	1.9493
981	.293	120.157	00 00	3.02	•3755	•0202	0201	.0016 .0015	.0003	15.346 14.960	.0038	1-8880
982 983	•294	120.157	00	4.03 5.04	•4516	.0251			.0005			1.8758
	•294	120-160			• 4910	•0301	0151 0077	.0015 .0021	-0004	15.019	.0038	1.6919
984	•294	120.160	00 00	6.11 7.12	•5859	.0356	0077 0042		.0005	14.581	.0038	1.6919
985 986	•294	119.599	00	8.19	• 5859 • 6550	.0418	-•0042 •0026	.0015 .0017	-0011	14.022	.0037	1.7777
		118.853		9.26	• 7259	•0553			-0021	11.844	.0037	7.3315
987	•292 •292	118.894	00 00	10.39	• 7259 • 7918	.0787	•0132	.0037	•0024	9.224	.0037	15.3011
988		118.894				.1112	.0516	.0092	•0022	7.121	.0035	29.4250
989	- 291	118.342	00	11.46	• 8024	.1305	-0698	.0096	-0015	6.149	.0035	33.4709
990	.291		00	12.52 14.73	.8532	.1629	•1034	.0071	• 0005	5.238	.0034	36.7199
991	-292	119.047 119.799	00		•8854 0300	.2199	•1452	.0015	0000	4.026	.0032	41.0723
992	.293		00	16.79	•9298	•2731	.1743	.0008	0001	3.405	.0030	37.6394
993	.293	119.882	00	18.80	.9864	•3325	•1983 2005	.0012	0000	2.967	.0028	33.8387
994	.293	119.959	00	20.84	1.0100	-3848	-2085	.0007	.0003	2.625	.0024	32.4901
995	•292	118-923	00	8.21	<b>.</b> 6485	.0539	•0050	.0012	.0022	12.025	.0037	7.2579

	TEST= 7	78 RUN= 2	2 <b>7</b>								
						BODY AXI	S COLFFICIENT	rs		BODY PRESS.	COEFF
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	ÇSF	CAB	CAC
10	.932	731.969	01	-15	-1702	.0213	.0020	.0006	.0010	.0064	0.0000
11	.93i	731.520	01	1.38	.2881	.0269	.0011	•0005	.0013	.0064	0.0000
12	.931	731.624	01	2.51	.3794	.0243	.0011	.0006	.0008	.0063	0.0000
13	.933	732.671	01	3.72	<b>.</b> 4848	.0230	.0016	•0005	.0007	•0063	0.0000
14	.933	733.224	01	4.91	<b>.</b> 5751	.0219	.0009	•0005	.0009	.0063	0.0000
15	.934	733.865	01	6.08	•6583	.0202	.0016	.0003	.0018	.0062	0.0000
16	.934	733.924	01	7.30	.7470	.0183	.0030	•0004	.0019	.0062	0.0000
17	.935	734.619	01	8.49	.8212	.0169	.0051	.0007	•0005	.0062	0.0000
18	.939	737.405	01	9.68	.9039	.0163	.0070	.0007	.0014	.0060	0.0000
19	•936	734.948	01	10.85	•9645	.0146	•0120	.0010	.0011	.0058	0.0000

	TEST= 7	78 RUN=	27									
					STA	BILITY AXIS	COEFFICIENTS			STAB	.PRESS.COEF	F
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	P8-1
10	.932	731.969	01	- 15	.1702	.0217	0924	.0020	.0006	7.843	.0064	16.3676
11	.931	731.520	01	1.38	.2875	0309	0946	.0011	•0005	9.304	.0064	29.7315
12	.931	731.624	01	2.51	.3781	.0410	0913	-001i	• 0005	9.222	•0063	37.4555
13	.933	732.671	01	3.72	.4824	.0544	0895	.0017	•0004	8.868	•0063	54.8040
14	.933	733.224	01	4.91	.5713	.0709	0884	.0009	• 0004	8.058	.0063	60.8116
15	.934	733.865	01	6.08	•652 <b>7</b>	•0899	0841	.0016	•0002	7.260	•0062	91.9537
16	.934	733.924	01	7.30	.7390	.1130	0783	.0031	.0001	6.540	.0061	114.5131
17	.935	734.619	01	8.49	.8101	•1379	0705	.005L	0000	5.875	.0061	120.6433
18	-939	737.405	01	9.68	.8888	.1680	0721	.0070	0005	5.290	.0059	155.4631
19	.936	734.948	01	10.85	•9450	-1960	0537	.0120	0013	4.821	•0057	149.5781

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	28									
							S COEFFICIENT				PRESS.COEF	
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	ÇNB	CSF		CAB	CAC
34	-861	675.312	01	05	.1452	•0155	.0017	.0006	.0007		.0055 0	-0000
35	.863	676.704	01	1.15	•2696	.0134	.0020	.0007	.0020		.0054 0	•0000
36	.863	676.745	01	2.33	.3975	.0093	•0016	•0006	.0019			.0000
37	.864	677.383	01	3.56	•5288	•0059	.0015	•0003	.0016			.0000
38	-864	677.802	00	4.72	.6267	و0033	.0029	•0004	.0011			-0000
39	-863	676.909	01	5.88	.7051	•0024 •0005	.0028	.0008	-0004			•0000
40	-865	678.505	01	7.04	<b>.7720</b>		•0028	.0013	0006			•0000
41	.864	677.645	01	8.20	<ul><li>8207</li></ul>	•0006	-0048	.0017	0012			.0000
42	.866	679.285	01	9.31	-8615	.0016	.0066	.0017	0017			•0000
43	.863	676.828	02	10.38	<ul><li>8685</li></ul>	.0023	.0118	•0022	0008			-0000
44	-861	675.065	01	09	.1418	.0139	.0017	.0007	.0007			.0000
	TEST= 7	78 RUN≃	28		STABI	ILITY ÄXIS (	COEFFICIENTS			STAB	.PRESS.COEF	F
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
34	.861	675.312	01	05	•1453	•0154	0653	.0017	.0006	9.435	•0055	11.9417
35	.863	676.704	01	1-15	• 2693	.0188	0672	.0020	.0007	14.324	-0054	15.9877
36	.863	676.745	01	2.33	• 3968	.0254	0707	.0016	.0005	15.622	.0054	17.5325
37	-864	677.383	01	3.56	• 5276	•0387	0798	.0016	-0002	13.633	.0053	19.8618
38	.864	677.802	00	4.72	•6244	0554	0823	.0029	.0001	11.271	•0053	31.3253
39	.863	676-909	01	5.88	<b>.</b> 7014	.0746	0683	.0029	.0005	9.402	•0053	60.0760
40	-865	678.505	01	7.04	<b>.</b> 7665	•0951	0453	.0029	.0009	8.060	.0052	82.7577
41	-864	677.645	01	8 - 20	.8127	1175	0176	.0050	.0010	6.917	•0052	82.3899
42	.866	679.285	01	9.31	•8504	1408	.0072	.0068	.0006	6.040	•0050	84.7194
43	.863	676.828	02	10.38	. 8544	-1587	.0344	.0120	.0000	5.384	.0050	135.6011
44	.861	675.065	01	09	.1419	.0137	0657	.0017	.0007	10.356	.0055	11.9662

	TEST= 7	78 KUN= 2	29			RODY AXI	S COEFFICIEN	115		RODY	PRESS.COEF	F
POINT	MACH	٥	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		AB	CAC
109	.930	729.125	01	14	0020	•0199	.0003	•0006	.0005			•0000
110	.931	729.723	01	1.07	.1246	.0203	0001	.0005	•0005			•0000
111	.930	729.380	01	2.29	.2342	.0199	•0003	.0005	.0007			•0000
112	.931	729.563	01	3.50	•3362	.0186	0005	•0004	•0009			.0000
112	.933	731.256	01	4.69	.4541	.0185	0008	.0005	•0009			.0000
114	•935	732.665	01	5.93	•5647	.0202	•0006	.0005	.0013			•0000
115	.935	732.661	01	7.15	•6633	.0216	.0001	•0005	.0013			•0000
116	935	732.727	00	8.31	.7265	.0224	0002	.0003	.0007			•0000
117	.936	733.592	00	9.54	.8057	.0231	.0002	•0002	.0007			•0000
118	.937	734.470	00	10.69	•8752	.0234	.0007	•0002	-0008			•0000
	931	729.741	01	05	0024	.0200	0002	•0005	.0010			•0000
119	. 731	1270171	01	05	- 10024	*0200	•0002	•0005	*****			••••
	TEST= 7	78 RUN=	29		STAB	ILITY AXIS	COEFFICIENTS				PRESS.COEF	
POINT	MACH	ú	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
109	.930	729.125	01	14	0020	.0199	• 0065	.0003	.0006	099	.0062	11.5535
110	.931	729.723	01	1.07	.1242	<ul><li>0227</li></ul>	0016	0001	•0005	5.482	.0062	15.1970
111	.930	729.380	01	2.29	.2332	.0292	0048	.0003	•0005	7 <b>.</b> 992	.0061	21.8726
112	.931	729.563	01	3.50	.3345	.0390	•0002	0005	.0005	8.568	.0062	20.8539
113	.933	731.256	01	4.69	.4511	• 0556	0133	0008	.0006	8.118	.0061	27.0861
114	.935	732.665	01	5.93	•5596	.0784	0202	•0006	.0004	7.138	.0060	41.7078
115	.935	732.667	01	7.15	.6554	.1041	0201	.0001	•0005	6.298	.0059	77.0635
116	.935	732.727	00	8.31	.7156	.1272	.0021	0002	.0003	5.624	.0059	109-8431
117	.936	733.592	00	9.54	. 7907	•1563	.0087	•0003	-0001	5.058	.0057	131-3556
118	.937	734.470	00	10.69	.8557	-1853	.0136	.0007	.0001	4.617	.0056	154.3668
119	.931	729.741	01	05	0024	.0200	.0071	0002	•0005	120	.0061	10.8584

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

		_					S COEFFICIENT			BODY PRESS.	
OINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
132	. 863	675.122	00	16	0126	.0170	0000	•0006	0001	.0053	0.000
133	.863	674.634	00	•99	<b>.</b> 1006	•0159	.0004	•0006	0010	.0053	0.000
134	-801	673.513	01	2.19	•2171	•0120	-0004	-0006	•0004	.0053	0.000
135	-866	676.976	00	3.43	-3458	.0061	.0006	•0006	0003	.0053	0.000
136	-862	673.896	00	4.65	-4707	-0011	.000L	.0005	0003	.0053	0.000
137	-862	674.322	00	5.86	•5855	• 0004	•0005	-0005	0001	.0052	0.000
138	-865	676.724	00	7.07	•6594	•0054	0015	.0001	.0008	.0052	0.000
139	. 865	676.543	00	8.19	.7035	.0087	.0031	.0007	0003	.0051	0.000
140	-865	677.057	01	9.31	•7329	.0132	.0095	-0012	0001	.0051	0.000
141	.869	679.740	00	10.36	.7202	.0193	.0017	.0003	.0004	.0051	0.000
142	-865	676.334	00	11.45	.7439	•0223	0001	.0001	.0006	.0051	0.000
143	.866	677.540	00	12.56	.7846	.0243	.0001	.0000	.0011	.0050	0.000
144	.869	679.947	00	13.76	-8201	•0255	.0001	.0001	.0007	.0050	0.000
145	.868	679.205	00	16.04	•8994	-0263	0003	•0002	0008	.0047	0.000
146	.803	674.378	01	13	0144	.0166	.0000	.0006	.0009	.0053	0.000
147	-863	674.383	00	13	0126	.0169	.0000	.0006	0002	.0054	0.000

	TEST= 7	78 RUN=	30									
					STAE	BILITY AXIS (	OEFFICIENTS			STAB	PRESS.COEF	F
POINT	MACH	ú	BÉTA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
132	.863	675.122	00	16	0126	.0170	.0071	0000	•0006	736	.0053	9.7798
133	•8 <b>•</b> 3	674.639	00	•99	-1003	.0177	.0080	.0004	.0006	5.670	.0053	10.2831
134	-861	673.513	01	2.19	•2165	.0203	.0110	.0004	-0006	10.672	.0053	12.8000
135	•866	676.976	00	3.43	•3449	•0268	.0088	•0006	• 0006	12.881	.0053	16.9708
136	-862	673.896	00	4.65	• 4691	.0393	.0046	•0002	-0005	11.934	•0052	19.6674
137	-862	674.322	00	5.86	•5824	.0602	.0007	•0006	<b>-0004</b>	9.669	.0052	38.4718
138	-865	676.724	00	7.07	•6537	.0865	• 0256	0014	.0002	7.558	-0051	75.3856
139	-865	676.543	00	8.19	• 6951	.1088	•0560	.0031	.0002	6.386	-0051	89.1689
140	- 865	677.057	01	9.31	•7211	.1316	.0848	•0096	0004	5.478	.0050	119.9106
141	-869	679.740	00	10.36	. 7050	.1485	.1119	.0017	0000	4.748	.0051	134.2320
142	- 865	676.334	00	11.45	•7247	.1695	.1275	0000	.0001	4.276	•0050	99.4755
143	•866	677.540	00	12.56	•7605	<b>-1944</b>	.1355	-0001	.0000	3.913	.0049	96.3594
144	.869	679.941	00	13.76	• 7905	.2198	.1423	.0001	.0001	3.596	.0048	108.1047
145	.868	679.205	00	16.04	<ul><li>8572</li></ul>	.2737	-1573	0002	-0002	3.132	.0045	104.9886
146	-863	674.378	01	~.13	0144	.0167	.0076	.0000	-0006	863	.0053	10.1633
147	- 863	674.383	00	13	0125	.0169	-0065	.0000	-0006	741	•0054	10.1633

BODY AXIS COEFFICIENTS

CLB

CAF

BODY PRESS.COEFF

CAB

CAC

CSF

CNB

	MALH	ų	DETA	ALPHA	CINE	LAF	CLB	CND	USF		-AD	LAL
161	.806	624.062	01	13	0138	.0167	0002	.0007	.0000			0.0000
162	.806	623.642	01	•98	.0859	.0159	0002	.0007	.0018	• (	0049	0.0000
163	.807	025.147	01	2.15	•1931	.0123	•0005	.0008	.0006			0.0000
164	-807	625.170	01	3.34	•2979	.0064	.0001	.0007	.0003			0.0000
165	.807	625.217	01	4.49	-4125	0011	.0005	.0007	.0004	• 0	0050	0.0000
166	.807	624.588	01	5.73	-5293	0075	•0005	8000	.0009	•(	0048	0.0000
167	.805	622.862	00	6.88	•6035	0065	0005	.0003	.0011	•(	0047	0.0000
168	.808	626.038	01	8.02	•659l	.0000	.0019	.0007	.0010	• (	0048	0.0000
169	-807	624-497	00	9.12	•6770	.0079	.0009	•0004	.0011	• (	0048	0.0000
170	.808	625.446	00	10.18	.7019	.0135	0001	-0002	.0015	•(	0048	0.0000
171	.808	625.670	00	11.31	.7338	.0172	0003	• 00 Ó Z	.0011	• (	0047	0.0000
172	.810	627.917	00	12.42	.7652	.0201	0002	.0001	.0016	•0	0047	0.0000
173	.809	626.380	00	13.58	-8014	-0224	0000	-0002	.0010	•(	0046	0.0000
174	.811	628.180	00	15.81	.8586	.0246	.0001	.0003	.0002	•(	0044	0.0000
175		628.316	00	17.97	.9345	•0254	.0000	.0005	0002	• (	0042	0.0000
176	-812	629.122	•00	20.10	1.0117	.0255	.0000	0001	0006	• (	0035	0.0000
177		623.794	01	17	0158	.0167	0003	.0007	.0013	• (	0049	0.0000
	TEST= 7	78 RUN=	<b>31</b>		<b>\ΤΔ</b> н	ILITY AXIS C	DEFEICIENTS			STAR	.PRESS.COE	FF
POINT	MACH	ú	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	
161		024.062	01	13								PH-1
162	-806	021002			(1) 3/	-0167						PB-1 8-9887
		623-642			0137 -0856	.0167 .0173	.0064	0002	.0007	820	.0049	8.9887
			01	•98	-0856	.0173	.0064	0002 0002	.0007 .0007	820 4.937	.0049 .0049	8.9887 8.8449
163	.807	625.147	01 01	•98 2•15	•0856 •1926	.0173 .0195	.0064 .0087 .0133	0002 0002 .0005	.0007 .0007 .0008	820 4.937 9.869	.0049 .0049 .0050	8.9887 8.8449 8.5573
164	.807 .807	625.147 625.170	01 01 01	.98 2.15 3.34	•0856 •1926 •2971	.0173 .0195 .0237	.0064 .0087 .0133 .0195	0002 0002 .0005 .0001	.0007 .0007 .0008 .0007	820 4.937 9.869 12.520	.0049 .0049 .0050 .0049	8.9887 8.8449 8.5573 10.9303
164 165	.807 .807	625.147 625.170 625.217	01 01 01	.98 2.15 3.34 4.49	.0856 .1926 .2971 .4113	.0173 .0195 .0237 .0312	.0064 .0087 .0133 .0195	0002 0002 .0005 .0001 .0005	.0007 .0007 .0008 .0007	820 4.937 9.869 12.520 13.188	.0049 .0049 .0050 .0049	8.9887 8.8449 8.5573 10.9303 12.4165
164 165 166	.807 .807 .807	625.147 625.170 625.217 624.588	01 01 01 01	.98 2.15 3.34 4.49 5.73	.0856 .1926 .2971 .4113 .5274	.0173 .0195 .0237 .0312 .0453	.0064 .0087 .0133 .0195 .0242 .0258	0002 0002 .0005 .0001 .0005	.0007 .0007 .0008 .0007 .0007	820 4.937 9.869 12.520 13.188 11.636	.0049 .0049 .0050 .0049 .0050	8.9887 8.8449 8.5573 10.9303 12.4165 17.3063
164 165 166 167	.807 .807 .807 .807	625.147 625.170 625.217 624.588 622.862	01 01 01 01 01	.98 2.15 3.34 4.49 5.73 6.88	.0856 .1926 .2971 .4113 .5274	.0173 .0195 .0237 .0312 .0453	.0064 .0087 .0133 .0195 .0242 .0258	0002 0002 .0005 .0001 .0005 .0006	.0007 .0007 .0008 .0007 .0007 .0007	820 4.937 9.869 12.520 13.188 11.636 9.123	.0049 .0049 .0050 .0049 .0050 .0048	8.9887 8.8449 8.5573 10.9303 12.4165 17.3063 38.1722
164 165 166 167 168	.807 .807 .807 .807 .805	625.147 625.170 625.217 624.588 622.862 626.038	01 01 01 01 00 01	.98 2.15 3.34 4.49 5.73 6.88 8.02	.0856 .1926 .2971 .4113 .5274 .5999	.0173 .0195 .0237 .0312 .0453 .0658	.0064 .0087 .0133 .0195 .0242 .0258 .0431	0002 0002 .0005 .0001 .0005 .0006 0004	.0007 .0007 .0008 .0007 .0007 .0007 .0003	820 4.937 9.869 12.520 13.188 11.636 9.123 7.094	.0049 .0049 .0050 .0049 .0050 .0048 .0047	8.9887 8.8449 8.5573 10.9303 12.4165 17.3063 38.1722 61.0036
164 165 166 167 168 169	.807 .807 .807 .805 .808	625.147 625.170 625.217 624.588 622.862 626.038 624.497	01 01 01 01 00 01 00	.98 2.15 3.34 4.49 5.73 6.88 8.02 9.12	.0856 .1926 .2971 .4113 .5274 .5999 .6526	.0173 .0195 .0237 .0312 .0453 .0658 .0920	.0064 .0087 .0133 .0195 .0242 .0258 .0431 .0771	0002 0002 .0005 .0001 .0005 .0006 0004 .0020	.0007 .0007 .0008 .0007 .0007 .0007 .0003 .0004	820 4.937 9.869 12.520 13.188 11.636 9.123 7.094 5.799	.0049 .0049 .0050 .0049 .0050 .0048 .0047	8.9887 8.8449 8.5573 10.9303 12.4165 17.3063 38.1722 61.0036
164 165 166 167 168 169 170	.807 .807 .807 .807 .805 .808	625.147 625.170 625.217 624.588 622.862 626.038 624.497 625.446	01 01 01 01 00 01 00 00	.98 2.15 3.34 4.49 5.73 6.88 8.02 9.12 10.18	.0856 .1926 .2971 .4113 .5274 .5999 .6526 .6672	.0173 .0195 .0237 .0312 .0453 .0658 .0920 .1150	.0064 .0087 .0133 .0195 .0242 .0258 .0431 .0771 .1081	0002 0002 .0005 .0001 .0005 .0006 0004 .0020 .0009	.0007 .0007 .0008 .0007 .0007 .0007 .0003 .0004 .0002	820 4.937 9.869 12.520 13.188 11.636 9.123 7.094 5.799 5.010	.0049 .0049 .0050 .0049 .0050 .0048 .0047 .0048	8.9887 8.8449 8.5573 10.9303 12.4165 17.3063 38.1722 61.0036 106.2476 92.9442
164 165 166 167 168 169 170	.807 .807 .807 .805 .805 .808 .808	625.147 625.170 625.217 624.588 622.862 626.038 624.497 625.446 625.670	01 01 01 01 00 00 00 00	.98 2.15 3.34 4.49 5.73 6.88 8.02 9.12 10.18 11.31	.0856 .1926 .2971 .4113 .5274 .5999 .6526 .6672 .6884	.0173 .0195 .0237 .0312 .0453 .0658 .0920 .1150 .1374 .1609	.0064 .0087 .0133 .0195 .0242 .0258 .0431 .0771 .1081 .1259	0002 0002 .0005 .0001 .0006 0004 .0020 .0009 0001	.0007 .0007 .0008 .0007 .0007 .0007 .0003 .0004 .0002	820 4.937 9.869 12.520 13.188 11.636 9.123 7.094 5.799 5.010 4.452	.0049 .0049 .0050 .0049 .0050 .0048 .0047 .0048 .0047	8.9887 8.8449 8.5573 10.9303 12.4165 17.3063 38.1722 61.0036 106.2476 92.9442 96.5397
164 165 166 167 168 169 170 171	.807 .807 .807 .805 .805 .805 .808 .808	625.147 625.170 625.217 624.588 622.862 626.038 624.497 625.6446 625.670 627.917	01 01 01 01 00 00 00 00 00	.98 2.15 3.34 4.49 5.73 6.88 8.02 9.12 10.18 11.31 12.42	.0856 .1926 .2971 .4113 .5274 .5999 .6526 .6672	.0173 .0195 .0237 .0312 .0453 .0658 .0920 .1150	.0064 .0087 .0133 .0195 .0242 .0258 .0431 .0771 .1081	0002 0002 .0005 .0001 .0005 .0006 0004 .0020 .0009	.0007 .0007 .0008 .0007 .0007 .0007 .0003 .0004 .0002	820 4.937 9.869 12.520 13.188 11.636 9.123 7.094 5.799 5.010	.0049 .0049 .0050 .0049 .0050 .0048 .0047 .0048	8.9887 8.8449 8.5573 10.9303 12.4165 17.3063 38.1722 61.0036 106.2476 92.9442
164 165 166 167 168 169 170 171 172	.807 .807 .807 .805 .805 .807 .808 .807 .808	625.147 625.170 625.217 624.588 622.862 626.038 624.497 625.446 625.670 627.917 626.380	01 01 01 01 00 00 00 00 00 00	.98 2.15 3.34 4.49 5.73 6.88 8.02 9.12 10.18 11.31 12.42 13.58	.0856 .1926 .2971 .4113 .5274 .5999 .6526 .6672 .6884 .7162 .7430	.0173 .0195 .0237 .0312 .0453 .0658 .0920 .1150 .1374 .1609 .1842 .2099	.0064 .0087 .0133 .0135 .0242 .0258 .0431 .0771 .1081 .1259 .1412	0002 0002 .0005 .0001 .0005 .0006 0004 .0020 .0009 0001 0002	.0007 .0007 .0008 .0007 .0007 .0007 .0003 .0004 .0002 .0003	820 4.937 9.869 12.520 13.188 11.636 9.123 7.094 5.799 5.010 4.452 4.033	.0049 .0049 .0050 .0049 .0050 .0048 .0047 .0048 .0047	8.9887 8.8449 8.5573 10.9303 12.4165 17.3063 38.1722 61.0036 106.2476 92.9442 96.5397 106.6072
164 165 166 167 168 169 170 171 172 173 174	.807 .807 .807 .805 .805 .805 .808 .808 .808 .810	625.147 625.170 625.217 624.588 622.862 626.038 624.497 625.446 625.670 627.917 626.380 628.180	0101010100000000	.98 2.15 3.34 4.49 5.73 6.88 8.02 9.12 10.18 11.31 12.42	.0856 .1926 .2971 .4113 .5274 .5999 .6526 .6672 .6884 .7162	.0173 .0195 .0237 .0312 .0453 .0658 .0920 .1150 .1374 .1609	.0064 .0087 .0133 .0195 .0242 .0258 .0431 .0771 .1081 .1259 .1412 .1543 .1658	0002 0002 .0005 .0001 .0005 .0006 0004 .0020 .0009 0001 0002 .0002	.0007 .0007 .0008 .0007 .0007 .0007 .0003 .0004 .0002 .0003 .0002	820 4-937 9-869 12-520 13-188 11-636 9-123 7-094 5-799 5-010 4-452 4-033 3-686	.0049 .0049 .0050 .0049 .0050 .0048 .0047 .0048 .0047 .0046 .0046	8.9887 8.8449 8.5573 10.9303 12.4165 17.3063 38.1722 61.0036 106.2476 92.9442 96.5397 106.6072 90.2476
164 165 166 167 168 169 170 171 172	.807 .807 .807 .807 .805 .805 .808 .808 .810 .809 .811	625.147 625.170 625.217 624.588 622.862 626.038 624.497 625.446 625.670 627.917 626.380	0101010100010000	.98 2.15 3.34 4.49 5.73 6.88 8.02 9.12 10.18 11.31 12.42 13.58 15.81	.0856 .1926 .2971 .4113 .5274 .5999 .6526 .6672 .6884 .7162 .7430 .7737	.0173 .0195 .0237 .0312 .0453 .0658 .0920 .1150 .1374 .1609 .1842 .2099	.0064 .0087 .0133 .0195 .0242 .0258 .0431 .0771 .1081 .1259 .1412 .1543 .1658	0002 0002 .0005 .0001 .0005 .0006 0004 .0020 .0009 0001 0002 0002	.0007 .0007 .0008 .0007 .0007 .0007 .0003 .0004 .0002 .0003 .0002 .0002	820 4-937 9-869 12-520 13-188 11-636 9-123 7-094 5-799 5-010 4-452 4-033 3-686 3-181	.0049 .0049 .0050 .0049 .0050 .0048 .0047 .0046 .0046 .0046 .0046	8.9887 8.8449 8.5573 10.9303 12.4165 17.3063 38.1722 61.0036 92.9442 96.5397 106.6072 90.2476 85.3936

TEST= 778 RUN= 31

BETA ALPHA

CNF

MACH

POINT

POINT         MACH         Q         BETA         ALPHA         CNF         CAF           191         .753         573.003        01        10        0130         .0164           192         .752         572.404        01         .97         .0817         .0156           193         .755         575.026        01         2.11         .1816         .0125           194         .754         573.551        01         3.24         .2786         .0070           195         .754         574.187        01         4.38         .3724         .0004           196         .754         574.389        01         5.57         .4708        003           197         .755         575.239        01         6.72         .5439         .0010           198         .750         576.110        00         7.84         .5951         .006           199         .754         574.272        01         8.96         .6356         .009	650001 .0008 .0012 .0047 0.0000 580000 .0007 .0018 .0047 0.0000 25 .0002 .0008 .0011 .0048 0.0000
191	650001 .0008 .0012 .0047 0.0000 580000 .0007 .0018 .0047 0.0000 25 .0002 .0008 .0011 .0048 0.0000
192	580000 .0007 .0018 .0047 0.0000 25 .0002 .0008 .0011 .0048 0.0000
193       .755       575.026      01       2.11       .1816       .012         194       .754       573.551      01       3.24       .2786       .0070         195       .754       574.187      01       4.38       .3724       .0004         196       .754       574.389      01       5.57       .4708      003         197       .755       575.239      01       6.72       .5439       .0010         198       .750       576.110      00       7.84       .5951       .006         199       .754       574.272      01       8.96       .6356       .009	25 .0002 .0008 .0011 .0048 0.0000
194	
195	70 .0002 .0007 .0004 .0047 0.0000
196     .754     574.389    01     5.57     .4708    003;       197     .755     575.239    01     6.72     .5439     .0010       198     .756     576.110    00     7.84     .5951     .0060       199     .754     574.272    01     8.96     .6356     .009	
197	04 .0001 .0007 .0012 .0047 0.0000
198	32 .0005 .0007 .0014 .0047 0.0000
199 .754 574.27201 8.96 .6356 .009	10 .0018 .0010 .0004 .0047 0.0000
	60
	97 •0005 •0005 •0023 •0046 0•0000
200 .756 575.60300 10.09 .6831 .0126	26 •0004 •0004 •0017 •0046 0•0000
201 .755 575.13900 11.21 .7320 .015	530009 .0003 .0011 .0045 0.0000
202 .755 574.96500 12.30 .7612 .0179	750011 .0003 .0021 .0044 0.0000
203 .756 575.77400 13.44 .7837 .0194	940006 .0003 .0010 .0044 0.0000
204 .757 576.90800 15.67 .8412 .0224	24 .0002 .0004 .0008 .0043 0.0000
205 .758 577.46700 17.80 .9052 .0236	36 .0002 .0005 .0003 .0041 0.0000
206 .758 577.88100 19.92 .9799 .024	49 -0002 -0000 -0025 -0034 0-0000
207 .758 577.64500 22.02 1.0588 .0238	380003 .00040013 .0027 0.0000
210 .754 573.99101140144 .0169	65 -0007 .0008 .0017 .0047 0.0000
211 •754 573•836 -•01 •97 •0814 •015	590002 .0008 .0020 .0048 0.0000
212 .754 573.39701 2.10 .1761 .0129	25 .0003 .0008 .0023 .0047 0.0000
213 .754 573.41301 3.24 .2784 .007	71 .0001 .0007 .0017 .0047 0.0000
214 .753 573.00401 4.40 .3731 .000	
215 .753 572.36201 5.57 .4703003.	03 .0000 .0007 .0012 .0047 0.0000

	TEST= 7	78 RUN=	32									
					STA	BILITY AXIS (	COEFFICIENTS			STAB	.PRESS.COEF	F
PUINT	MACH	Ų	BETA	ALPHA	CL	CO	CPM	CLS	CNS	L/D	CDB	PB-1
191	•753	573.003	01	10	0129	.0165	.0057	0001	.0008	783	.0047	8.3416
192	•752	572.404	01	•97	.0814	.0172	•0096	0000	.0007	4.726	.0047	8.6652
193	•755	575.026	01	2.11	.1810	-0192	.0149	•0002	.0008	9.426	•0048	8.3296
194	• 754	573.551	01	3.24	• 2777	<b>.</b> 0228	-0219	•0003	.0007	12.181	.0047	8.7011
195	.754	574.187	01	4.38	•3713	• 0288	.0279	•0001	•0006	12.884	.0047	9.6120
196	• 754	574.389	01	5.57	• 4688	.0425	.0337	• 0005	•0006	11.025	.0047	15.6045
197	.755	575.239	01	6.72	•5401	.0646	• 0575	.0019	•0008	8.356	.0047	45.1834
198	• 756	576.110	00	7.84	•5888	.0871	.0854	.0007	•0004	6.760	.0046	66.3969
199	• 754	574.272	01	8.96	•6264	.1086	.1100	•0006	-0004	5.768	.0045	81.2588
200	• 756	575.603	00	10.09	•6704	.1321	.1287	.0004	.0003	5.075	• 0045	106.4274
201	• 755	575.139	00	11.21	•7151	.1574	-1441	0009	•0005	4.544	.0044	209.9772
202	.755	574.965	00	12.30	•7400	.1792	<ul><li>1566</li></ul>	0010	•0005	4.129	.0043	257.0790
203	- 756	575.774	00	13.44	.7577	.2010	.1713	0005	.0004	3.769	.0043	139.8653
204	.757	576.908	00	15.67	.8039	.2487	-1868	.0003	.0003	3.232	.0042	77.3037
205	<b>-7</b> 58	577.467	00	17.80	<ul><li>8547</li></ul>	.2992	•1946	•0003	•0004	2.856	•0039	81.7981
206	∙758	577.881	00	19.92	-9128	• 3572	.1926	.0002	0001	2.555	.0032	85.7532
207	.758	577.645	00	22.02	•9727	•4190	.2004	0001	•0005	2.322	•0025	98.3375
210	• 754	573.991	01	14	0144	.0166	•0055	-0007	.0008	867	•0047	8.4374
211	• 754	573.836	01	•97	.0811	.0172	•0096	0001	.0008	4.703	.0048	8.3895
212	.754	573.397	01	2.10	• 1756	.0189	.0135	•0003	.0008	9.286	•0047	8.1498
213	.754	573.413	01	3.24	• 2776	•0228	-0219	•0002	.0007	12.165	.0047	8.7970
214	.753	573.004	01	4.40	.3720	.0290	.0272	.0001	.0007	12.849	.0047	8.9168
215	.753	572.362	01	5.57	<b>.</b> 4084	•0424	.0343	.0005	.0007	11.037	.0047	15.0771

	TEST≂ 7	78 RUN=	33								
						BODY AXI	S COEFFICIEN	TS.		BODY PRESS.	COEFF
POINT	MACH	Ú	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
229	•700	519.721	01	08	0183	.0165	.0004	.0008	.0009	• 0045	0.0000
230	.701	520.739	01	. 97	•0721	•0160	0002	.0007	.0010	.0046	0.0000
231	.701	520.357	00	2.09	•1652	.0127	0002	.0007	.0003	•0046	0.0000
232	.702	520.835	00	3.23	.2538	.0076	•0002	.0006	0005	•0046	0.0000
233	•702	521.323	00	4.32	·3459	.0011	0003	•0005	.0007	.0045	0.0000
234	•702	521.404	00	5.50	.4411	0034	.0002	•0005	.0008	• 0045	0.0000
235	.701	520.058	00	6.63	.5189	•0002	.0010	.0007	0008	•0045	0.0000
236	.703	521.963	00	7.74	•5704	.0053	0004	.0003	.0010	.0044	0.0000
237	<b>.</b> 703	522.247	00	8.87	.6198	.0082	.0002	•0004	•0008	.0044	0.0000
238	.702	521.897	00	9.96	•0633	.0102	.0004	.0004	.0013	.0043	0.0000
239	.702	521.506	00	11.09	.7001	.0127	.0001	•0003	.0009	.0043	0.0000
240	د70ء	522.641	00	12.18	.7351	.0149	0001	•0003	•0006	.0043	0.0000
241	•703	522.496	00	13.33	•7697	.0169	0001	.0002	.0014	•0042	0.0000
242	• 704	523.378	00	15.56	.8330	•0206	.0000	.0004	•0005	.0041	0.0000
243	.705	524.332	00	17.68	.8896	.0219	0001	.0004	.0001	.0040	0.0000
244	• 705	524 <b>-</b> 174	00	19.77	•9555	.0243	.0001	.0003	0003	.0034	0.0000
245	.706	525.533	.00	21.87	1.0225	.0235	•0002	.0002	0009	.0027	0.0000
246	•699	518-136	01	11	0184	.0164	.0002	.0008	.0011	• 0044	0.0000

	TEST= 7	78 KUN=	33									
					STA	BILITY AXIS	COEFFICIENTS			STAB	PRESS.COEF	F
PUINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
229	•700	519.721	01	08	0183	.0165	.0051	.0004	.0009	-1.106	-0045	8.7730
230	.701	520.739	01	•97	.0719	.0172	.0094	0002	.0007	4.185	.0046	7.5505
231	.701	520.351	00	2.09	.1646	.0187	.0149	0001	.0007	8.792	•0046	7.7663
232	.70∠	520.835	00	3.23	. 2530	.0219	.0214	.0002	•0006	11.546	•0046	7.7663
233	•702	521.323	00	4.32	. 3448	.0271	.0284	0003	.0005	12.722	.0045	8.0539
234	.702	521.404	00	5.50	• 4394	•0388	.0372	.0003	.0005	11.314	.0045	10.1633
235	.701	520.658	00	6.63	•5154	.0601	· 0545	-0011	•0006	8.574	•0045	42.0074
236	.703	521.963	00	7.74	• 5644	.0821	•0846	0004	.0003	6.875	.0044	57.6478
237	.703	522.247	00	8.87	.6111	-1037	-1106	.0003	• 0004	5.895	.0043	67.1160
238	.702	521.897	00	9.96	.6516	.1248	.1303	-0004	.0003	5.222	.0043	69.7527
239	-70∠	521.560	00	11.09	•6846	.1471	.1478	•0002	.0003	4.653	.0042	75.8650
240	.703	522.041	00	12.18	.7154	.1697	.1617	0001	.0003	4.216	.0042	74.7864
241	.703	522.496	00	13.33	.7450	.1940	.1743	0000	.0002	3.840	.0041	74.4268
242	.704	523.378	00	15.56	• 7969	. 2433	.1931	.0001	.0004	3.275	.0039	75.2658
243	.705	524.332	00	17.68	.8409	.2911	.2015	0000	-0004	2.889	.0038	73.8276
244	.735	524.174	00	19.77	.8910	.3460	.1977	.0001	.0002	2.575	•0032	84.0148
245	. 700	525.533	.00	21.87	.9401	.4026	-2022	.0003	.0001	2.335	•0025	92.4043
246	.699	518.130	01	11	0184	.0165	.0043	.0002	-0008	-1.116	.0044	7.7903

TEST= 778 KUN= 34

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 KUN= 3	14									
						BODY AXI	S CUEFFICIEN	TS		BODY	PRESS.COEF	F
PUINT	MACH	ن	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		AB	CAC
260	•490	305.654	00	01	0118	.0171	.0004	.0007	.0019			.0000
261	.497	306.717	00	1.01	.0667	.0166	•0000	.0008	.0017			.0000
262	490	306.097	00	2.04	.1454	.0135	0004	.0008	.0016			.0000
263	.498	301.253	00	3.09	.2280	.0095	.0004	.0007	.0003			.0000
264	498	307.786	00	4.11	.3022	.0029	0001	•0006	-0002			.0000
265	499	308.416	00	5.20	.3800	0045	0001	•0002	.0020			.0000
266	498	307.846	00	6.32	.4704	0067	-0001	.0002	.0012			0.0000
267	498	307.310	00	7.40	.5370	0024	0003	.0004	.0008			0.0000
268	.497	306.775	00	8.50	.5913	.0008	•0005	•0005	0010			0.0000
269	.497	300.855	•00	9.56	.6404	.0022	.0004	.0003	0018			0.0000
270	499	308.538	00	10.68	.6872	.0037	.0000	.0004	0000			0.0000
271	.497	300.673	00	11.72	.7200	.0059	.0001	.0005	.0017			0.0000
272	499	308.552	00	12.86	.7631	.0081	.0002	.0002	•0009			0.0000
273	-498	307.425	00	15.05	.8272	.0119	0000	.0002	.0002			0.0000
274	.498	307.463	00	17.15	.8923	.0151	0003	.0003	0004			0.0000
275	.497	300.970	00	19.24	.9524	.0175	0001	.0003	0012			0.0000
276	-498	307.828	00	21.24	1.0004	.0206	0009	.0006	0004			0.0000
277	•490	305.290	00	07	0160	.0173	0001	.0007	.0024			0.0000
	TEST= 7	78 RUN= .	34		STAD	ILLEY AVIC O	OSSESSOR			C.F.L.O.	PR 500 COS	
00				** ***		ILITY AXIS C					PRESS COE	
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
260	•496	305.654	00	01	0118	.0171	•0053	-0004	.0007	692	•0041	4.5663
261	•497	306.717	00	1.01	-0664	.0177	-0111	•0000	.0008	3.745	-0041	4.7101
262	• 496 • 498	306.097	00	2.04	.1449	.0187	.0170	0004	•0009	7.761	.0041	4.6622
263		307.253 307.786	00 00	3.09	• 2272	.0218 .0246	•0233	•0004	.0007	10.433	-0041	4.7700
264	• 498 • 499	308.416		4.11	•3012 •3788		•0286 •0357	0000	•0006	12.246	•0040	4.3985
265		308.416	00	5.20 6.32	• 3788 • 4683	.0300 .0451		0001	•0002	12.646	-0041	4.4344
266 267	• 498 • 498	367.310	00 00	7.40	• 5328	.0667	•0442	•0001	•0002	10.389	•0040	9.4202
268	•490 •497	306.775	00	8.50	• 5528 • 5866	.0885	.0621 .0884	0003	.0004 .0005	7.987	-0040	32.0599
269	•497	306.119	•00	9.56	•6312	.1086		•0006		6.630	.0039	51.8950
270	•491	308.538		10.68	•6746	.1310	-1136	•0005	-0003	5.814	•0038	55.4905
	•497	300.530	00	11.72			-1384	•0001	.0004	5.149	.0037	56.4493
271 2 <i>1</i> 2		308.552	00	12.86	• 7038 • 7422	.1520	•1557	•0002	•0005	4.629	.0036	60.4044
273	-499		00			.1777	-1720	•0002	-0001	4.176	.0036	61-2433
213 274	•498	307.425 307.463	00 00	15.05 17.15	• <b>7</b> 958	.2262	•1983	•0000	•0002	3.517	.0034	67.3557
	-498 407	306.976		19.24	•8482 vo35	• 2776	-2190	0002	.0003	3.056	.0033	62.4418
275	-49 <i>1</i>	307.828	00		• 8935 0350	.3303	•2284	0000	.0003	2.705	.0030	62.3220
276 277	•498 404	307.828	00 00	21.24 07	•9250 -•0160	.3817	•2195	0006	•0009	2.423	•0024	71.5504
211	•496	303.290	00	07	0100	.0174	•0049	0001	.0007	921	.0040	4.3386

	TEST= 7	78 RUN=	35			DODY AVI	e corestetes	LTC		PONV	PRESS.COE	£ <b>E</b>
_					64.5		S COEFFICIEN		CSF		AB	CAC
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	.0008	•0005			0.0000
278	.290	116.858	00	07	0209	.0178	0006	.0008	0006			0.0000
279	.291	117.535	00	• 94	.0580	.0176	.0001		0012			0.0000
280	-292	118.114	00	1.93	.1358	.0148	.0001	.0008				0.0000
281	.293	118.696	00	2.97	.2028	.0120	0003	• 0006	0013			0.0000
282	.294	119.373	00	3.95	- 2684	.0066	0003	•0009	.0041			0.0000
283	-292	110.024	00	4.99	.3500	0006	-0002	•0007	.0033			0.0000
284	.291	117.355	00	6.06	•4206	0070	.0002	.0005	.0028			
285	.291	117.377	00	7.08	•4971	0054	0003	.0003	.0027			0.0000
286	.292	117.981	00	8-14	-5607	0032	.0001	•0005	.0014			0.0000
287	.292	117.909	00	9.18	.6179	0027	.0007	.0007	.0000			0.0000
288	. 291	117.258	00	10.26	•6579	0020	.0007	•0008	0008			0.0000
289	•292	117.963	00	11.32	.7009	0006	.0012	.0005	0020			0.0000
290	. 292	117.994	00	12.41	•7462	.0008	.0000	•0007	0017			0.0000
291	.291	117.385	•00	14.57	.8238	.0048	0005	•0005	0024		033	0.0000
292	-292	118.034	.00	16.63	-8835	.0086	0005	•0002	0035			0.0000
293	.289	115.060	•00	18.67	•9145	-0111	0007	.0003	0036			0.0000
294	.292	118.086	.00	20.69	1.0026	.0145	0001	.0006	0051			0.0000
295	.291	117.064	00	10.26	.6591	0021	.0007	.0008	0007	• 0	035	0.0000
	TEST= 7	778 RUN=	35		STAF	ATLETY AXIS (	DEFEICIENTS			STAB	.PRESS_COF	FF
DOINT				AI OLIA		BILITY AXIS C		CI S	CNS		.PRESSCOE	
POINT	MACH	4	BETA	ALPHA	CL	CD	CPM	CLS 0006	CNS - 0008	L/D	CDB	PB-1
278	MACH •290	ي 116.858	BETA 00	07	CL 0209	CD •0178	CPM •0044	0006	.0008	L/D -1.172	CDB •0038	PB-1 1.5940
278 279	MACH •290 •291	116.858 117.535	BETA 00 00	07 .94	CL 0209 .0577	CD •0178 •0186	CPM •0044 •0091	0006 .0001	.0008	L/D -1.172 3.107	CDB •0038 •0039	PB-1 1.5940 1.7738
278 279 280	MACH •290 •291 •292	116.858 117.535 118.114	BETA 00 00	07 .94 1.93	CL 0209 .0577 .1352	CD •0178 •0186 •0194	CPM •0044 •0091 •0172	0006 .0001 .0001	.0008 .0010 .0008	L/D -1.172 3.107 6.980	CDB •0038 •0039 •0039	PB-1 1.5940 1.7738 1.8337
278 279 280 281	MACH •290 •291 •292 •293	116.858 117.535 118.114 118.696	BETA 00 00 00 00	07 .94 1.93 2.97	CL 0209 .0577 .1352 .2019	CD •0178 •0186 •0194 •0225	CPM •0044 •0091 •0172 •0241	0006 .0001 .0001 0003	.0008 .0010 .0008 .0006	L/D -1.172 3.107 6.980 8.985	CDB •0038 •0039 •0039 •0039	PB-1 1.5940 1.7738 1.8337 1.9296
278 279 280 281 282	MACH •290 •291 •292 •293 •294	116.858 117.535 118.114 118.696 119.373	BETA 00 00 00 00	07 .94 1.93 2.97 3.95	CL 0209 .0577 .1352 .2019 .2673	CD •0178 •0186 •0194 •0225 •0251	CPM .0044 .0091 .0172 .0241 .0309	0006 .0001 .0001 0003 0002	.0008 .0010 .0008 .0006	L/D -1.172 3.107 6.980 8.985 10.659	CDB •0038 •0039 •0039 •0039	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933
278 279 280 281 282 283	MACH •290 •291 •292 •293 •294 •292	116.858 117.535 118.114 118.696 119.373 118.024	BETA 00 00 00 00 00	07 .94 1.93 2.97 3.95 4.99	CL 0209 .0577 .1352 .2019 .2673	CD .0178 .0186 .0194 .0225 .0251	CPM .0044 .0091 .0172 .0241 .0309 .0359	0006 .0001 .0001 0003 0002	.0008 .0010 .0008 .0006 .0010	L/D -1.172 3.107 6.980 8.985 10.659 11.680	CDB .0038 .0039 .0039 .0039 .0038 .0039	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933 1.6180
278 279 280 281 282 283 284	MACH .290 .291 .292 .293 .294 .292 .291	116.858 117.535 118.114 118.696 119.373 118.024	BETA 00 00 00 00 00 00	07 .94 1.93 2.97 3.95 4.99 6.06	CL 0209 .0577 .1352 .2019 .2673 .3488 .4190	CD •0178 •0186 •0194 •0225 •0251 •0299 •0374	CPM .0044 .0091 .0172 .0241 .0309 .0359 .0432	0006 .0001 .0001 0003 0002 .0002	.0008 .0010 .0008 .0006 .0010 .0007	L/D -1.172 3.107 6.980 8.985 10.659 11.680 11.196	CDB .0038 .0039 .0039 .0039 .0038 .0039 .0039	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933 1.6180 2.6727
278 279 280 281 282 283 284 285	MACH •290 •291 •292 •293 •294 •291 •291	116.858 117.535 118.114 118.696 119.373 118.024 117.355 117.377	BETA 00 00 00 00 00 00 00	07 .94 1.93 2.97 3.95 4.99 6.06 7.08	CL 0209 .0577 .1352 .2019 .2673 .3488 .4190	CD .0178 .0186 .0194 .0225 .0251 .0299 .0374 .0559	CPM .0044 .0091 .0172 .0241 .0309 .0359 .0432	0006 .0001 .0001 0003 0002 .0002 0002	.0008 .0010 .0008 .0006 .0010 .0007 .0005	L/D -1.172 3.107 6.980 8.985 10.659 11.680 11.196 8.843	CDB .0038 .0039 .0039 .0039 .0038 .0039 .0039	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933 1.6180 2.6727 9.9955
278 279 280 281 282 283 284 285 286	MACH .290 .291 .292 .293 .294 .292 .291 .292	116.858 117.535 118.114 118.696 119.373 118.024 117.357 117.981	BETA00000000000000	07 .94 1.93 2.97 3.95 4.99 6.06 7.08 8.14	CL 0209 .0577 .1352 .2019 .2673 .3488 .4190 .4939	CD • 0178 • 0186 • 0194 • 0225 • 0251 • 0299 • 0374 • 0559 • 0763	CPM .0044 .0091 .0172 .0241 .0309 .0359 .0432 .0511 .0717	0006 .0001 .0001 0003 0002 .0002 0002	.0008 .0010 .0008 .0006 .0010 .0007 .0005 .0004	L/D -1.172 3.107 6.980 8.985 10.659 11.680 11.196 8.843 7.283	CDB .0038 .0039 .0039 .0039 .0038 .0039 .0039 .0037	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933 1.6180 2.6727 9.9955 20.6142
278 279 280 281 282 283 284 285 286 287	MACH • 290 • 291 • 292 • 293 • 294 • 292 • 291 • 291 • 292 • 292	116.858 117.535 118.114 118.696 119.373 118.024 117.355 117.377 117.981	BETA00000000000000	07 .94 1.93 2.97 3.95 4.99 6.06 7.08 8.14 9.18	CL 0209 .0577 .1352 .2019 .2673 .3488 .4190 .4939 .5555	CD • 0178 • 0186 • 0194 • 0225 • 0251 • 0299 • 0374 • 0559 • 0763 • 0959	CPM .0044 .0091 .0172 .0241 .0309 .0359 .0432 .0511 .0717	0006 .0001 .0001 0003 0002 .0002 .0002 0003 .0002	.0008 .0010 .0008 .0006 .0010 .0007 .0005 .0004	L/D -1.172 3.107 6.980 8.985 10.659 11.680 11.196 8.843 7.283 6.367	CDB .0038 .0039 .0039 .0039 .0039 .0037 .0037	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933 1.6180 2.6727 9.9955 20.6142 28.7640
278 279 280 281 282 283 284 285 286 287 288	MACH .290 .291 .292 .293 .294 .291 .291 .292 .292 .292	116.858 117.535 118.114 118.696 119.373 118.024 117.355 117.377 117.981 117.909	BETA00000000000000	07 .94 1.93 2.97 3.95 4.99 6.06 7.08 8.14 9.18	CL 0209 .0577 .1352 .2019 .2673 .3488 .4190 .4939 .5555 .6104	CD .0178 .0186 .0194 .0225 .0251 .0299 .0374 .0559 .0763 .0959 .1152	CPM .0044 .0091 .0172 .0241 .0309 .0359 .0432 .0511 .0717	0006 .0001 .0001 0003 0002 .0002 0003 .0002 0003	.0008 .0010 .0008 .0006 .0010 .0007 .0005 .0004 .0005	L/D -1.172 3.107 6.980 8.985 10.659 11.680 11.196 8.843 7.283 6.367 5.621	CDB .0038 .0039 .0039 .0039 .0039 .0037 .0037	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933 1.6180 2.6727 9.9955 20.6142 28.7640 32.7790
278 279 280 281 282 283 284 285 286 287 288	MACH .290 .291 .292 .293 .294 .291 .291 .292 .292 .292 .294	116.858 117.535 118.114 118.696 119.373 118.024 117.355 117.377 117.981 117.909 117.258 117.463	BETA00000000000000	07 .94 1.93 2.97 3.95 4.99 6.06 7.08 8.14 9.18 10.26 11.32	CL 0209 .0577 .1352 .2019 .2673 .3488 .4190 .4939 .5555 .6104 .6478	CD .0178 .0186 .0194 .0225 .0251 .0299 .0374 .0559 .0763 .0959 .1152 .1370	CPM .0044 .0091 .0172 .0241 .0309 .0359 .0432 .0511 .0717 .0915 .1166 .1381	0006 .0001 .0001 0003 0002 .0002 0003 .0002 .0008	.0008 .0010 .0008 .0006 .0010 .0007 .0005 .0004 .0005 .0006	L/D -1.172 3.107 6.980 8.985 10.659 11.680 11.196 8.843 7.283 6.367 5.621 5.019	CDB .0038 .0039 .0039 .0039 .0038 .0039 .0037 .0036 .0036	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933 1.6180 2.6727 9.9955 20.6142 28.7640 32.7790
278 279 280 281 282 283 284 285 286 287 288 289 290	MACH 290 291 292 293 294 291 291 292 292 291 292 292	116.858 117.535 118.114 118.696 119.373 118.024 117.355 117.377 117.981 117.909 117.258 117.963	BETA00000000000000	07 .94 1.93 2.97 3.95 4.99 6.06 7.08 8.14 9.18 10.26 11.32	CL 0209 .0577 .1352 .2019 .2673 .3488 .4190 .4939 .5555 .6104 .6474 .6874	CD .0178 .0186 .0194 .0225 .0251 .0299 .0374 .0559 .0763 .0959 .1152 .1370	CPM .0044 .0091 .0172 .0241 .0309 .0359 .0432 .0511 .0717 .0915 .1166 .1381	0006 .0001 .0001 0003 0002 .0002 0003 .0002 .0002 .0008 .0009	.0008 .0010 .0008 .0006 .0010 .0007 .0005 .0004 .0005 .0005	L/D -1.172 3.107 6.980 8.985 10.659 11.680 11.196 8.843 7.283 6.367 5.621 5.019	CDB .0038 .0039 .0039 .0038 .0039 .0037 .0037 .0036 .0036 .0034	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933 1.6180 2.6727 9.9955 20.6142 28.7640 32.7790 30.2022 33.9775
278 279 280 281 282 283 284 285 286 287 288 289 290 291	MACH .290 .291 .292 .293 .294 .291 .291 .292 .291 .292 .292 .292 .292	116.858 117.535 118.114 118.696 119.373 118.024 117.355 117.377 117.981 117.909 117.258 117.963 117.964	BETA00000000000000	07 .94 1.93 2.97 3.95 4.99 6.06 7.08 8.14 9.18 10.26 11.32 12.41 14.57	CL 0209 .0577 .1352 .2019 .2673 .3488 .4190 .4939 .5555 .6104 .6478 .6874	CD 0178 0186 0194 0225 0251 0299 0374 0559 0763 0959 1152 1370 1611	CPM .0044 .0091 .0172 .0241 .0309 .0359 .0432 .0511 .0717 .0915 .1166 .1381 .1567	0006 .0001 .0001 0003 0002 .0002 0003 .0002 .0008 .0009 .0012 .0002 0003	.0008 .0010 .0008 .0006 .0010 .0007 .0005 .0004 .0005 .0005 .0006	L/D -1.172 3.107 6.980 8.985 10.659 11.680 11.196 8.843 7.283 6.367 5.621 5.019 4.522 3.758	CDB .0038 .0039 .0039 .0039 .0039 .0037 .0037 .0036 .0036 .0034 .0034	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933 1.6180 2.6727 9.9955 20.6142 28.7640 32.7790 30.2022 33.9775 38.2321
278 279 280 281 282 283 284 285 286 287 288 289 290 291	MACH .290 .291 .292 .291 .292 .291 .292 .291 .292 .291 .292 .292	116.858 117.535 118.114 118.696 119.373 118.024 117.355 117.377 117.981 117.999 117.258 117.993 117.993	BETA00000000000000	07 .94 1.93 2.97 3.95 4.99 6.06 7.08 8.14 9.18 10.26 11.32 12.41 14.57	CL 0209 .0577 .1352 .2019 .2673 .3488 .4190 .4939 .5555 .6104 .6478 .6874 .7286 .7961	CD .0178 .0186 .0194 .0225 .0251 .0299 .0374 .0559 .0763 .0959 .1152 .1370 .1611 .2118	CPM .0044 .0091 .0172 .0241 .0309 .0359 .0432 .0511 .0717 .0915 .1166 .1381 .1567 .1903	0006 .0001 .0001 0003 0002 .0002 0003 .0002 0003 .0009 .0012 .0009 0003 0004	.0008 .0010 .0008 .0006 .0010 .0007 .0005 .0004 .0005 .0006 .0002	L/D -1.172 3.107 6.980 8.985 10.659 11.680 11.196 8.843 7.283 6.367 5.621 5.019 4.522 3.758 3.232	CDB .0038 .0039 .0039 .0039 .0037 .0037 .0036 .0036 .0034 .0034 .0032 .0030	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933 1.6180 2.6727 9.9955 20.6142 28.7640 32.7790 30.2022 33.9775 38.2321 34.8764
278 279 280 281 282 283 284 285 286 287 290 291 292 293	MACH .290 .291 .292 .293 .294 .291 .291 .292 .291 .292 .291 .292 .291 .292 .291 .292 .291	116.858 117.535 118.114 118.696 119.373 118.024 117.355 117.377 117.981 117.909 117.258 117.963 117.994 117.385 116.034 116.060	BETA00000000000000	07 .94 1.93 2.97 3.95 4.99 6.06 7.08 8.14 9.18 10.26 11.32 12.41 14.57 16.63 18.67	CL0209 .0577 .1352 .2019 .2673 .3488 .4190 .4939 .5555 .6104 .6478 .6874 .7286 .7961 .8440	CD .0178 .0186 .0194 .0225 .0251 .0299 .0374 .0559 .0763 .0959 .1152 .1370 .1611 .2118 .2611	CPM .0044 .0091 .0172 .0241 .0309 .0359 .0432 .0511 .0717 .0915 .1166 .1381 .1567 .1903 .2175 .2299	0006 .0001 .0001 0003 0002 .0002 0003 .0002 .0008 .0009 .0012 .0002 0003 0004 0006	.0008 .0010 .0008 .0006 .0010 .0007 .0005 .0004 .0005 .0006 .0002 .0006 .0006 .0004	L/D -1.172 3.107 6.980 8.985 10.659 11.680 11.196 8.843 7.283 6.367 5.621 5.019 4.522 3.758 3.232 2.846	CDB .0038 .0039 .0039 .0039 .0037 .0037 .0036 .0034 .0034 .0034 .0032	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933 1.6180 2.6727 9.9955 20.6142 28.7640 32.7790 30.2022 33.9775 38.2321 34.8764 30.7415
278 279 280 281 282 283 284 285 286 287 288 289 290 291	MACH .290 .291 .292 .293 .294 .291 .291 .292 .291 .292 .291 .292 .291 .292 .293	116.858 117.535 118.114 118.696 119.373 118.024 117.355 117.377 117.981 117.999 117.258 117.993 117.993	BETA00000000000000	07 .94 1.93 2.97 3.95 4.99 6.06 7.08 8.14 9.18 10.26 11.32 12.41 14.57	CL 0209 .0577 .1352 .2019 .2673 .3488 .4190 .4939 .5555 .6104 .6478 .6874 .7286 .7961	CD .0178 .0186 .0194 .0225 .0251 .0299 .0374 .0559 .0763 .0959 .1152 .1370 .1611 .2118	CPM .0044 .0091 .0172 .0241 .0309 .0359 .0432 .0511 .0717 .0915 .1166 .1381 .1567 .1903	0006 .0001 .0001 0003 0002 .0002 0003 .0002 0003 .0009 .0012 .0009 0003 0004	.0008 .0010 .0008 .0006 .0010 .0007 .0005 .0004 .0005 .0006 .0002	L/D -1.172 3.107 6.980 8.985 10.659 11.680 11.196 8.843 7.283 6.367 5.621 5.019 4.522 3.758 3.232	CDB .0038 .0039 .0039 .0039 .0037 .0037 .0036 .0036 .0034 .0034 .0032 .0030	PB-1 1.5940 1.7738 1.8337 1.9296 2.1933 1.6180 2.6727 9.9955 20.6142 28.7640 32.7790 30.2022 33.9775 38.2321 34.8764

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	70 RUN= 3	36									
							S COEFFICIENT	-			PRESS.COEF	
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		AB	CAC
357	•932	736.432	01	13	0011	•0264	-0017	•0004	.0012	• 0		•0000
358	.931	735.885	01	1.04	.1043	.0266	.0320	-0004	.0015	• 0	0061 0	•0000
359	•933	737.326	00	2.25	.1987	.0294	•0032	.0003	.0008	• 0	061 0	.0000
360	• 933	137.090	01	3.43	.3045	•0289	.0024	.0004	.0020	• C	0061 0	.0000
361	.934	738.256	01	4.61	.4070	• 0294	.0022	•0004	.0016	•0	0061 0	-0000
362	.934	737.675	00	5.83	.5007	•0294	.0016	•0004	.0007	• 0	059 0	.0000
363	.936	739.255	00	7.08	•6060	.0306	.0024	•0002	.0014	• 0	0060 0	.0000
364	.936	739.544	01	8.26	.6861	.0317	.0018	.0006	.0006	•0	058 0	.0000
365	.938	140.830	01	9.46	.7613	.0324	.0029	•0006	0000			.0000
366	-940	742.423	01	10.64	.8299	.0321	.0018	.0005	.0006	• 0	0057	.0000
367	.942	744.413	01	11.92	-9452	.0334	.0048	•0007	0000			0.000
368	.932	730.560	01	06	0072	.0273	.0019	.0005	.0011			.0000
	TEST= 7	778 KUN=	36		21.42	ILITY AXIS O	OFFECTENTS			STAD	.PRESS.COEF	= <b>c</b>
POINT	MACH	ü	BETA	ALPHA	CL	CD CD	CPM	CLS	CNS	L/D	CDB	
357	•932	736.432	01	13	0010	• 0264	•0094	.0017	• 0004			PB-1
358	.932	735.885	01	1.04	.1038	• 0285				038	.0061	18.3905
	•933	137.326					• 0064	-0020	-0004	3.646	.0061	50.7586
359		737.090	00	2.25	• 1974	.0372	.0134	•0032	• 0002	5.312	-0061	49.3793
360	. 933		01	3.43	• 3022	.0470	•0127	•0024	•0002	6.424	•0060	45.7011
361	• 934	138.256	01	4.61	•4033	.0620	.0129	•0023	.0002	6.506	•0061	44.2299
362	.934	737.675	00	5.83	. 4951	.0801	.0164	.0017	•0002	6.181	.0059	60.8735
363	• 936	739.255	00	7.08	•5976	.1050	.0169	•0024	0000	5.693	•0060	125.2413
364	•936	739.544	Oi	8.26	•6744	.1299	.0157	.0019	-0003	5.190	.0058	156.6896
365	-938	740.830	01	9.46	• 7457	. 1571	.0235	.0030	.0001	4.748	.0057	139.5862
366	-940	742.423	01	10.64	.8097	.1847	.0284	.0018	•0002	4.384	.0056	143.4482
367	•942	744.413	01	11.92	.9179	.2278	•0006	.0048	0003	4.029	•0052	156.6896
368	•932	736.560	01	06	0072	•0273	•0092	.0019	• 0005	263	-0061	16.8089

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	73 RUN=	37									
							S COEFFICIEN				PRESS.CDE	
POINT	MALH	Q	BETA		CNF	CAF	CLB	CNB	CSF		CAB	CAC
418	• 86 3	684.124	01	•04	0198	.0166	.0019	•0006	.0013			0.0000
419	<b>.</b> 802	682.995	01	1.15	<b>-1030</b>	.0154	.0014	•0006	.0022	. (	0054	0.0000
420	•866	o 80.530	01	2.40	•2354	.0121	.0013	.0007	.0017	• (	0054	0.0000
421	.862	682.905	01	3.63	• 3605	.0075	.0015	.0005	.0022	• (	0053	0.0000
422	.804	684.862	01	4.72	•4730	.0076	•0023	•0004	.0021	. (	0053	0.0000
423	• 404	685.422	01	5.88	•5583	.0092	.0057	.0012	.0003	•(	0052	0.0000
424	.864	685.225	01	7.06	•6370	.0117	.0014	.0006	.0011	. (		0.0000
425	-860	686.793	01	8.17	•6789	.0132	.0081	.0016	0005			0.0000
426	.804	684.830	01	9.30	•7242	.0129	.0066	.0017	.0001			0.0000
427	.805	085.870	01	10.35	.7336	.0172	.0090	.0018	0008			0.0000
428	.862	683.664	01	11.42	•7316	.0215	.0091	.0019	0012			0.0000
429	-862	683.316	01	21	0237	.0163	.0015	•0007	.0027			0.0000
	TEST= 7	18 RUN=	37									
						ILITY AXIS C					PRESS.COE	FF
POINT	MACH	J	BETA	ALPHA	CL	Cυ	CPM	CLS	ČNS	L/D	CDB	P8-1
418	• 803	o 84 • 124	01	•04	-•0198	.0166	.0104	.0019	.0006	-1.196	•0054	12.9837
419	-862	082.995	01	1.15	· 1027	.0175	.0119	.0014	-0006	5.878	.0054	12.5791
420	.866	086.530	01	2.40	<ul><li>2347</li></ul>	-0219	.0078	.0013	.0006	10.713	.0054	17.3239
421	-862	o 82.905	01	3.63	-3593	.0303	.0021	.0016	.0004	11.863	.0053	19.4939
422	.864	684.882	01	4.72	• 4708	.0465	.0014	.0023	.0002	10.125	.0053	28.6896
423	-804	685.422	01	5.88	• 5544	.0663	-0162	•0058	.0006	8.356	.0052	105.9316
424	.864	685.225	01	7.06	•6307	.0898	.0387	.0014	.0004	7.020	.0051	65.4716
425	.860	686.793	01	8.17	.6702	.1095	•057ช	.0082	•0005	6.121	.0051	91.9545
426	.864	684.830	01	9.30	.7126	.1298	.0766	.0068	.0006	5.492	•0050	106.4833
427	•805	085.870	01	10.35	.7186	.1487	•0986	.0092	.0002	4.833	•0050	124.3225
428	.862	683.664	01	11.42	.7129	.1659	•1141	.0093	.0001	4.297	•0050	120.0000
429	.802	683.315	01	21	0236	.0164	.0100	.0015	.0007	-1.439	•0053	
		2030310			•0230	*0107	•0100	•0013	• 0001	-10427	• 0003	13.6458

TEST= 778 KUN= 38

BETA ALPHA

CNF

PUINT

#### TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

CAF

BODY AXIS COEFFICIENTS

CLB

CNB

CSF

BODY PRESS.COEFF

CAC

CAB

PUINT	MACH	ð,	BEIA	ALPHA	CNF	CAF	CLB	CNR	CZE		AB	CAC
444	• 806	032.344	01	-•18	0255	•0165	.0012	•0006	.0011			.0000
445	-806	632.418	01	•99	•0820	.0154	.0013	•0006	.0015	• 0	049 (	0.0000
446	.806	032.571	01	2.13	.1951	.0114	.0013	•0006	.0009	•0	049 (	0.000
447	408e	632.732	00	3.37	.3100	.0042	.0013	.0005	.0004	•0	049	.0000
448	.834	031.353	01	4.54	•4239	0037	.0012	.0005	.0010	• 0	049 (	0.0000
449	•806	633.118	00	5.76	• 5405	0075	.0004	.0004	.0011	.0	049 (	.0000
450	• მეი	633.351	00	6.93	•6051	0050	.0012	.0005	.0005	• 0	048 (	0.0000
451	a08.	033.021	01	8.06	-6584	0024	.0067	.0018	0008	•0	048 (	0.0000
452	-806	633.329	01	9.17	•6920	•0033	.0075	.0018	0013	•0	047	0.000
453	•80₫	634.548	00	10.24	.7374	.0063	0019	.0005	.0004	•0	047	0.000
454	.808	634.378	01	11.36	.7419	-0142	.007B	.0018	0027	•0	046 (	0.000
455	- 80 ខ	634.984	00	12.43	•7447	.0206	-0015	.0007	0002	• 0	046	0.000
456	.308	610.018	00	13.57	.7672	.0239	.0005	.0005	0007	• 0	046	0.0000
457	-810	036.461	00	15.82	.8334	•0266	.0002	.0008	0012	• 0	044	0.0000
458	.810	030.770	01	18.01	.9107	.0276	•0006	.0014	0032	•0	041	0.0000
459	.812	638.680	00	20.11	.9863	•0289	.0001	.0014	0064	• 0	035	0.0000
460	.815	640.771	•00	22.32	1.0944	.0273	0006	-0016	0099	• 0	026	0.000
461		633.846	00	5.83	•5490	0067	.0004	.0003	.0010			0.0000
	TEST= 7	78 RUN=	38		STAH	ILITY AXIS C	OFFEIGIENTS			STAR.	PRESS.COE	= <b>£</b>
TAIDA	MACH	J	BETA	ALPHA	CL	co	CPM	CLS	CNS	L/D	CDB	PB-1
444	.806		01	18	0255	.0166	.0089	.0012	.0006	-1.534	.0049	12.0642
445	-806	632.418	01	•99	.0817	.0168	.0129	.0013	.0006	4.856	.0049	12.4320
446	.806	032.571	01	2.13	. 1945	.0186	.0155	.0014	.0006	10.443	.0049	12.5055
447	-806	632.132	00	3.37	.3092	.0224	.0164	.0013	.0004	13.786	.0049	12.8733
448	-804	631.353	01	4.54	•4228	.0298	-0191	.0012	.0004	14.171	.0049	16.5147
449	•806	633.118	00	5.76	•5385	.0467	.0242	.0004	.0004	11.526	.0048	30.7860
450	•806	633.351	00	6.93	•6013	.0681	.0502	•0012	.0004	8.826	.0048	56.3678
451	• 80b	633.021	01	8.06	•6522	.0899	.0717	.0069	.0009	7.257	•0047	78.3452
452	• 800	633.329	01	9.17	•6826	.1136	• 0949	.0077	.0006	6.009	.0047	102.9890
453	.808	634.548	00	10.24	·7245	.1373	.0888	0018	.0009	5.277	.0046	124.1386
454	-808	634.378	01	11.36	• 7246	.1600	.1250	.0080	.0002	4.530	.0046	187-5841
455	•808	634.984	00	12.43	•7228	.1805	.1590	.0016	.0003	4.005	• 0045	160.3660
450	• 808	635.018	00	13.57	• 7402	.2032	.1686	•0006	.0004	3.642	•0045	105.5620
457	-010	636.461	00	15.82	• 7945	. 2527	.1840	.0005	.0007	3.144	.0042	101.1499
458	-810	636.770	01	18.01	. 8575	.3079	.1878	.0010	.0011	2.785	.0039	104.0925
459	-812		00	20.11	.9162	.3663	.1847	•0006	.0013	2.501	.0033	124.3205
460	-815	640.771	•00	22.32	1.0020	•4408	.1950	.0001	.0017	2.273	.0024	157.0557
461	.807	633.840	00	5.83	• 5469	• 0492	.0239	•0004	.0003	11.124	•0048	30.8963

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	39									
							S COEFFICIEN				PRESS.COE	FF
TAIDS	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNR	CSF	(	CAB	ÇAC
475	.754	582.493	01	12	0239	.0164	.0010	.0006	.0015			0.0000
476	.754	582.494	01	• 96	.0732	•0156	.0014	•0006	.0018	•1	0047	0.0000
477	.753	581.527	01	2.13	.1767	.0119	.0015	.0005	.0011			0.0000
478	.754	582.733	00	3.28	-2810	-0052	.0013	•0005	.0007	• (	0047	0.0000
479	.753	581.705	00	4.43	.3820	0029	.0005	.0003	.0008	-(	0047	0.0000
480	<b>.</b> 756	584.456	00	5.63	<b>.</b> 4809	0116	.0006	.0003	.0013	. (	0047	0.0000
481	•754	582.645	01	6.80	•5717	0122	.0028	.0013	0002	. (	0047	0.0000
482	•755	583.947	01	7.96	•6349	0101	.0069	•0020	0011			0.0000
483	.753	581.611	01	9.07	•6744	0052	.0079	.0021	0017	•1	0045	0.0000
484	.754	582.969	01	10.12	.7057	.0013	.0086	.0022	0019	•1	0045	0.0000
485	. 756	584.816	01	11.27	.7171	.0105	.0017	.0007	.0009		0045	0.0000
486	.750	585.279	00	12.34	•7444	•0152	.0004	.0005	.0002	. (	0044	0.0000
487	.755	584.149	00	13.46	.7630	.0188	.0003	.0004	.0012			0.0000
488	•755	584.418	00	15.70	.8249	.0234	.0000	.0006	0006	-1		0.0000
489	•757	585.719	01	17.85	-8835	.0255	.0000	.0014	0035	- (	0041	0.0000
490	.757	585.931	00	19.97	•9590	.0273	.0002	.0015	0039	• (		0.0000
491	.761	589.283	•00		1.0496	.0265	0005	.0015	0088			0.0000
492	. 755	583.410	01	12	0255	.0164	.0017	.0006	.0021	• (	0047	0.0000
	TEST= 7	78 RUN=	39		(TA)	THE AVEC O	DEFERGRENTS.			67.0	P0556 695	
0071.7				41.0114		ILITY AXIS C		61.6	511.0		.PRESS.COE	
POINT	MACH	Q (0)	RETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
475	.754	582.493	01	12	0239	.0165	•0079	.0010	.0006	-1.449	•0047	10.6288
476	.754	582.494	01	•96	.0730	.0168	.0129	•0014	• 0006	4.336	.0047	13.2779
477	.753	581.527 582.733	01	2.13	.1761	.0184 .0213	.0158 .0209	.0015 .0013	.0005	9.547	-0047	10.4826
478	.754 .753	581.705	00	3.28	.2002 .3811	.0266	.0270	.0005	.0004 .0003	13.142	•0047	10.8136
479	• 756	584.456	00	4.43	•4797	.0356	.0309	.0006	.0003	14.336 13.464	.0047 .0047	11.3653 14.7860
480 481	• 754	582.645	00 01	5.63 6.80	•5691	.0555	.0457	•0029	.0002	10.254	.0047	37.3333
	.755	583.947	01	7.95	.6302	•0779	.0668	•0071	.0010	8.094	.0046	60.5977
482 483	•155 •753	581.611	01	9.07	•6668	.1012	•0924	.0071	.0008	6.586	•0045	77.6096
484	• 755 • 754	582.969	01	10.12	•6945	.1253	.1128	•0089	.0007	5.543	•0045	100.2304
	.756	584.816	01	11.27	.7012	.1505	•1499	•0018	.0007	4.659	•0044	180.5957
485	• 756 • 756	585.279	00	12.34	.7239	.1739	.1669	•0005	•0004	4.162	•0044	110.8971
486	• 755	584.149		13.46	• 7377	.1959	.1782	•0004	.0003	3.765	•0043	97.6557
487 488	.755	584.418	00 00	15.70	.7878	• 1959 • 2457	.1961	.0002	•0006	3.206	•0043	90.6671
489	.757	585.719	01	17.85	.8331	• 2952	.2008	.0002	•0014	2.823	•0041	86.6211
490	.757	585.931	00	19.97	•8920	• 3532	.1997	.0007	.0014	2.526	•0039	98.5752
491	.761	589.283	•00	22.10	•9625	•4194	.2055	.0001	.0016	2.295	•0025	118.2535
492	.755	583.410	01	12	0254	.0165	.0084	.0017	.0006	-1.543	•0047	10.8127
	-1,	- 034 140						,				

TEST= 778 RUN= 39

	TEST= 7	78 RUN=	40												
						BODY AXI	S COEFFICIEN	TS	BODY PRESS.COErF						
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC			
506	<b>-7</b> 02	530.006	01	11	0216	.0164	.0015	.0007	.0013			0.0000			
507	-701	529.460	01	•98	.0743	.0156	.0018	.0006	.0018			0.0000			
508	.701	529.543	01	2.10	.1697	.0122	.0013	•0006	.0017			0.0000			
509	-702	<b>&gt;30.722</b>	00	3.26	•2692	.0059	.0012	•0006	.0012			0.0000			
510	-702	529.719	00	4.34	.3588	0018	-0010	.0004	.0008			0.0000			
511	.701	529.360	00	5.52	•4522	0114	•0006	.0004	.0018			0.0000			
512	•703	531.649	00	6.67	-5431	0170	.0007	•0006	.0010			0.0000			
513	•701	529.215	01	7.82	<b>-</b> 6052	0122	•0045	.0018	0004			0.0000			
514	.705	533.688	01	8.92	•6484	0051	.0079	.0022	0018			0.0000			
515	-701	529.531	01	9.99	<b>-6853</b>	•0004	.0087	•0025	0019			0.0000			
516	-702	529.880	01	11:12	-7158	.0068	-0044	.0012	0004			0.0000			
517	•703	531.056	00	12.22	.7426	.0109	•0002	.0005	.0013			0.0000			
518	-704	531.934	00	13.36	.7688	.0143	0001	.0004	.0010			0.0000			
519	•704	532.438	00	15.58	-8215	•0202	0001	.0007	0012			0.0000			
520	-703	531.597	00	17.70	.8807	.0230	0000	.0013	0031			0.0000			
521	• 704	532.388	01	19.81	.9432	•0260	0001	.0016	0032			0.0000			
522	-706	533.963	01	21.86	.9997	.0257	.0004	.0014	0026			0.0000			
523	•702	530.228	01	11	0196	.0164	.0014	•0006	.0027			0.0000			
	TEST= 7	78 RUN=	40		CTA0	ILITY AVIC O	0155161555								
POINT	MACH	٥	BÉTA	ALPHA	CL	ILITY AXIS C					.PRESS.COE				
506	•702	530.006	01	11	0216	CD	CPM	CLS	CNS	L/D	CDB	PB-1			
507	•701	529.460	01	•98	.0740	•0165	-0084	•0015	.0007	-1.309	.0045	11.2357			
508	.701	529.543	01	2.10	.1691	•0168	-0135	•0018	• 0006	4.397	-0045	11.5667			
.509	•702	530.722	01	3.26	• 1691 • 2684	•0184	.0177	.0013	•0006	9.199	• 0045	11.3285			
510	•702	529.719	00	4.34	• 3579	•0212 •0254	.0217	.0012	.0005	12.660	•0045	11.2182			
511	•701	529.360	00	5.52	• 4512	•0254	•0284 •0363	•0010	• 0004	14.112	• 0045	11.2550			
512	•703	531.649	00	6.67	• 5414	•0462	•0440	•0006	.0003	14.031	•0045	10.0412			
513	•701	529.215	01	7.82	.6012	.0703		•0008	•0005	11.711	•0044	16.2204			
514	•705	533.688	01	8.92	.6413	•0955	.0647 .0919	-0047	•0012	8-555	.0044	50.7586			
515	•701	529.537	01	9.99	•6749	•1192		-0081	.0010	6.714	.0043	74.2992			
516	•702	529.880	01	11.12	.7010		•1116	.0090	.0010	5.661	-0042	91.5867			
517	•703	531.056	00	12.22		• 1448 1. 70	-1414	•0046	•0004	4.842	.0042	222.5263			
518	•703	531.934	00	13.36	•7234 •7447	.1679	-1691	.0003	.0005	4.309	.0041	100-4127			
519	•704	532.438	00	15.58	• 7447 • 7859	•1916 2600	-1826	•0000	.0004	3.887	.0041	94.5292			
520	•704	531.597	00	17.70	• 1859 • 8320	• 2400	.2021	.0001	-0006	3.275	•0040	93.2419			
521	•704	532.388	01	19.81	• 8320 • 8785	•2896 •3441	-2109	•0004	•0012	2.873	-0037	84.4142			
522	•706	533.963	01	21.86	.9182		.2081	-0005	-0015	2.553	.0032	90.8510			
523	•702	530-228	01	11	0196	•3962	•20 <b>76</b>	•0009	.0011	2.318	•0026	109-9776			
,,,	• 102	2300220	-•01	-•11	0170	-0164	.0086	.0014	.0007	-1.191	•0045	10.6288			

POINT   MACH   U   BETA   ALPHA   CNF   CAF   CLB   CNS   CNS   CAS   CAC		1E51= 7	78 RUN=	41			bUDY AXI	S COEFFICIEN	TS		BODY	PRESS.COE	FF
1.497   312,041  01  05  026   .0169   .0008   .0007   .0038   .0040   .00000	POINT	масн	Lì	6FTA	AI PHA	CNF	CAF	CLB	CNB	C SF	(	CAB	CAC
13								.0008	.0007	.0038	•	0040	0.0000
1.39								.0011	.0006	.0029		0040	0.0000
540												0040	0.0000
\$41													
311.09900 5.20 38.090071 .0005 .0002 .0014 .0040 0.0000   344 .498 312.35500 6.28 .4993 .0179 .0000 .0002 .0014 .0040 0.0000   344 .498 313.48500 7.37 .53470298 .0004 .0004 .0027 .0039 0.0000   345 .498 313.88100 8.48 .01510312 .0010 .00130007 .0039 0.0000   347 .497 312.66100 9.54 .66410220 .0010 .0003 .0007 .0038 0.0000   348 .498 313.8300 10.66 .69160094 .0005 .00040001 .0038 0.0000   349 .497 312.50400 11.73 .72550039 .0003 .00040001 .0038 0.0000   349 .497 312.50400 11.73 .72550039 .0003 .00040009 .0038 0.0000   350 .497 312.50400 12.83 .7586 .0010 .0002 .0003 .00040009 .0038 0.0000   351 .495 309.91400 15.06 .8297 .0082 .0001 .00050025 .0036 0.0000   352 .497 312.5400 17.16 .8914 .01550001 .00090032 .0034 0.0000   353 .499 313.82800 19.27 .9339 .0171 .0003 .00150041 .0032 0.0000   354 .499 314.42100 21.31 .9884 .0197 .0002 .0016 .0006 .0008 .0007 .0000   355 .499 311.77500080220 .0174 .0012 .0006 .0012 .0006 .0025 0.0000   356 .499 311.77500080220 .0174 .0012 .0006 .0012 .0006 .0008   357 .499 314.40300 .99 .0020 .0174 .0012 .0006 .0012 .0006 .0008   358 .498 313.42800 .99 .0020 .0174 .0012 .0006 .0012 .0006 .0008   359 .499 314.80500 .412 .2999 .0233 .0275 .0006 .0000 .0006 .7546 .0040 .0031 .0006 .7546 .0040 .0031 .0006 .7546 .0040 .0009 .0000   359 .499 314.80500 .412 .2999 .0233 .0275 .0034 .0000 .0006 .7546 .0040 .0031 .0066 .7546 .0040 .0031 .0066 .7546 .0040 .0031 .0066 .7546 .0040 .0031 .0066 .7546 .0040 .0031 .0060 .7546 .0040 .0031 .0060 .7546 .0040 .0031 .0060 .7546 .0040 .0031 .0060 .7546 .0040 .0031 .0060 .7546 .0040 .0031 .0060 .7546 .0040 .0051 .0060 .0													
A													
A-98   313-4-95   -0.00   7.37   -0.5347   -0.0298   .0004   .0004   .0007   .0040   .00000   .545   .498   313-4-95   -0.00   8.498   .0151   -0.0312   .0010   .00013   -0.0007   .0038   0.0000   .547   .498   313-6-93   -0.00   .00-5   .6641   -0.0220   .0010   .0003   .0007   .0038   0.0000   .548   .497   312-2-51   -0.00   .00-5   .6641   -0.0220   .0010   .0003   .0004   -0.0011   .0038   0.0000   .549   .497   312-504   -0.00   .173   .7255   -0.039   .0003   .0004   -0.0001   .0038   0.0000   .549   .497   312-2-504   -0.00   .12-83   .7586   .0010   .0002   .0003   -0.0014   .0037   0.0000   .559   .497   312-2-50   -0.00   .297   .0082   .00010   .0005   -0.0025   .0036   0.0000   .551   .495   309-914   -0.00   15-06   .297   .0082   .0001   .0005   -0.0025   .0036   0.0000   .553   .497   313-2-8   -0.00   17-10   .9914   .0155   -0.001   .0009   -0.032   .0034   0.0000   .553   .497   313-2-8   -0.00   17-10   .9914   .0155   -0.001   .0009   -0.0032   .0034   0.0000   .555   .497   311-775   -0.00   .21-31   .9844   .0197   .0002   .0016   -0.005   .0025   .0036   0.0000   .555   .497   311-775   -0.00   -0.08   -0.020   .0174   .0012   .0006   .0012   .0040   0.0000   .0000   .555   .497   311-775   -0.00   -0.08   -0.020   .0174   .0012   .0006   .0012   .0040   0.0000   .00000   .00000   .0000   .00000   .00000   .00000   .00000   .0000   .00000   .													
STAB_PRESS_COEFF   STAB_PRESS_													
1													
Test= //8 Run= 41													
11.73													
TEST=   18   NUN=   41	548												
Test   18   Rune   41     Stability axis cuefficients   Stab   Peter	549	.497		00									
Test= //8 run= 41	550	•497	312.084										
TEST=   178 RUN=   41   STABILITY AXIS CUEFFICIENTS   STAB-PRESS-CUEFF	551	.495	309.914	00	15.06								
TEST= /18 RUN= 41  STABILITY AXIS CUEFFICIENTS  POINT MACH U BETA ALPHA CL CD CPM CLS CNS L/D CDB PB-1 537 .97 \$12.04101050220 .0174 .0012 .0006 .0007 -1.334 .0040 11.0711 539 .497 312.22200 .98 .0620 .0174 .0132 .0012 .0006 7.546 .0040 11.4717 539 .497 312.22200 2.00 .1393 .0185 .0163 .0010 .0006 7.546 .0040 8.5332 540 .498 313.40500 3.09 .2235 .0206 .0215 .0015 .0005 3.570 .0040 8.5332 541 .498 313.40500 3.09 .2235 .0206 .0215 .0015 .0005 10.853 .0040 8.1286 542 .499 314.03900 5.20 .3800 .0275 .0346 .0005 .0006 .0008 12.852 .0040 7.2091 543 .498 313.40500 5.20 .3800 .0275 .0346 .0005 .0001 .0006 13.838 .0039 5.5903 544 .498 313.40500 5.20 .3800 .0275 .0346 .0005 .0002 13.838 .0039 5.5903 545 .498 313.40500 5.20 .3800 .0275 .0346 .0005 .0002 13.838 .0039 5.5903 546 .498 313.34100 8.48 .6130 .0599 .0560 .0012 .0011 .0020 14.123 .0040 6.4793 547 .498 313.34100 8.48 .6130 .0599 .0560 .0012 .0011 .0020 14.123 .0040 6.4793 549 .498 313.34100 8.48 .6130 .0599 .0560 .0012 .0011 .0020 14.123 .0039 6.8959 545 .498 313.34100 8.48 .6130 .0599 .0560 .0012 .0011 .0020 14.123 .0039 6.8959 546 .498 313.34100 8.48 .6130 .0599 .0560 .0012 .0011 .0020 14.123 .0039 6.8959 547 .497 312.26100 9.54 .6586 .0885 .0824 .0011 .0001 7.445 .0038 83.4947 548 .498 313.63300 10.66 .6814 .1187 .1234 .0006 .0003 5.741 .0037 82.9430 550 .497 312.36400 11.73 .7111 .1437 .1510 .0004 .0003 3.5764 .0037 82.9430 550 .497 312.50400 11.73 .7111 .1437 .1510 .0004 .0003 3.576 .0034 83.7476 551 .495 319.91400 12.83 .7395 .1095 .1704 .0002 .0003 3.576 .0034 87.7476 552 .497 312.50400 11.36 .8478 .2760 .2226 .0001 .0009 3.072 .0033 88.2763 553 .499 313.82400 17.16 .8478 .2760 .2226 .0001 .0009 3.072 .0033 88.2763 553 .499 313.82400 19.27 .8760 .3243 .2229 .0007 .0014 2.701 .0030 71.9084	552	.497	312.543	00	17.16	.8914	•0135						
TEST= /18 RUN= 41  TEST= /18 RUN= 41  STABILITY AXIS CUEFFICIENTS  POINT MACH WETA ALPHA CL CD CPM CLS CNS L/D CDB PB-1 537 .90 12.041 -0.01 -0.05 .00000 .0000 .00000 .00000 .00000 .0000 .00000 .0000 .0000 .0000 .0000 .00000 .00000 .00000 .	553	•499	313.828	00	19.27	•9339	.0171	.0003	•0015				
TEST= ///8 RUN= 41  STABILITY AXIS CUEFFICIENTS  POINT MACH U BETA ALPHA CL CD CPM CLS CNS L/D CD8 P8-1 537 .497 312.04101050226 .0169 .0066 .0008 .0007 -1.334 .0040 11.0711 538 .498 313.28200 .98 .0020 .0174 .0132 .0012 .0005 3.570 .0040 11.4757 539 .497 312.22200 2.00 .1393 .0185 .0163 .0010 .0006 7.546 .0040 8.5332 540 .498 313.40500 3.09 .2235 .0206 .0215 .0015 .0005 10.883 .0040 8.1286 541 .498 313.40500 4.12 .2999 .0233 .0272 .0004 .0003 12.882 .0040 7.2091 543 .498 312.85500 6.28 .4585 .0325 .0391 .0001 .0002 13.838 .0039 5.5903 543 .498 313.48500 7.37 .5341 .0390 .0473 .0005 .0002 13.838 .0039 6.8959 544 .498 313.4381 .008 .848 .6130 .0599 .0560 .0012 .0011 .0002 14.123 .0040 6.4729 544 .498 313.4381 .008 .48 .6130 .0599 .0560 .0012 .0011 .0002 14.123 .0040 6.4729 544 .498 313.33400 7.37 .5341 .0390 .0473 .0005 .0004 13.702 .0039 6.8959 545 .499 313.331 .008 .48 .6130 .0599 .0560 .0012 .0011 .0022 14.123 .0040 6.4729 544 .498 313.336 .00 10.66 .6814 .1187 .1234 .0006 .0003 5.741 .0037 82.9430 549 .497 312.50400 11.73 .7111 .1437 .1510 .0004 .0003 5.745 .0038 83.4947 549 .497 312.50400 11.73 .7111 .1437 .1510 .0004 .0003 4.948 .0037 72.2762 550 .497 312.00400 11.73 .7111 .1437 .1510 .0004 .0003 4.948 .0037 72.2762 550 .497 312.00400 11.73 .7111 .1437 .1510 .0004 .0003 3.576 .0034 89.7476 552 .499 313.82800 19.27 .8760 .3243 .2329 .0007 .0014 2.701 .0033 88.2763 553 .499 313.82800 19.27 .8760 .3243 .2329 .0007 .0015 2.720 .0034 79.6326 553 .499 313.82800 19.27 .8760 .3243 .2329 .0007 .0016 2.701 .0030 .0024 79.6326 554 .499 313.82800 19.27 .8760 .3243 .2329 .0007 .0016 2.701 .0030 .0024 .79.6326 553 .499 313.82800 19.27 .8760 .3243 .2329 .0007 .0016 2.701 .0030 .0024 .79.6326 554 .499 313.82800 19.27 .8760 .3243 .2329 .0007 .0016 2.701 .0030 .0024 .79.6326		.479	314.421	00	21.31	•9884	.0197	.0002	.0016				
TEST= //8 RUN= 41  STABILITY AXIS COEFFICIENTS  POINT MACH		.497	311.775	00	08	0220	.0174	.0012	.0006	.0012	•	0040	0.0000
POINT MACH		TEST= /	18 KUN=	41		STAR	ILITY AYIS C	DEFEICIENTS			STAR.	.PRESS.COE	FF
537         .497         312.041        01        05        0026         .0169         .0066         .0008         .0007         -1.334         .0040         11.0711           538         .498         313.282        00         .98         .0020         .0174         .0132         .0012         .0005         3.570         .0040         11.4757           539         .497         312.222        00         2.00         .1393         .0185         .0163         .0010         .0006         .7546         .0040         8.5332           540         .498         313.405        00         3.09         .2235         .0206         .0215         .0015         .0005         10.853         .0040         8.5332           541         .498         .313.405        00         4.12         .2999         .0233         .0272         .0004         .0003         12.852         .0040         7.2091           542         .499         .314.085        00         .520         .3800         .0275         .0346         .0005         .0002         13.838         .0039         .55903           543         .498         .313.485        00         7.37         .5341<	TIALOR	MACH	. •	HETA	ALDHA				CLS	CNS			
538         .498         313.282        00         .98         .0020         .0174         .0132         .0012         .0005         3.570         .0040         11.4757           539         .497         312.222        00         2.00         .1393         .0185         .0163         .0010         .0006         7.546         .0040         8.5332           540         .498         313.463        00         3.09         .2235         .0206         .0215         .0015         .0005         10.853         .0040         8.5332           541         .498         313.465        00         4.12         .2999         .0233         .0272         .0004         .0003         12.852         .0040         7.2091           542         .499         314.089        00         5.20         .3800         .0275         .0346         .0005         .0002         13.838         .0039         5.5903           543         .498         312.855        00         6.28         .4585         .0325         .0391         .0001         .0002         14.123         .0040         6.4729           544         .498         313.485        00         7.37         .5341													
539         .497         312.222        00         2.00         .1393         .0185         .0163         .0010         .0006         7.546         .0040         8.5332           540         .498         313.463        00         3.09         .2235         .0206         .0215         .0015         .0005         10.853         .0040         8.1286           541         .498         .313.465        00         4.12         .2999         .0233         .0272         .0004         .0003         12.852         .0040         7.2091           542         .499         .14.089        00         5.20         .3800         .0275         .0346         .0005         .0002         13.838         .0039         5.5903           543         .498         .312.855        00         .6.28         .4585         .0325         .0391         .0001         .0002         14.123         .0040         .64729           544         .498         .313.485        00         7.37         .5341         .0390         .0473         .0005         .0004         13.702         .0039         6.8959           545         .499         .313.381        00         7.546         .088													
540         .448         313.463        00         3.09         .2235         .0206         .0215         .0015         .0005         10.853         .0040         8.1286           541         .498         313.465        00         4.12         .2999         .0233         .0272         .0004         .0003         12.852         .0040         7.2091           542         .499         314.089        00         5.20         .3800         .0275         .0346         .0005         .0002         13.838         .0039         5.5903           543         .498         312.855        00         6.28         .4585         .0325         .0391         .0001         .0002         14.123         .0040         6.4729           544         .498         313.485        00         7.37         .5341         .0390         .0473         .0005         .0004         13.702         .0039         6.8959           545         .498         313.381        00         8.48         .6130         .0599         .0560         .0012         .0011         10.240         .0039         21.7378           547         .497         312.261        00         9.54         .6586 <td></td>													
541         .498         313.465        00         4.12         .2999         .0233         .0272         .0004         .0003         12.852         .0040         7.2091           542         .499         314.089        00         5.20         .3800         .0275         .0346         .0005         .0002         13.838         .0039         5.5903           543         .498         312.855        00         6.28         .4585         .0325         .0391         .0001         .0002         14.123         .0040         6.4729           544         .498         313.485        00         7.37         .5341         .0390         .0473         .0005         .0004         13.702         .0039         6.8859           545         .498         313.381        00         8.48         .6130         .0599         .0560         .0012         .0011         10.240         .0039         21.7378           547         .497         312.261        00         9.54         .6586         .0885         .0824         .0011         .0001         7.445         .0038         83.4947           549         .497         312.504        00         11.73         .7111 </td <td></td>													
542         .499         314.089        00         5.20         .3800         .0275         .0346         .0005         .0002         13.838         .0039         5.5903           543         .498         312.855        00         6.28         .4585         .0325         .0391         .0001         .0002         14.123         .0040         6.4729           544         .498         313.485        00         7.37         .5341         .0390         .0473         .0005         .0004         13.702         .0039         6.8959           545         .498         313.481        00         8.48         .6130         .0599         .0560         .0012         .0011         10.240         .0039         21.7378           547         .497         312.261        00         9.54         .6586         .0885         .0824         .0011         .0001         7.445         .0038         83.4947           543         .498         313.63d        00         10.66         .6814         .1187         .1234         .0006         .0003         5.741         .0037         82.9430           549         .497         312.504        00         11.73         .7111<													
543         .498         312.855         -00         6.28         .4585         .0325         .0391         .0001         .0002         14.123         .0040         6.4729           544         .498         313.485         -00         7.37         .5341         .0390         .0473         .0005         .0004         13.702         .0039         6.8959           545         .498         313.381         -00         8.48         .6130         .0599         .0560         .0012         .0011         10.240         .0039         21.7378           547         .497         312.261         -00         9.54         .6586         .0885         .0824         .0011         .0001         7.445         .0038         83.4947           543         .498         313.63d        00         10.66         .6814         .1187         .1234         .0006         .0003         5.741         .0037         82.9430           549         .497         312.504        00         11.73         .7111         .1437         .1510         .0004         .0003         5.741         .0037         72.2762           550         .497         312.084        00         12.83         .7395 <td></td>													
544         .498         313.485        00         7.37         .5341         .0390         .0473         .0005         .0004         13.702         .0039         6.8959           545         .498         313.381        00         8.48         .6130         .0599         .0560         .0012         .0011         10.240         .0039         21.7378           547         .497         312.261        00         9.54         .6586         .0885         .0824         .0011         .0001         7.445         .0038         83.4947           548         .498         313.638        00         10.66         .6814         .1187         .1234         .0006         .0003         5.741         .0037         82.9430           549         .497         312.504        00         11.73         .7111         .1437         .1510         .0004         .0003         4.948         .0037         72.2762           550         .497         312.084        00         12.83         .7395         .1695         .1704         .0002         .0003         4.363         .0036         81.6556           551         .495         309.914        00         15.06         .799													
545         .498         313.381        00         8.48         .6130         .0599         .0560         .0012         .0011         10.240         .0039         21.7378           547         .497         312.261        00         9.54         .6586         .0885         .0824         .0011         .0001         7.445         .0038         83.4947           548         .498         313.638        00         10.66         .6814         .1187         .1234         .0006         .0003         5.741         .0037         82.9430           549         .497         312.504        00         11.73         .7111         .1437         .1510         .0004         .0003         4.948         .0037         72.2762           550         .497         312.504        00         12.83         .7395         .1695         .1704         .0002         .0003         4.948         .0037         72.2762           551         .495         309.914        00         15.06         .7990         .2235         .2011         .0003         .0005         3.576         .0034         89.7476           552         .497         312.543        00         17.16         .84	543												
547         .497         312.261        00         9.54         .6586         .0885         .0824         .0011         .0001         7.445         .0038         83.4947           548         .498         313.638        00         10.66         .6814         .1187         .1234         .0006         .0003         5.741         .0037         82.9430           549         .497         312.504        00         11.73         .7111         .1437         .1510         .0004         .0003         4.948         .0037         72.2762           550         .497         312.084        00         12.83         .7395         .1695         .1704         .0002         .0003         4.363         .0036         81.6556           551         .495         309.914        00         15.06         .7990         .2235         .2011         .0003         .0005         3.576         .0034         89.7476           552         .497         312.543        00         17.16         .8478         .2760         .2226         .0001         .0009         3.072         .0033         88.2763           553         .499         314.421        00         21.31         .91	544												
548         .498         313.638        00         10.66         .6814         .1187         .1234         .0006         .0003         5.741         .0037         82.9430           549         .497         312.504        00         11.73         .7111         .1437         .1510         .0004         .0003         4.948         .0037         72.2762           550         .497         312.084        00         12.83         .7395         .1695         .1704         .0002         .0003         4.363         .0036         81.6556           551         .495         309.914        00         15.06         .7990         .2235         .2011         .0003         .0005         3.576         .0034         89.7476           552         .497         312.543        00         17.16         .8478         .2760         .2226         .0001         .0009         3.072         .0033         88.2763           553         .499         313.82d        00         19.27         .8760         .3243         .2329         .0007         .0014         2.701         .0030         71.9084           554         .499         314.421        00         21.31         .9	545	.498	313.381										
549     .497     312.504    00     11.73     .7111     .1437     .1510     .0004     .0003     4.948     .0037     72.2762       550     .497     312.084    00     12.83     .7395     .1695     .1704     .0002     .0003     4.363     .0036     81.6556       551     .495     309.914    00     15.06     .7990     .2235     .2011     .0003     .0005     3.576     .0034     89.7476       552     .497     312.543    00     17.16     .8478     .2760     .2226     .0001     .0009     3.072     .0033     88.2763       553     .499     314.82d    00     19.27     .8760     .2243     .2329     .0007     .0014     2.701     .0030     71.9084       554     .499     314.421    00     21.31     .9136     .3776     .2317     .0008     .0015     2.420     .0024     79.6326	547	•497	312.261	00	9.54								
550 .497 312.08400 12.83 .7395 .1695 .1704 .0002 .0003 4.363 .0036 81.6556 551 .495 309.91400 15.06 .7990 .2235 .2011 .0003 .0005 3.576 .0034 89.7476 552 .497 312.54300 17.16 .8478 .2760 .2226 .0001 .0009 3.072 .0033 88.2763 553 .499 313.82d00 19.27 .8760 .3243 .2329 .0007 .0014 2.701 .0030 71.9084 554 .499 314.42100 21.31 .9136 .3776 .2317 .0008 .0015 2.420 .0024 79.6326	548	.478	313.638	00	10.66	-6814							
551	549	.497	312.504	00	11.73	.7111							
551     .495     309.914    00     15.06     .7990     .2235     .2011     .0003     .0005     3.576     .0034     89.7476       552     .497     312.543    00     17.16     .8478     .2760     .2226     .0001     .0009     3.072     .0033     88.2763       553     .499     313.828    00     19.27     .8760     .3243     .2329     .0007     .0014     2.701     .0030     71.9084       554     .499     314.421    00     21.31     .9136     .3776     .2317     .0008     .0015     2.420     .0024     79.6326	550	.497	312.084	00	12.83	.7395	.1695			.0003			
552     .497     312.543    00     17.16     .8478     .2760     .2226     .0001     .0009     3.072     .0033     88.2763       553     .499     313.828    00     19.27     .8760     .3243     .2329     .0007     .0014     2.701     .0030     71.9084       554     .499     314.421    00     21.31     .9136     .3776     .2317     .0008     .0015     2.420     .0024     79.6326				00	15.06	.7990	.2235	.2011	.0003	•0005			
553 .499 313.82d00 19.27 .8760 .3243 .2329 .0007 .0014 2.701 .0030 71.9084 554 .499 314.42100 21.31 .9136 .3776 .2317 .0008 .0015 2.420 .0024 79.6326						.8478		.2226	.0001	.0009			
554 .499 314.42100 21.31 .9136 .3776 .2317 .0008 .0015 2.420 .0024 79.6326							.3243	.2329	.0007	.0014	2.701	.0030	
201										•0015	2.420	.0024	
									.0012	.0006	-1.264	.0040	9.9309

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

		78 RUN= 4	-			BODY AXI	S CUEFFICIEN	TS		BODY	PRESS-COE	FF
TAIDS	MACH	J.	BETA	ALPHA	CNF	CAF	CLB	CNB	ÇSF		CAB	ÇAC
556	-292	119.997	-00	07	0181	.0187	.0020	•0003	0017	•	0037	0.0000
557	-293	121.349	00	•92	.0575	-0184	.0015	•0005	0019	•	0038	0.0000
558	.292	120.673	.00	1.93	.1247	.0159	.0015	•0003	0022		0037	0.0000
559	.293	121.445	00	2.94	.1996	.0111	.0014	•0005	0027		0038	0.0000
560	.291	119.516	00	3.95	.2795	•0049	.0014	.0005	•0028	•	0037	0.0000
561	.293	121.448	00	5.00	.3512	0023	.0017	.0003	.0019	•		0.0000
562	•290	118.940	•00	6.03	.4161	0117	.0002	0000	0030	•		0.0000
563	.291	114.521	00	7.07	.4891	0232	.0006	.0003	• 0021	•		0.0000
564	-291	119.524	00	8.11	•5546	0353	.0001	.0001	.0020			0.0000
565	.243	120.785	•00	9.15	•6233	0481	0002	•0006	0043			0.0000
566	• 293	121.483	•00	10.33	•6760	0525	.0004	0013	.0009			0.0000
567	.209	118.334	• 00	11.40	• 7488	0484	0018	0019	•002I			0.0000
568	-290	119.050	00	12.51	.8283	0439	0012	0007	• 0062			0.0000
569	- 291	119.837	• 00	14.71	.8119	0050	.0004	•0000	0030			0.0000
570	• 297	124.409	00	16.74	.8990	.0041	0005	•0005	.0019			0.0000
571	-292	120.382	•00	18.76	• 9475	•0092	0005	•0005	0044		0028	0.0000
572	- 292	120.463	•00	20.81	1.0067	.0130	0006	•0007	0049	•	0024	0.0000
	TEST= 7	78 RUN=	42		STAR	ILLIA AVIC C	CIECUC IENTS			CTA D	DOESS COS	
DU I MÎ				AI DHA		ILITY AXIS C		CI S	CNC		.PRESS.COE	
PUIN1	MACH	ų	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB,	P8-1
556	MACH	ų 119.997	BETA •00	07	CL 0180	CD •0187	CPM •0045	.0020	•0003	L/D -•965	CDB.	PB-1 2-3170
556 557	MACH •242 •243	119.997 121.349	BETA •00 -•00	07 .92	CL 0180 .0572	CD •0187 •0193	CPM •0045 •0123	.0020 .0015	•0003 •0005	L/D -•965 2•9 <b>57</b>	CDB. •0037 •0038	P8-1 2-3170 1-8573
556 557 558	MACH •292 •293 •292	119.997 121.349 120.673	BETA •00 -•00 •00	07 .92 1.93	CL 0180 .0572 .1241	CD •0187 •0193 •0201	CPM •0045 •0123 •0159	.0020 .0015 .0015	•0003 •0005 •0003	L/D 965 2.957 6.170	CDB. •0037 •0038 •0037	P8-1 2.3170 1.8573 2.1147
556 557 558 559	MACH •292 •293 •292 •293	119.997 121.349 120.673 121.445	BETA •00 ••00 •00 ••00	07 .92 1.93 2.94	CL 0180 .0572 .1241 .1988	CD .0187 .0193 .0201 .0213	CPM .0045 .0123 .0159 .0203	.0020 .0015 .0015 .0014	.0003 .0005 .0003 .0005	L/D 965 2.957 6.170 9.321	CDB, •0037 •0038 •0037 •0038	P8-1 2-3170 1-8573 2-1147 2-1331
556 557 558 559 560	MACH • 242 • 243 • 242 • 243 • 241	119.997 121.349 120.673 121.445 119.516	BETA .00 00 .00 00 00	07 .92 1.93 2.94 3.95	CL 0180 .0572 .1241 .1988 .2785	CD .0187 .0193 .0201 .0213 .0242	CPM .0045 .0123 .0159 .0203 .0252	.0020 .0015 .0015 .0014 .0014	.0003 .0005 .0003 .0005	L/D 965 2.957 6.170 9.321 11.522	CDB, .0037 .0038 .0037 .0038	P8-1 2-3170 1-8573 2-1147 2-1331 1-9676
556 557 558 559 560 561	MACH •242 •243 •242 •243 •241 •243	119.997 121.349 120.673 121.445 119.516	BETA .00 00 .00 00 00 00	07 .92 1.93 2.94 3.95 5.00	CL 0180 .0572 .1241 .1988 .2785	CD •0187 •0193 •0201 •0213 •0242 •0283	CPM .0045 .0123 .0159 .0203 .0252 .0327	.0020 .0015 .0015 .0014 .0014	.0003 .0005 .0003 .0005 .0004	L/D 965 2.957 6.170 9.321 11.522 12.363	CDB. •0037 •0038 •0037 •0038 •0037 •0038	PB-1 2-3170 1-8573 2-1147 2-1331 1-9676 1-4711
556 557 558 559 560 561 562	MACH 242 243 242 243 243 243 243	119.997 121.349 120.673 121.445 119.516 121.448 118.940	BETA .00 00 .00 00 00 00	07 .92 1.93 2.94 3.95 5.00 6.03	CL 0180 .0572 .1241 .1988 .2785 .3501 .4151	CD •0187 •0193 •0201 •0213 •0242 •0283 •0321	CPM .0045 .0123 .0159 .0203 .0252 .0327 .0358	.0020 .0015 .0015 .0014 .0014 .0018	.0003 .0005 .0003 .0005 .0004 .0001	L/D 965 2.957 6.170 9.321 11.522 12.363 12.949	CDB. •0037 •0038 •0037 •0038 •0037 •0038	PB-1 2.3170 1.8573 2.1147 2.1331 1.9676 1.4711 1.8941
556 557 558 559 560 561 562 563	MACH • 242 • 243 • 242 • 241 • 243 • 240 • 241 • 241	119.997 121.349 120.673 121.445 119.516 121.448 118.940 119.521	BETA .00 00 .00 00 00 00 00 00	07 .92 1.93 2.94 3.95 5.00 6.03 7.07	CL 0180 -0572 -1241 -1988 -2785 -3501 -4151	CD •0187 •0193 •0201 •0213 •0242 •0283 •0321 •0372	CPM .0045 .0123 .0159 .0203 .0252 .0327 .0358 .0434	.0020 .0015 .0015 .0014 .0014 .0018 .0002	.0003 .0005 .0003 .0005 .0004 .0001	L/D 965 2.957 6.170 9.321 11.522 12.363 12.949 13.111	CDB, -0037 -0038 -0037 -0038 -0037 -0038 -0036	PB-1 2.3170 1.8573 2.1147 2.1331 1.9676 1.4711 1.8941
556 557 558 559 560 561 562 563 564	MACH •292 •293 •292 •294 •294 •290 •291 •291	119.997 121.349 120.673 121.445 119.516 121.448 118.940 119.521 119.524	BETA .00 00 .00 00 00 00 00 00	07 .92 1.93 2.94 3.95 5.00 6.03 7.07 8.11	CL0180 .0572 .1241 .1988 .2785 .3501 .4151 .4882	CD •0187 •0193 •0201 •0213 •0242 •0283 •0321 •0372 •0433	CPM .0045 .0123 .0159 .0203 .0252 .0327 .0358 .0434 .0501	.0020 .0015 .0015 .0014 .0014 .0018 .0002	.0003 .0005 .0003 .0005 .0004 .0001 0001	L/D 965 2-957 6-170 9-321 11-522 12-363 12-949 13-111	CDB, -0037 -0038 -0037 -0038 -0037 -0038 -0037	P8-1 2-3177 1.8573 2-1147 2-1331 1.9676 1.4711 1.8941 1.783
556 557 558 559 560 561 562 563 564 565	MACH -242 -243 -243 -243 -243 -290 -291 -291 -293	119.997 121.349 120.673 121.445 119.516 121.448 118.940 119.521 119.521 120.785	BETA .00 00 .00 00 00 00 00 00	07 .92 1.93 2.94 3.95 5.00 6.03 7.07 8.11 9.15	CL0180 .0572 .1241 .1988 .2785 .3501 .4151 .4882 .5540	CD •0187 •0193 •0201 •0213 •0242 •0283 •0321 •0372 •0433 •0517	CPM .0045 .0123 .0159 .0203 .0252 .0327 .0358 .0434 .0501 .0573	.0020 .0015 .0015 .0014 .0014 .0018 .0002 .0006	.0003 .0005 .0003 .0005 .0004 .0001 0001 .0002 .0001	L/D 965 2.957 6.170 9.321 11.522 12.363 12.949 13.111 12.793 12.058	CDB. -0037 -0038 -0037 -0038 -0037 -0038 -0037 -0037	PB-1 2-3177 1.8573 2-1147 2-1331 1.9676 1.4711 1.8941 1.7833 1.9866
556 557 558 559 560 561 562 563 564 565	MACH -242 -243 -243 -241 -243 -290 -291 -291 -293 -243	119.997 121.349 120.673 121.445 119.516 121.448 118.940 119.521 119.524 120.785	BETA .00 00 .00 00 00 00 00 00 00 00	07 .92 1.93 2.94 3.95 5.00 6.03 7.07 8.11 9.15 10.33	CL0180 .0572 .1241 .1988 .2785 .3501 .4151 .4882 .5540 .6230	CD •0187 •0193 •0201 •0213 •0242 •0283 •0321 •0372 •0433 •0517 •0696	CPM .0045 .0123 .0159 .0203 .0252 .0358 .0434 .0501 .0573 .0592	.0020 .0015 .0015 .0014 .0014 .0008 .0002 .0006 .0001	.0003 .0005 .0003 .0005 .0004 .0001 0001 .0002 .0001	L/D 965 2.957 6.170 9.321 11.522 12.363 12.949 13.111 12.793 12.058 9.695	CDB, -0037 -0038 -0037 -0038 -0037 -0038 -0037 -0037 -0037	P8-1 2-3177 1-8573 2-1147 2-1331 1-9676 1-4711 1-8941 1-783 1-9866 3-4388
556 557 558 559 560 561 562 563 564 565 566 567	MACH -242 -243 -242 -243 -241 -243 -291 -291 -243 -243	119.997 121.349 120.673 121.445 119.516 121.448 118.940 119.521 119.521 120.785 121.483 118.334	BETA .00 .00 .00 .00 .00 .00 .00 .0	07 .92 1.93 2.94 3.95 5.00 6.03 7.07 8.11 9.15 10.33	CL0180 .0572 .1241 .1988 .2785 .3501 .4151 .4882 .5540 .6230 .6745	CD •0187 •0193 •0201 •0213 •0242 •0283 •0321 •0372 •0433 •0517 •0696 •1005	CPM .0045 .0123 .0159 .0203 .0252 .0327 .0358 .0434 .0501 .0573 .0592 .0802	.0020 .0015 .0015 .0014 .0014 .0018 .0002 .0006 .0001	.0003 .0005 .0003 .0005 .0004 .0001 -0001 .0002 .0001 .0006 -0013	L/D 965 2.957 6.170 9.321 11.522 12.363 12.949 13.111 12.793 12.058 9.695 7.396	CDB, -0037 -0038 -0037 -0038 -0037 -0036 -0037 -0036 -0035 -0033	P8-1 2-3177 1.8573 2-1147 2-1331 1.9677 1.4711 1.8941 1.783 1.9866 3.4388 13-5355
556 557 558 559 560 561 562 563 564 565 566 567	MACH • 242 • 243 • 242 • 243 • 243 • 241 • 243 • 243 • 243 • 243 • 243 • 243	119.997 121.349 120.673 121.449 119.516 121.448 118.940 119.524 120.785 121.483 118.334 119.056	BETA .00 .00 .00 .00 .00 .00 .00 .0	07 .92 1.93 2.94 3.95 5.00 6.03 7.07 8.11 9.15 10.33 11.40 12.51	CL0180 -0572 -1241 -1988 -2785 -3501 -4151 -4882 -5540 -6230 -6745 -7436 -8181	CD •0187 •0193 •0201 •0213 •0242 •0283 •0321 •0372 •0433 •0517 •0696 •1005 •1365	CPM .0045 .0123 .0159 .0203 .0252 .0327 .0358 .0434 .0501 .0573 .0592 .0802 .1128	.0020 .0015 .0015 .0014 .0014 .0018 .0002 .0006 .0001 0001 .0002 0022	.0003 .0005 .0003 .0005 .0004 .0001 -0001 .0002 .0001 .0006 -0013 -0015	L/D 965 2-957 6-170 9-321 11-522 12-363 12-949 13-111 12-793 12-058 9-695 7-396 5-993	CDB, -0037 -0038 -0037 -0038 -0037 -0036 -0037 -0036 -0035 -0033	P8-1 2-3177 1.8573 2.1147 2.1331 1.9676 1.4711 1.8941 1.783 1.9860 3.4388 13.5354 22.6577
556 557 558 559 560 561 562 563 564 565 566 567 568	MACH • 242 • 243 • 242 • 243 • 243 • 240 • 241 • 243 • 243 • 243 • 243 • 243 • 244	119.997 121.349 120.673 121.445 119.516 121.448 118.940 119.521 119.524 120.785 121.483 118.334 118.335 119.837	BETA -00 -00 -00 -00 -00 -00 -00 -0	07 .92 1.93 2.94 3.95 5.00 6.03 7.07 8.11 9.15 10.33 11.40 12.51 14.71	CL01d0 .0572 .1241 .1948 .2785 .3501 .4151 .4882 .5540 .6230 .6745 .7430 .8181	CD •0187 •0193 •0201 •0213 •0242 •0283 •0321 •0372 •0433 •0517 •0696 •1005 •1365 •2013	CPM .0045 .0123 .0159 .0203 .0252 .0327 .0358 .0434 .0501 .0573 .0592 .0802 .1128	.0020 .0015 .0015 .0014 .0014 .0018 .0002 .0006 .0001 0001 .0002 0022 0023	.0003 .0005 .0003 .0005 .0004 .0001 0001 .0002 .0001 .0006 0013 0005	L/D965 2.957 6.170 9.321 11.522 12.363 12.949 13.111 12.793 12.058 9.695 7.396 5.993 3.907	CDB, -0037 -0038 -0037 -0038 -0037 -0036 -0037 -0037 -0035 -0035 -0035 -0032	P8-1 2-317 1.8573 2.1147 2.133 1.9676 1.4711 1.8941 1.7836 3.438 13.5354 22.6571 27.9544
556 557 558 559 560 561 562 563 564 565 566 567	MACH • 242 • 243 • 242 • 243 • 243 • 241 • 243 • 243 • 243 • 243 • 243 • 243	119.997 121.349 120.673 121.449 119.516 121.448 118.940 119.524 120.785 121.483 118.334 119.056	BETA .00 .00 .00 .00 .00 .00 .00 .0	07 .92 1.93 2.94 3.95 5.00 6.03 7.07 8.11 9.15 10.33 11.40 12.51	CL0180 -0572 -1241 -1988 -2785 -3501 -4151 -4882 -5540 -6230 -6745 -7436 -8181	CD •0187 •0193 •0201 •0213 •0242 •0283 •0321 •0372 •0433 •0517 •0696 •1005 •1365	CPM .0045 .0123 .0159 .0203 .0252 .0327 .0358 .0434 .0501 .0573 .0592 .0802 .1128	.0020 .0015 .0015 .0014 .0014 .0018 .0002 .0006 .0001 0001 .0002 0022	.0003 .0005 .0003 .0005 .0004 .0001 -0001 .0002 .0001 .0006 -0013 -0015	L/D 965 2-957 6-170 9-321 11-522 12-363 12-949 13-111 12-793 12-058 9-695 7-396 5-993	CDB, -0037 -0038 -0037 -0038 -0037 -0036 -0037 -0036 -0035 -0033	PB-1 2-3177 1-8573 2-1147 2-1331 1-9676 1-4711 1-8941 1-783 1-986

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST≈ 7	78 RUN=	43									
							IS COEFFICIE				PRESS.COE	
POINT	MACH	Q	BETA		CNF	CAF	CLB	CNB	CSF		CAB	CAC
601	•930	739.454	01	18	0110	.0195	.0007	•0005	.0021			0.0000
602	•932	740.848	0i	1.06	.1318	•0203	.0005	-0004	.0019	•	0062	0.0000
603	•931	740.444	01	2.26	•2528	.0202	.0005	.0001	.0025	•	0061	0.0000
604	.932	740.783	00	3.52	.3625	.0199	.0009	0000	.0026	•	0061	0.0000
605	.933	741.973	01	4.69	• 4589	•0205	.0011	0001	.0038	•	0060	0.0000
606	.937	744.539	01	5.88	•5506	.0210	.0008	0003	.0045	•	0060	0.0000
607	•935	143.524	00	7.12	•6573	•0211	.0009	0005	.0041		0060	0.0000
608	.936	744.295	00	8.33	.7442	.0214	0002	0005	.0035	•	0059	0.0000
609	.937	745.042	00	9.51	.0163	.0218	0017	0003	.0025	•	0058	0.0000
610	.938	745.513	00	10.70	.8924	.0217	0029	0003	.0021		0056	0.0000
611	-940	747-417	00	11.94	1.0000	.0221	0060	0003	.0021	•	0053	0.0000
612	•929	738.290	01	11	0190	•0185	.0005	.0005	.0013	•	0061	0.0000
	TEST≈ 7	78 RUN=	43									
					STAB	ILITY AXIS	COEFFICIENTS			STAB	<ul><li>PRESS.COE</li></ul>	FF
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
601	•930	739.454	01	18	0110	.0195	-0111	.0007	• 0005	563	.0061	11.5296
602	.932	740.848	01	1.06	. 1314	.0227	0027	• UOO5	•0004	5.785	.0062	14.2807
603	.931	740.444	01	2.26	-2518	.0302	0088	.0005	.0001	8.337	.0061	25.4473
604	•932	740.783	00	3.52	• 3606	•0421	0072	.0008	0001	8.571	.0061	28.1358
605	•933	741.973	01	4.69	• 455 <i>1</i>	.0579	0036	-0011	0002	7.865	.0060	26.3226
606	•937	744.539	01	5.88	• 5455	.0772	0016	•0008	0004	7.063	.0060	41.2662
607	.935	743.524	00	7.12	• 6490	<ul><li>1024</li></ul>	0049	.0008	0006	6.345	.0059	74.1541
608	.936	744.295	00	8.33	• 7332	.1290	0025	0002	0004	5.686	.0058	116.5452
60 <del>9</del>	•937	745.042	00	9.51	.8015	.1564	.0044	0018	0000	5.124	•0057	153.5596
610	• 938	745.513	00	10.70	.8728	.1869	.0051	0029	.0002	4.670	.0055	179.3195
611	•940	747.417	00	11.94	• 9738	-2286	0177	0059	•0009	4.260	.0051	226.9633
612	•929	738-290	01	11	0189	.0185	.0125	•0005	• 0005	-1.024	.0061	11.5796

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

						BODY AXI	S COEFFICIEN	18		BODY PRESS.	COEFF
TNIDS	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	C SF	CAB	CAC
626	.864	o85.292	00	17	0185	.0168	•0006	•0005	.0003	•0053	0.000
627	.804	685•288	00	•99	•0962	•0155	•0002	•0005	.0001	•0053	0.000
628	.864	685.297	00	2.21	•2252	.0113	.0008	•0006	0000	•0053	0.000
629	-864	685.374	00	3.50	•3644	•0056	.0013	•0006	.000l	.0053	0.000
630	-862	683.974	00	4.71	•4979	•0025	-0014	.0003	.0006	• 0052	0.000
631	-862	683.836	00	5.94	•6009	.0017	.0007	•0003	•0006	.0051	0.000
632	.864	685.564	-00	7.13	.6701	.0057	0008	0003	.0010	•0051	0.000
633	.866	686.945	00	8.29	.7182	•0082	.0021	0000	.0017	•0051	0.000
634	-865	685.845	01	9.38	•7298	-0118	•0046	.0001	.0027	• 0050	0.000
635	-864	685.828	•00	10.41	.7340	.0172	0031	0006	-0018	•0050	0.000
636	-866	686.915	•00	11.54	•7628	•0196	0029	0007	•0022	.0049	0.000
637	-860	087.274	•00	12.64	•7981	.0213	0039	0006	.0018	.0049	0.000
638	.866	687.529	•00	13.85	.8384	-0219	0043	0005	.0017	.0048	0.000
639	-861	682.845	01	÷.08	0188	.0164	•0003	•0006	.0006	• 0052	0.000

	1F21= 1	/8 KUN=	44									
					STAI	BILITY AXIS (	STAB.PRESS.COEFF					
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
626	.864	685.292	00	17	0185	.0168	.0100	.0006	.0005	-1.098	.0053	9.7789
627	.864	685.288	00	•99	•0960	•0172	-0125	•0002	.0005	5.584	.0053	10.3791
628	-864	685.297	00	2.21	-2246	.0199	.0136	.0008	•0006	11.266	.0053	14.8809
629	-864	685.374	00	3.50	•3634	.0278	.0079	.0013	.0005	13.069	•0053	20.8830
630	-862	683.974	00	4.71	• 4960	•0433	•0009	•0015	.0002	11-448	•0052	22.9463
631	.852	683.836	00	5.94	•5975	.0638	•0057	.0008	.0002	9.360	.0051	54.2713
632	.864	685.564	•00	7.13	•6642	.0888	•0292	-:0009	0002	7.479	.0051	62.2744
633	.866	686.945	00	8.29	<b>.</b> 7095	.1117	•0550	•0021	0003	6.354	.0051	88.1595
634	.865	685.845	01	9.38	.7181	•1305	•0850	•0046	0007	5.502	.0049	119.0462
635	.864	685.828	•00	10.41	•7188	•1496	-1066	0032	0000	4.806	.0049	121.0469
636	-866	686.915	.00	11.54	.7435	•1718	.1169	0030	0001	4.327	.0048	111.5433
637	-866	687.274	.00	12.64	.7740	<ul><li>1955</li></ul>	-1243	0040	.0003	3.959	.0048	110.5429
638	.800	687.529	•00	13.85	.8087	•2219	-1330	0043	.0005	3.644	.0047	113.0438
639	.861	682.845	01	08	0188	•0164	.0106	•0003	.0006	-1.146	.0052	10.3541

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TES[≈ 7	78 KUN= 4	45								
						BODY AXI	S COEFFICIEN	ITS		BODY PRESS.	COEFF
POINT	MACH	w	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
653	.805	168.160	01	17	0184	.0165	.0005	.0007	.0005	.0048	0.0000
654	.805	631.881	01	1.00	.0879	.0155	.0004	.0006	.0011	.0049	0.0000
655	• du 7	633.958	01	2.14	.1978	.0115	.0010	.0007	.0001	.0049	0.0000
656	.806	633.471	01	3.34	.3095	.0049	.0010	.0007	.0005	.0049	0.0000
657	•80°	633.189	01	4.55	• 4269	0024	.0010	.0007	0001	•0049	0.0000
658	.800	033-505	00	5.76	.5437	0075	.0006	.0004	.0007	.0048	0.0000
659	.807	633.902	-00	6.95	.6206	0054	0005	0002	.0008	.0047	0.0000
660	* BD 7	634.275	00	8.08	•0699	0002	0003	0001	.0018	.0047	0.0000
661	• 808	034.653	•00	9.17	•6855	.0066	0021	0004	.0016	.0047	0.0000
662	• 808	635.037	-00	10.27	.7185	.0113	0027	0005	.0015	.0046	0.0000
663	•877	635.928	00	11.40	•7493	.0149	0030	0004	•0024	.0046	0.0000
664	.809	635.807	.00	12.50	.7812	.0175	0034	0006	•0023	.0045	0.0000
665	-808	635-184	.00	13.65	.8116	.0190	0036	0005	.0021	• 0045	0.0000
666	• 808	635.947	00	15.91	•8772	.0217	0009	.0000	0001	.0043	0.0000
667	.810	636.859	00	18.08	•9548	.0224	.0005	•0003	•0002	.0040	0.0000
668	.812	038.690	.00	20.24	1.0253	.0223	.0003	.0003	0021	•0034	0.0000
669	.815	641.281	.01	22.40	1.1280	.0210	0003	.0003	0067	•0025	0.0000
670	•806	632.953	01	08	0185	.0163	.0003	.0007	.0007	.0049	0.0000

	TEST= 7	78 RUN≃	45										
					STA	BILITY AXIS	DEFFICIENTS	ı	STAB.PRESS.COEFF				
TAIOS	MACH	ú	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1	
o 5 3	-805	031.881	01	17	0183	.0165	.0097	.0005	.0007	-1.110	.0048	10.2041	
654	• 805	031.881	01	1.00	.0876	.0170	.0144	.0004	• 0006	5.152	.0049	8.7785	
655	.807	633.958	01	2.14	.1972	.0189	.0168	.0010	•0006	10.446	-0049	9.6539	
656	-806	633.471	01	3.34	-3087	.0229	.0220	.0010	.0007	13.462	0049	11.3545	
57ه	ە06.	633.189	01	4.55	•4258	.0315	.0246	.0011	.0007	13.523	.0049	15.7813	
458	-806	633.505	00	5.76	.5417	.0471	.0272	.0006	.0003	11.503	.0048	24.1343	
659	.807	633.902	.00	6.95	.6166	.0698	.0480	0005	0001	8.835	.0047	54.5214	
660	<b>.</b> 8∪7	634.275	00	8.08	.6633	.0939	.0782	0003	0001	7.061	.0047	68.7769	
661	• 80 B	634.653	.00	9.17	.6757	.1157	.1033	0021	0001	5.838	• 0046	87.5343	
662	•80₫	035.037	.00	10.27	.7050	.1392	·1205	0027	0000	5.063	-0046	99.2261	
663	.809	635.928	00	11.40	.7315	.1627	.1335	0030	.0002	4.496	-0045	99.9764	
664	.809	635.807	.00	12.50	.7589	.1862	.1455	0034	.0002	4.076	.0044	92.8486	
665	<b>.</b> 808	635.184	.00	13.05	. 7842	.2100	. 1554	0036	.0004	3.734	.0044	95.2871	
606	- 809	035.947	00	15.91	. 8377	.2613	.1770	0008	.0003	3.205	.0041	89.0972	
667	-810	636.859	00	18.08	• 9007	.3177	.1848	.0006	.0001	2.835	.0038	91-1605	
668	-812	633.690	.00	20.24	. 9543	.3755	.1856	.0004	.0002	2.541	•0032	101.2894	
669	-815	641.281	.01	22.40	1.0349	• 4492	.1918	0002	.0004	2.304	.0023	119.6716	
670	.806	632.953	01	08	0185	.0163	.0097	.0003	.0007	-1.132	.0049	9-4038	

TEST= 7/8 RUN= 46

701

.753 582.169 -.01 6.75

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

BODY AXIS COEFFICIENTS

BODY PRESS-COEFF

.0045

40.5781

							2 COEFFICIEN			BODY	/ PRESS.COE	FF
POINT	MACH	7	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
684	.755	583.780	01	22	0180	.0167	.0003⋅	.0007	.0008	,	.0047	0.0000
685	.754	582.307	01	.88	•0795	.0157	•0002	.0007	.0003		0046	0.0000
686	<b>.</b> 755	583.936	01	2.06	· 1849	.0119	.0008	.0007	.0004		.0047	0.0000
687	.753	582.009	01	3.20	•2853	.0059	.0012	.0008	.0007		.0046	0.0000
688	.753	582.191	01	4.37	•3828	0014	•0012	•0007	.0001		.0046	0.0000
689	. 753	581-856	01	5.55	• 4867	0066	.0014	.0009	.0005		0046	0.0000
690	.754	582.609	00	6.70	<b>∙</b> 5655	0043	.0018	-0004	.0005		0046	0.0000
691	.754	583.443	•00	7.84	-6115	.0033	0007	0004	.0017		.0045	0.0000
692	• 754	583.198	•00	8.94	•0594	.0075	.0005	0005	.0011		0045	0.0000
693	.754	<b>583.464</b>	•00	10.05	•6940	.0103	0021	0005	.0015		.0044	0.0000
694	.756	584.810	•00	11.20	.7387	.0122	0026	0004	.0013		0044	0.0000
695	.755	od4.042	00	12.29	•7702	.0143	0031	0005	•0025		.0043	0.0000
696	.754	583.526	.00	13.44	• 4009	.0161	0038	0007	.0027		.0043	0.0000
697	.757	o 85.509	00	15.68	-8601	.0195	0016	•0001	.0011		.0042	0.0000
698	.756	584.475	00	17.84	•9167	.0209	.0007	.0001	•0009		.0040	0.0000
699	.759	588.025	.00	19.07	• 9635	.0217	•0006	0002	.0007		.0037	0.0000
700	.759	587.841	•00	22.06	1.0738	•0204	0005	•0003	0038		.0026	0.0000
701	د 75 ه	582.169	01	6.75	•5640	0045	•0020	.0005	.0016		.0046	0.0000
	TEST= 7	73 KUN=	46		STAB	ILITY AXIS C	OFFFICIENTS			RATS	-PRESS-COE	CE
POINT	MACH	J	BETA	ALPHA	CL	CD	CPM	CLS	CNS	1/D	CDB	PB-1
684	.755	583.780	01	22	0180	.0167	• 0093	.0003	.0007	-1.074	•0047	8.3533
685	.754	582.367	01	-88	• 0792	.0170	.0138	.0002	.0007	4.671	•0046	7.8031
686	.755	583.930	01	2.06	. 1844	.0186	.0184	.0009	•0006	9.932	•0047	7.8531
687	. 753	582.009	01	3.20	- 2845	.0218	.0239	•0012	•0007	13.025	•0046	8.8535
688	•753	582.197	01	4.37	-3818	.0278	.0298	.0012	-0006	13.732	•0046	9.3787
689	.753	581.856	01	5.55	·4851	.0405	.0357	•0015	•0007	11.975	.0046	13.3303
690	.754	582.609	00	6.70	•5621	.0617	.0529	•0019	•0002	9.118	.0046	38.7649
691	•754	583.443	•00	7.84	• 6054	• 0866	.0827	0007	0003	6.988	-0045	66.1509
692	.754	583.198	•00	8.94	•6502	•1099	•1028	•0005	0006	5.917	.0045	70.6527
693	.754	583.464	.00	10.05	•6816	•1312	-1221	0021	0001	5.196	.0044	81.4069
694	<b>.</b> 750	<b>584.810</b>	•00	11.20	•7222	·1554	.1389	0026	.0001	4.648	.0043	91.1607
695	• 755	584.042	00	12.29	• 7495	.1780	·1523	0031	-0002	4.211	.0042	89.0972
696	.754	583.526	•00	13.44	•7752	.2018	.1636	0039	• 0002	3.842	.0042	86.4712
697	.757	585.509		15.68	• 8229	.2512	.1840	0015	•0005	3.276	.0040	93.5989
698	.750	584.475		17.84	.8662	• 3006	•1954	-0007	0001	2.881	.0038	77.0925
699	.759	580.025		19.07	• 9036	.3352	•1957	•0005	0004	2.696	.0035	83.8451
700	.759			22.06	•9875	• 4223	. 1995	0003	•0005	2.338	.0024	101.6646
701	- 75 1	582-169	01	6.75	5605	0610	0527	0021	2002	0.010		

.0619

•5600

.0527

.0021

.0003

9.060

	1551= 1	/8 KUN=	47									
						RODA VXI	S CUEFFICIER	NTS		BODY	PRESS-COE	FF
POINT	MACH	پ	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
716	-702	529.764	00	11	0173	.0166	.0004	.0006	0005		0045	0.0000
717	.702	529.845	00	•94	.0703	•0157	.0004	.0007	0010	•	0045	0.0000
718	.701	529.462	00	2.04	•1689	.0123	.0004	•0006	0003		0045	0.0000
719	.702	530.560	00	3.16	·2651	•0065	.0009	•0007	0013		0045	0.0000
720	.701	529.014	00	4.28	.3576	0009	.0004	•0006	0002		0045	0.0000
721	•703	530.881	00	5.43	•4527	0071	.0008	.0008	0011		0045	0.0000
722	.702	529.956	00	6.58	.5413	0060	.0017	.0005	0013	•	0044	0.0000
723	.702	530.279	•00	7.72	•5884	.0016	0009	0003	000l	•	0044	0.0000
724	<b>.7</b> 02	530.332	•00	8.82	•6421	.0051	0003	0003	.0013		0043	0.0000
725	.702	530.706	•00	9.91	•6869	.0074	0000	0005	.0003		0043	0.0000
726	.703	531.001	•00	11.03	.7165	.0097	0026	0006	•0006	•	0042	0.0000
727	.704	532.252	•00	12.13	.7550	.0118	0033	0006	.0007		0042	0.0000
728	.703	531.011	•00	13.28	. 7902	.0136	0035	0007	.0005	•	0041	0.0000
<b>729</b>	.704	531.912	.00	15.54	•8539	.0171	0025	0000	.0000		0040	0.0000
730	<b>.7</b> 05	533.351	00	17.67	•9053	.0194	•0004	.0004	0006		0039	0.0000
731	.705	533.273	00	19.72	•9696	•0210	.0006	.0003	•0004	•	0033	0.0000
732	•705	533.759	•00	21.81	1.0301	.0201	0002	.0003	0020		0026	0.0000
733	<b>.7</b> 02	530.594	00	6.60	•5331	0050	.0002	0000	.0014		0044	0.0000
734	<b>.7</b> 01	529.581	00	6.60	•5362	0051	.0001	.0001	.0015		0044	0.0000
	TEST= 7	78 RUN=	47		STAR	BILITY AXIS C	DEELLIENTS			C#AD	BDEC: 600	
POINT	MACH	J	BÉTA	ALPHA	CL	CD CD	CPM	CLS	CNS	L/D	.PRESS.COE	
716	.732	529.764	00	11	0173	•0166	• 0090	•0004	•0006	-1.042	CDB	PB-1
717	.702	529.845	00	.94	.0700	.0169	.0133	•0004	•0007	4.146	•0045	6.9778
718	.701	529.462	00	2.04	.1683	.0183	.0188	.0004	.0007	9.201	•0045	7.3779
719	.702	530.560	00	3.16	• 2544	.0211	.0233	•0009	.0006	12.533	•0045 •0044	7.8781 7.4530
720	.701	529.014	00	4.28	• 3567	.0258	.0304	•0005	•0006	13.815	•0044	7.1779
721	• 703	530.881	00	5.43	•4513	.0358	.0379	•0008	-0007	12.619	•0044	9.0286
722	.732	529.956	00	6.58	• 5385	•0560	•0500	.0017	.0003	9.610	•0044	30.0740
723	•702	530.279	•00	7.72	•5828	•0806	.0816	0009	0002	7.233	•0043	53.5210
724	.702	530.332	.00	8.82	.6337	.1035	•1031	0004	0003	6.125	.0043	65.4006
725	-702	530.706	.00	9.91	.6754	.1255	.1219	0001	0005	5.382	.0042	72.0282
726	.703	531.001	•00	11.03	.7015	.1466	.1406	0027	0001	4.786	•0041	76.2799
727	.704	532.252		12.13	.7357	.1702	.1548	0033	•0001	4.323	•0041	81.0318
728	.703	531.011		13.28	.7659	. 1947	.1666	0036	.0001	3.933	•0040	87.6593
729	.704	531.912		15.54	.8181	-2453	.1876	0024	•0001	3.335	.0039	95.0995
730	. 705	533.351	00	17.67	.8567	.2932	.2031	.0005	•0003	2.922	.0037	73.9038
731	.705	533.273	00	19.72	.9056	.3470	•1991	.0006	•0001	2.610	•0031	80.4688
732	.705	533.759		21.81	•9489	.4014	-2013	0001	.0003	2.364	.0025	90.9729
733	.702	530.594	00	6.60	.5302	.0563	.0522	.0002	0001	9.419	.0044	41.0157
734	.701	529.581	00	6.60	.5332	.0566	.0518	.0001	.0001	9.422	-0044	40.2029

	TEST= 7	78 KUN= 4	¥8								
						BODY AXE	S COEFFICIEN	TS		BODY PRESS.	COEFF
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
748	.292	120.670	00	• 05	0171	.0170	.0000	.0008	0001	.0038	0.0000
749	.292	120.671	00	1.06	.0526	.0168	•0002	.0006	0008	.0038	0.0000
750	. 243	121.445	00	2.02	.1320	.0149	.0019	.0008	0027	.0038	0.0000
751	-294	122.121	00	3.03	.2087	.0101	.0007	.0006	0022	.0038	0.0000
752	-292	120.772	00	4.01	.2810	.0051	.0018	.0008	0037	.0038	0.0000
753	-293	120.872	•00	5.03	.3685	0021	•0006	.0007	0033	•0038	0.0000
754	•293	120.874	.00	6.04	•4374	0116	0001	•0005	0032	•0038	0.0000
755	.292	120.691	.00	7.08	•5155	0184	•0005	0006	0041	.0037	0.0000
756	.292	120.722	•00	8.13	•5925	0134	•0034	.0012	0073	.0037	0.0000
757	.242	120.752	•00	9.16	•6507	0102	.0059	.0017	0102	• 0035	0.0000
758	.292	120.789	.00	10.26	.7028	0043	0009	0008	0055	•0036	0.0000
759	-293	120.816	•00	11.28	.7388	0036	0024	0006	0050	•0034	0.0000
760	.292	120.075	•00	12.36	.7803	0021	0031	0005	0050	•0033	0.0000
761	.294	122.078	•00	14.52	.8367	.0039	0000	.0000	0090	.0031	0.0000
762	.292	120.221	• 00	16.59	•9188	.0080	0001	.0003	0102	• 0029	0.0000
763	.293	120.875	•00	18.62	•9742	.0105	0001	.0000	0108	•0028	0.0000
764	- 294	122.308	•00	20.62	1.0251	.0132	0001	.0004	0112	•0024	0.0000
765	.293	121.205	•00	8.07	•5906	0126	.0033	.0011	0131	.0037	0.0000

	TEST= 7	78 RUN=	48									
					STA	BILITY AXIS	COEFFICIENTS			STAB	.PRESS.COEFF	=
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	СОВ	PB-1
748	.242	120.670	00	•05	0172	.0170	.0050	-0000	•0008	-1.010	.0038	1.4631
749	.242	120.671	00	1.06	.0523	.0177	.0127	•0002	• 0006	2.950	.0038	1.5381
750	.293	121.445	00	2.02	.1313	.0195	.0181	•0019	.0007	6.733	.0038	1.8507
751	•294	122.121	00	3.03	.2078	.0211	.0232	•0008	.0006	9.844	.0038	1.6882
752	.292	120.772	00	4.01	-2800	•0248	.0313	.0018	.0007	11.296	.0038	1.5881
753	. 293	120.872	•00	5.03	.3673	.0303	.0376	•0007	•0006	12.141	.0038	1.5131
754	.243	120.874	.00	6.04	• 4361	.0345	• 0452	0000	•0005	12.632	.0038	1.7757
755	•292	120.691	•00	7.08	•5138	.0453	.0499	•0005	0007	11.338	.0036	3.0762
756	- 242	120.722	.00	8.13	• 5884	• 0705	.0613	• 0035	.0007	8.346	.0036	14.5558
757	.292	120.752	•00	9.16	•6440	•0936	.0775	•0061	.0008	6.881	.0035	22.4340
758	.242	120.789	-00	10.26	.6924	.1209	.1135	0013	0006	5.727	.0035	32.3874
759	. 293	120.816	•00	11.28	•7252	.1410	.1341	0025	0001	5-144	.0034	33.5754
760	-292	120.075	•00	12.36	.7626	.1649	-1489	0031	.0002	4.624	.0032	37.8895
761	-294	122.078	•00	14.52	<ul><li>8090</li></ul>	-2136	.1914	0000	.0000	3.788	.0030	38.5148
762	.292	120,221	•00	16.59	.8783	<b>.27</b> 00	.2227	.0000	•0003	3.253	.0028	34.7008
763	.293	120.875	•00	18.62	•9198	.3210	.2382	0001	.0001	2.865	.0027	29.6364
764	. 294	122.308	•00	20.62	•9547	.3733	.2435	0000	•0004	2.557	•0022	33.3878
765	.293	121.205	.00	8.07	<b>.</b> 5866	-0705	-0612	-0035	.0006	8.324	.0036	14.5933

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

CAF

.0180

BODY AXIS COEFFICIENTS

CLB

-.0005

BODY PRESS.COEFF

CAB

.0040

CAC

0.0000

CSF

-.0043

CNB

.0007

767	•497	312.046	00	- 86	.0602	.0173	0002	•0006	0028		0040	0.000
768	.497	312.136	•00	1.89	-1430	•0146	.0003	-0005	0037	•	0040	0.0000
769	•497	312.138	00	2.97	.2253	.0097	•0006	.0007	0022	•	0040	0.000
770	•497	312.670	00	4.03	•3034	.0029	.0006	.0006	0027	•	0040	0.0000
771	.497	312.675	.00	5.11	.3853	0059	.0001	•0003	0028	•	0040	0.0000
772	•497	312.696	•00	6.20	.4673	0136	.0003	•0004	0036		0039	0.0000
773	•498	313.488	00	7.31	• 5442	0106	.0024	.0008	0037		0039	0.000
774	•497	312.251	00	8.40	.6184	0073	.0062	-0014	0056		0039	0.000
775	•49 d	312.961	00	9.49	•6733	0054	.0088	-0017	0062	•	0038	0.000
776	.497	312.430	00	10.58	.7263	0038	.0100	.0016	<b>→.</b> 0657		0037	0.000
777	•497	312.536	-00	11.65	• 7386	.0023	0029	0007	0026		0037	0.0000
778	.498	313.263	•00	12.76	•7792	.0047	0037	0007	0024	•	0036	0.0000
779	-498	312.959	.00	14.99	-8540	•0095	0024	.0001	0048	•	0035	0.0000
780	•478	313.699	•00	17.08	•9012	.0129	0002	.0004	0031			0.0000
781	.499	313.838	•00	19.14	.9613	.0149	.0002	.0003	0040	•	0031	0.0000
782	•500	315.400	•00	21.15	1.0053	.0169	0013	•0006	002 <b>7</b>	•	0024	0.0000
	TEST= 7	78 RUN=	49		STAB	ILITY AXIS C	OEFFICIENTS			STAB	.PRESS.COEF	F
PUINT	MACH	۵	BETA	ALPHA	CL	Cυ	CPM	CLS	CNS	L/D	CDB	PB-1
760	.491	312.040	.00	17	0220	.0180	.0069	0005	.0007	-1.222	.0040	4.4268
767	.477	312.040	00	-86	.0600	.0182	.0134	0002	.0006	3.294	.0040	4.2017
768	.497	312.130	-00	1.89	.1424	.0193	.0172	.0003	•0005	7.378	.0040	4.5268
769	.497	312.136	00	2.97	-2245	•0214	.0237	.0007	.0006	10.481	.0040	4.5393
770	• 497	312.670	00	4.03	.3024	.0242	.0298	.0006	.0005	12.485	.0040	4.2267
171	.477	312.675	<b>-00</b>	5.11	.3843	.0284	.0349	.0001	.0003	13.523	•0040	4.4018
172	• 497	312-695	.00	6.20	<b>.</b> 4660	.0369	.0440	.0003	•0004	12.631	•0039	4.7644
773	·478	313.408	00	7.31	.5411	.0587	.0550	•0024	.0005	9.214	•0039	19.6325
774	-497	312.251	00	8.40	•6128	.0830	.0709	•0064	• 0005	7.380	•0039	36.7016
775	.498	312.961	00	9.49	•6650	.1057	.0873	• 0089	•0002	6.293	.0037	47.2685
776	.447	312.430	00	10.58	-7147	.1297	•1036	.0102	0002	5.511	•0036	55.7719
777	•497	312.530	.00	11.65	.7229	. 1513	.1485	0030	0001	4.777	•0036	64.1501
778	•478	313.263		12.70	• 7590	.1766	.1620	0038	•0001	4-296	.0035	72.9036
779	• 498	312.959	• 00	14.99	• 8225	-2301	.1942	0023	•0008	3.574	.0034	93.4114
									0005			
780 781	•49d •499	313.699	.00	17.08 19.14	• 85 76 • 90 32	•2771 •3292	.2190 .2279	0000	.0005 .0002	3.095 2.744	.0032 .0029	62.6494 62.0867

.2222

-.0010

.0010

2.461

.0023

68.4641

TEST= 778 RUN= 49

.497 312.046

.530 315.400

782

MACH

BETA ALPHA

-.17

.00

CNF

-.0221

.9315

.00 21.15

.3785

TALOG

766

	TEST= 7	78 RUN= 5	0									
						BODY AXI	IS COEFFICIEN	TS		800Y	PRESS.CDEF	F
POINT	MACH	ú	BETA	ALPHA	C NF	CAF	CLB	CNB	CSF	(	AB	CAC
810	.933	741.242	00	11	.0026	.0204	.0003	.0008	0004	• (	062 0	.0000
811	. 930	738.828	01	1.13	.1181	.0198	•0006	.0008	0002	•0	062 0	.0000
812	-932	740.224	01	2.35	•2266	.0202	.0004	.0006	.0005	• (	062 0	.0000
813	. 433	741.112	01	3.59	.3302	.0201	•0002	.0006	.0011	•(	061 0	.0000
814	.932	740.325	01	4.76	-4283	.0196	0000	.0005	.0007	•0	060 0	.0000
815	. 935	742.149	00	5.97	•5277	.0200	0005	.0007	0004	• (	0061 0	.0000
810	•935	742.696	01	7.21	•6097	.0207	.0030	.0007	.0003	• (	060 0	.0000
817	-935	742.810	01	8.38	•6623	.0212	.0073	.0008	.0001	• (	060 0	.0000
818	•930	743.438	00	9.54	.7204	.0213	.0046	.0006	0004		059 (	.0000
819	-939	745.555	00	10.75	.8161	.0215	.0044	.0003	•0004	• (	058 (	.0000
820	.935	142.410	00	11.94	.8590	.0212	.0037	.0002	.0004	• (	057 0	.0000
821	.920	735.421	01	.06	0009	.0175	0001	.0008	.0009	• (	0062 0	.0000
	1ES1≈ 7	78 KUN=	50		STAR	ILITY AXIS (	COLFFICIENTS			STAR	PRESS.COEF	:=
POINT	MACH	Ų	BETA	ALPHA	CL	CD	CPM	CLS	CNS	£/D	CDB	PB-L
810	.933	141.242	00	11	•0026	•0204	.0037	•0003	.0008	.129	•0062	12.1015
811	.930	738.828	01	1.13	.1177	.0221	0037	•0006	.0008	5.324	.0062	12.1791
812	.932	140.224	01	2.35	. 2256	• 0295	0113	•0004	.0006	7.648	.0062	19.8977
813	.933	741.112	01	3.59	.3283	.0407	0175	•0002	.0006	8.069	.0061	24.0479
814	. 932	740.325	01	4.76	• 4252	.0551	0217	.0000	.0005	7.713	.0060	35.7816
815	.935	742.149	00	5.97	.5227	.0748	0266	0004	.0007	6.992	•0060	72.1453
816	.935	142.690	01	7.21	•6023	.0970	0262	•0031	.0003	6.207	.0059	99.4907
817	. 935	742.810	01	8.38	.6521	.1175	0110	.0074	0002	5.552	•0059	111.9028
818	.930	743.438	00	9.54	.7069	.1404	0066	•0046	0001	5.035	•0059	133-0422
819	.939	745.555	00	10.75	.7978	.1734	0181	•0044	0005	4.602	.0057	166.3997
820	.935	742.470	00	11.94	.8360	1985	0101	•0037	0006	4.212	-0056	188.1208
821	. 926	735.421	01	•06	0009	.0175	.0045	0001	.0008	052	.0062	11.1319

							S CUEFFICIENT			BODY PRESS.	
POINT	MACH	٥	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
836	.863	683.779	00	16	0088	.0159	.0006	.0008	0006	• 0052	0.0000
837	- 854	684.915	00	1.02	.0897	.0150	.0003	.0008	0012	.0053	0.0000
838	.864	684.918	00	2.17	.1917	.0120	.0002	.0007	0008	.0053	0.0000
839	.863	683.982	00	3.39	.2995	.0073	.0007	.0008	0009	.0052	0.0000
840	.861	682.392	00	4.61	-4114	.0033	.0006	.0007	0015	.0052	0.0000
841	.862	683.309	00	5.83	•5259	.0026	.0016	.0009	0017	• 0051	0.0000
842	.863	683.743	00	7.01	-6011	.0037	.0019	.0007	0005	.0051	0.0000
843	.864	684.825	00	8.10	.6303	.0082	0001	.0003	0009	.0051	0.0000
844	.864	685.181	00	9.23	•6725	.0111	.0022	•0006	0011	.0051	0.0000
845	-865	685.492	00	10.32	.6942	.0158	.0002	.0003	0011	.0051	0.0000
846	. 867	687.213	00	11.42	.7253	.0191	0005	.0003	0010	.0051	0.0000
847	-865	685.959	•00	12.53	.7644	.0204	0012	•0002	0008	.0050	0.0000
848	-865	685.938	.00	13.71	.8096	.0220	0006	.0002	0007	.0049	0.0000
849	.863	683.529	00	20	0124	.0158	0000	.0008	0011	.0053	0.0000

	TEST= 7	78 KUN=	51									
					STA	BILITY AXIS	COEFFICIENTS	•		STAB	.PRESS.COEF	F
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
836	.863	683.779	00	16	0087	.0159	.0052	.0006	.0008	549	.0052	13.0712
837	-864	684.915	00	1.02	.0894	.0166	•0089	٤٥٥٥.	.0008	5.381	.0053	13.4203
838	.864	684.918	00	2.17	.1911	.0192	.0118	•0002	.0007	9.952	.0053	13.9633
839	.863	683.982	00	3.39	.2986	•0250	.0128	.0008	-0007	11.938	.0052	14.6227
840	.861	082.392	00	4.61	.4098	.0363	.0099	.0007	.0007	11.277	.0052	25.0176
841	.862	683.309	00	5.83	.5229	.0560	.0021	.0017	.0007	9.340	.0051	40.2421
842	.863	083.743	00	7.01	.5961	.0771	.0077	.0020	.0005	7.732	.0051	67.2968
843	.864	684.825	00	8.10	.6228	• 0969	.0241	0001	.0003	6.424	.0051	147.4909
844	.804	685.181	00	9.23	•6620	-1188	.0348	.0023	.0002	5.572	.0050	159.7090
845	-865	685.492	00	10.32	•6802	.1399	•0435	.0003	.0003	4.862	.0050	175.1272
846	.867	687.213	00	11.42	.7071	.1623	-0484	0004	.0004	4.357	•0050	191.6117
847	-865	685.959	•00	12.53	.7418	.1857	.0532	0011	•0005	3.994	.0049	175.7087
848	-865	685.938	.00	13.71	.7813	.2132	.0558	0005	.0003	3.664	.0048	150.8845
849	.863	683.529	00	20	0124	.0159	.0046	0000	.0008	779	.0053	12.7609

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	1EST= 7	78 RUN= !	52									
							S COEFFICIEN	TS		BODY	PRESS-COEF	F
POINT	MACH	Ü	BETA	ALPHA	CNF	CÁF	CLB	CNB	CSF	C	AB	CAC
870	.805	032.715	00	24	0061	.0159	.0000	.0008	0002	• 0	048 0	.0000
871	<ul><li>80 5</li></ul>	632.865	01	•91	.0827	.0150	.0001	.0008	-0002	• 0	048 0	.0000
872	.807	634.361	01	2.09	.1766	.0118	.0001	.0008	.0005	• 0	048 (	.0000
873	.804	631.444	01	3.24	-2667	.0069	.0004	.0007	.0006			.0000
874	.806	633.125	01	4.43	.3621	.0006	.0005	.0007	.0009			.0000
875	.807	634.368	01	5.62	•4645	0049	•0002	.0007	.0014			.0000
876	.807	634.255	00	6.83	.5575	0049	•0009	.0006	.0002			.0000
877	.809	635.995	00	7.99	.6186	0014	•0003	.0003	.0011			0.000
878	.808	635.842	00	9.08	•6613	.0037	0002	.0002	.0020			0.000
879	.807	634.613	00	10.20	.7023	.0077	•0001	.0002	.0012			0.0000
880	.808	635.496	00	11.32	.7312	.0125	0007	.0001	•0025			0.0000
881	.808	634.994	00	12.41	•7602	.0153	0009	0000	.0023			0.0000
882	.809	636.818	00	13.57	.7940	.0172	•0000	.0000	.0022			0.0000
883	.809	636.348	00	15.81	.8568	.0199	•0004	.0001	.0023			0.0000
884	-813	639.704	01	18.01	.9326	.0222	•0003	0001	•0042			0.0000
885	.811	638.025	01	20.14	1.0117	.0237	.0008	0002	•0057			0.0000
886	.813	639.917	01		1.0940	.0230	.0017	0011	.0110			0.0000
887	.807	634.276	01	6.93	.5610	0048	.0010	.0007	.0012			0.0000
001	•001	0344210	•01	0.75	• 7010	*0040	•0010	•0001	*0012	• '	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0.0000
	TEST= 7	78 RUN=	52									
					STAB	LITY AXIS (	COEFFICIENTS			STAB	PRESS.COE	F F
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	P8-1
870	-805	632.715	00	24	0060	.0159	•0052	.0000	-0008	377	.0048	8.8820
871	-805	032.865	01	•91	.0825	.0163	•0099	.0001	.0008	5.055	.0048	9.4444
872	.807	634.361	01	2.09	.1761	.0183	.0147	.0001	•0008	9.646	.0048	9.6771
873	-804	631.444	01	3.24	.2659	.0219	.0194	•0005	.0007	12.116	.0048	10.5886
874	-836	633.125	01	4.43	.3610	•0285	.0243	.0006	•000 <b>7</b>	12.653	.0048	11.6552
875	- 807	634.368	01	5.62	.4627	•0406	•0266	.0003	-0007	11.384	•0048	15.7475
876	.807	634.255	00	6.83	• 5541	.0614	.0287	.0009	•0005	9.021	.0047	47.1269
877	.809	635.995	00	7.99	.6128	.0846	.0369	.0003	•0002	7.244	.0046	61.7693
878	-808	635.842	00	9.08	• 6525	.1080	•0458	0002	•0002	6.039	-0046	86.1089
879	.807	634.613	00	10.20	.6898	.1319	-0537	.000 L	.0002	5.229	.0046	106.6665
880	.808	635.490	00	11.32	.7145	<ul><li>1558</li></ul>	.0617	0007	•0002	4.587	.0046	121.6000
881	-808	634.994	00	12.41	.7392	.1783	•0682	0009	.0002	4.145	.0045	132.0727
882	<b>.</b> 809	636.818	00	13.57	.7678	.2031	.0746	.0000	0000	3.781	.0044	123.9272
883	•809	630.348	00	15.81	.8189	- 2520	.0834	.0004	.0000	3.242	.0042	125.0909
884	.813	639.704	01	18.01	.8800	.3095	.0799	.0003	0002	2.843	.0038	151.8545
885	-811	638.025	01	20.14	•9416	.3707	.0766	.0007	0005	2.540	•0029	171.0545
886	-813	639.917	01	22.27	1.0036	.4359	.0794	•0012	0017	2.302	.0021	175.9999
887	.807	634.276	01	6.93	•5575	.0629	.0293	.0010	•0006	8.862	.0047	47.9027

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	73 RUN=	53									
						BODY AXI	S COEFFICIEN				PRESS.COE	
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
901	.753	582.255	00	12	0065	.0156	.0000	.0008	0001			0.0000
902	.753	582.334	01	1.00	.0742	.0148	.0002	•0009	•0002			0.0000
903	.754	583.381	00	2.10	.1646	.0119	.0002	.0009	0005	•!		0.0000
904	.753	582.422	00	3.26	.2476	.0074	•0002	.0009	0001	• (		0.0000
905	.755	584.085	00	4.39	•3335	.0012	.0006	.0008	.0001			0.0000
906	.753	582.728	00	5.55	•4250	0047	.0005	.0008	0006	•	0046	0.0000
907	.754	583.049	01	0.74	.5137	0053	.0015	.0013	0007			0.0000
908	.753	582.234	00	7.85	.5733	0013	.0010	.0006	.0002			0.0000
909	.754	582.938	00	8.99	.6269	.0028	.0001	-0003	.0014	•	0045	0.0000
910	.754	583.567	00	10.10	.6851	•0053	.0003	.0003	.0005	•		0.0000
911	.755	583.841	00	11.27	•7235	.0077	0001	.0002	.0003	•	0044	0.0000
912	•725	584.278	00	12.34	.7582	.0107	.0004	.0002	.0006	• 1		0.0000
913	.757	586.153	00	13.48	.7826	.0137	.0008	.0002	.0011			0.0000
914	.755	584.483	00		.8388	.0176	.0009	.0001	.0016	•	0042	0.0000
915.	.757	586.470	00	17.87	.9056	.0202	.0007	0000	.0025	•	0039	0.0000
916	.750	587.102	01	20.00	.9718	.0226	.0001	.0002	.0026	•		0.0000
917	.759	588.135	01	22.10	1.0454	.0221	.0011	0006	.0062	•		0.0000
918	.752	581.572	01	10	0106	.0155	.0002	.0009	.0010	•	0046	0.0000
	IEST= 7	78 KUN=	53		CT 4.0	ILITY AXIS C	OFFERENCE			CTAD	.PRESS.COE	EE
				A . O	CL	CD CD	CPM	CLS	CNS	L/D	CDB	PB-1
POINT	MACH	Q	BETA	ALPHA	0065	•0156	•0045	•0000	.0008	417	•0045	14.8942
901	.753	582.255	00	12		.0161	.0098	.0003	•0009	4.599	•0046	14.3512
902	-753	582.334	01	1.00	.0740 .1641	.0180	.0147	•0002	•0009	9.131	•0046	14.7003
903	•754	583.381	00	2.10	• 1541 • 2468	.0215	.0201	.0002	.0009	11.491	•0046	15.3209
904	. 75 3	582.422	00	3.26 4.39	• 3325	.0267	.0255	.0007	.0007	12.441	•0046	16.6784
905	.755	584.085 582.728	00	5.55	• 4234	.0364	.0293	.0006	•0007	11.617	•0045	23.2722
906	•753		00	6.74	•5108	.0551	.0313	.0010	-0012	9.279	•0045	38.0118
907	.754	583.049	01	7.85	•5081	.0771	.0391	.0010	.0005	7.371	.0044	58.5693
908	.753	582.234	00	8.99	.6188	.1007	.0483	.0002	•0003	6.144	.0045	77.7695
909	•754	582.938	00 00	10.10	.6736	.1254	.0571	•0004	•0003	5.373	•0044	96.9695
910	•754 •755	583.567 583.841		11.27	.7081	.1490	•0666	0001	-0002	4.753	.0043	105.8907
911			00	12.34	.7383	.1725	.0754	•0004	.0001	4.281	.0042	107.8301
912	•755	584.270	00 00	13.48	.7578	.1958	.0832	.0009	•0000	3.871	•0042	104-1452
913	.757	580.153	00	15.73	.8026	• 2443	.0914	.0009	0001	3.285	.0042	112.0967
914	•755	584.483	00	17.87	• 8020 • 8557	.2443	.0920	.0006	0003	2.880	.0037	122.4727
915	•757	586.476 587.102	00	20.00	9054	.3537	.0854	•0002	•0002	2.560	.0030	138.4727
916	•758 •759	588.135	01	22.10	.9602	•4138	.0887	•0002	0002	2.320	.0022	149.2363
917		581.572	01	10	0105	.0155	.0044	•0002	•0009	680	.0046	14.7391
918	• <b>7</b> 52	2010215	01	10	0103	.0177	•0077	-000L	•0007	•000	\$0010	2 / L

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	1521- 1	IO RUN= :	94									
							S COEFFICIEN	TS		BODY	PRESS.COEF	F
POINT	MACH	ú	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	C	AB	CÅC
932		530.488	01	07	0095	.0158	0001	.0010	0000	• 0	044 0	•0000
933	.702	530.023	01	1.01	.0704	.0150	0003	.0010	.0007	.0	044 0	•0000
934	•703	531.281	00	2.12	·1505	.0122	.0001	•0008	0003	• 0	044 0	.0000
935	.731	529.723	00	3.20	.2311	.0078	.0005	•0009	.0001			.0000
936	.731	529.818	00	4.34	.3136	•0019	.0008	•0009	0009			•0000
937	.701	529.461	00	5.44	.3917	0043	.0007	<b>8000</b>	0002			•0000
938	.702	530.205	00	6.63	•4867	0061	.0007	.0008	0010			•0000
939	.703	531.956	00	7.75	-5581	0023	•0004	.0005	0000			• 0000
940	.732	540.585	00	8.87	•6091	.0010	.0008	•0005	.0003			.0000
941	.702	530.783	00	9.90	•6581	.0037	.0004	•0005	0001			.0000
942	.702	530.451	00	11.11	.7075	.0059	0003	.0003	0002			•0000
943	.702	530.199	00	12.20	.7403	.0088	.0004	.0003	.0002			•0000
944	.703	531.537	00	13.36	.7747	.0112	.0009	-0001	.0006			•0000
945	.703	531.464	00	15.60	.8320	.0154	.0013	.0002	.0010			•0000
946	. 703	531.788	00	17.72	.8913	.0178	.0014	0001	.0017			•0000
947	.704	532.725	00	19.81	•9550	•0211	.0004	•0003	•0009			•0000
948	.706	534.854	00	21.88	1.0137	.0215	0002	.0002	.0022			•0000
949	.730	528.071	00	10	0114	.0158	•0003	.0010	0003			•0000
										_		
	TEST= 7	78 RUN=	54		( T A 1)		0.55101000					_
DOTALT	44.2.1		01.74	41.01.4		ILITY AXIS C					PRESS.COEF	
PUINT	MACH	, JO ( 0 )	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CD8	PB-1
932 933	•702 •702	530.486	01	07	0094	-0158	.0042	0001	.0010	598	-0044	7.1172
		530.023	01	1.01	.0701	-0162	•0105	0003	.0010	4.317	+0044	6.2639
934	703	531.281	00	2.12	.1499	.0178	.0154	.0001	.0008	8.427	•0044	6.8845
935	- 701	529.723	00	3.20	.2303	.0207	.0211	•0005	• 0009	11.149	.0044	6.4385
936	.701	529.818	00	4.34	• 3126	•0256	.0268	.0008	.0008	12.192	•0044	7.0009
937	.701	529.461	00	5.44	- 3904	•0328	.0324	.0008	.0008	11.897	.0043	7.5051
938	702	530.205	00	6.63	-4041	.0501	.0339	.0008	.0007	9.661	-0043	26.1233
939	.733	531.956	00	7.75	•5533	.0730	.0398	•0005	•0005	7.576	•0042	55.9511
940	.732	230.585	00	8.87	.6017	•0949	.0499	.0009	•0004	6.338	.0042	74.0847
941	.702	530.783	00	9.96	.6475	.1175	•0599	•0005	.0004	5.511	.0042	91.3453
942	-702	530.451	00	11.11	.6931	.1422	.0706	0002	-0004	4.875	.0041	105.5028
943	.702	530.199	00	12.20	.7217	.1650	.0783	•0005	•0002	4.373	•0041	105.6968
944	•733	531.537	00	13.36	.7511	-1898	.0871	•0009	0001	3.957	.0040	106.6665
945	-703	531.464	00	15.60	• 7972	-2386	• 0965	.0013	0001	3.342	.0039	112.0967
946	-703	531.788	00	17.72	• 8436	-2883	•0996	.0013	0005	2.926	•0036	112.2907
947	•704	232.725	00	19.81	.8913	.3435	.0926	.0004	•0001	2.595	•0029	123.3452
948	• 706	534.854	00	21.88	.9327	•3977	•0931	0002	.0002	2.345	•0022	144.2909
949	.700	52d•077	00	10	0114	.0159	•0035	•0003	.0010	717	•0043	6.5160

BODY AXIS COEFFICIENTS

BODY PRESS.COEFF

							S COEFFICIE	VIS			PRESS.COE	FF
POINT	MACH	ų.	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
964	.242	120.479	00	09	0095	.0168	•0005	.0005	0004	•	0037	0.0000
965	-293	121.252	00	.91	.0479	.0166	.0018	.0007	0019	•		0.0000
966	.293	121.155	00	1.86	-1134	.0147	.0005	.0004	0016			0.0000
967	.292	120.577	.00	2.90	.1811	.0116	.0012	.0002	0028	•		0.0000
968	.293	121.351	•00	3.88	.2402	.0074	.0017	.0004	0038	• 1	0036	0.0000
969	-293	121.353	•00	4.89	.3125	.0015	.0016	.0001	0044	•	0036	0.0000
970	.293	121.355	.00	5.96	.3777	0056	.0003	.0004	0040			0.0000
971	.293	121.362	•00	7.00	.4449	0117	.0010	0004	0050	•	0036	0.0000
972	.293	121.280	.00	8.04	.5199	0149	•0002	•0005	0051			0.0000
973	د 29ء	121.308	•00	9.09	.5961	0116	•0009	.0002	0062		0035	0.0000
974	.293	121.332	.00		•0527	0114	.0014	.0004	0073			0.0000
975	.243	121.358	.00	11.21	.7095	0117	.0019	.0001	0083			0.0000
976	-293	121.486	•00	12.33	• 7555	0096	.0021	.0003	0091			0.0000
977	.292	120.206	•00	14.49	.8351	0011	.0013	0004	0038			0.0000
978	-292	120.860	.00	16.56	.9114	.0042	0001	0000	0038			0.0000
979	-292	120.250	.00		•9602	.0070	0001	0004	0044		0029	0.0000
980	.293	121.007	.00		1.0241	.0113	0002	0006	0048			0.0000
981	.293	121.378	•00	8.01	•5195	0139	.0002	.0005	0051	•	0037	0.0000
	7EST= 7	78 KUN=	55		H A T 2	ILITY AXIS C	OFFERT			STAR	.PRESS.COE	r.c
POINT	MACH	٥	BETA	ALPHA	CL	CD CD	CPM	CLS	CNS	L/D	CDB	PB-1
964	.292	120.479	00	09	0095	•0168	•0024	•0005	•0005	566	.0037	.0388
965	.293	121.252	00	.91	.0476	.0173	.0089	.0019	.0006	2.749	.0036	0776
966	.293	121.155	00	1.86	•1128	.0184	.0156	.0005	•0004	6.128	.0036	.0776
967	.292	120.577	•00	2.90	.1802	.0207	.0225	.0012	.0001	8.702	.0037	0.0000
968	.293	121.351	• 00	3.88	. 2451	•0241	.0291	.0017	.0003	10.185	.0036	.5818
969	.293	121.353	•00	4.89	.3112	•0282	.0330	.0017	.0000	11.038	.0036	•7951
970	.293	121.355	•00	5.96	.3762	.0337	.0369	•0003	.0004	11.165	.0036	•9309
971	.293	121.362	•00	7.00	•4430	.0426	.0380	.0010	0005	10.390	.0036	2.6568
972	.293	121.280	•00	8.04	.5109	.0580	.0422	.0002	.0004	8.913	.0036	12.7221
973	.293	121.308	•00	9.09	.5905	•0827	.0463	.0009	.0001	7.141	.0035	30.7777
974	.293	121.332	•00	10.18	.0444	•1042	.0555	.0015	.0002	6.185	.0035	31.1270
975	. 293	121.358	•00	11.21	. 6982	-1265	-0648	.0019	0002	5.520	.0033	36.6543
976	. 293	121.486	•00	12.33	.7401	.1519	.0737	.0021	0001	4.871	.0033	45.6724
977	.292	120.206	•00	14.49	.8089	.2079	.0949	.0012	0007	3.891	.0031	55.1754
978	. 292	120.860	•00	16.56	.8724	-2638	.1094	0001	.0000	3.307	.0029	54.0117
979	.292	120.250	•00	18.58	.9079	.3127	.1186	0002	0003	2.904	.0028	47.7087
980	.293	121.007	-00	20.58	.9547	.3706	.1167	0004	0005	2.576	•0024	53.0420
981	- 293	121.378	.00	8.01	.5164	.0587	•0422	.0002	.0004	8.798	.0036	14.3900

TEST= 778 RUN= 55

	TEST= 7	78 RUN= 5	56								
						BODY AXI	S COEFFICIEN	TS		BODY PRESS.	COEFF
TAIOS	MACH	Q	BETA	ALPHA	CNF	CAF	ÇLB	CNB	CSF	CAB	CAC
982	-497	312.326	00	10	0150	.0173	.0000	.0007	0023	•0039	0.0000
983	•496	311.706	00	•89	.0547	.0167	.0002	.0008	0008	.0039	0.0000
984	.498	313.125	00	1.92	.1349	.0145	0001	•0007	0014	•0040	0.0000
985	•497	312.507	00	3.05	•1976	.0105	0001	.0006	0019	• 0039	0.0000
986	•497	312.510	•00	4.09	.2636	•0056	0002	•0006	0026	•0039	0.0000
987	.498	313.132	00	5.12	•3362	0017	0002	•0005	0009	•0039	0.0000
988	.496	311.991	•00	6.19	.4078	0091	.0002	•0002	0018	.0039	0.0000
989	•497	312.750	00	7.34	<b>.</b> 4874	0112	.0002	.0001	0001	.0039	0.0000
990	•498	313.450	00	8.45	•5630	0084	.0002	•0004	0009	•0038	0.0000
991	•498	313.709	-00	9.50	•6247	0061	•0005	•0002	0018	•0038	0.0000
992	.498	313.714	•00	9.53	•6320	0060	.0005	.0003	0019	.0038	0.0000
993	•497	312.555	00	10.67	.6703	~.0042	•0003	•0002	0001	.0037	0.0000
994	.497	312.733	00	11.69	•7173	0019	-0002	•0002	0007	.0037	0.0000
995	-498	313.454	•00	12.77	.7591	.0011	.0004	.0002	0014	.0037	0.0000
996	•498	313.141	•00	15.01	<b>.</b> 8424	•0064	-0010	•0001	0006	•0036	0.0000
997	-498	313.172	•00	17.19	.8958	•0099	.0011	•0001	0014	•0035	0.0000
998	.499	314.550	00	19.22	•9552	•0134	.0004	•0000	•0009	-0031	0.0000
999	• 499	314.638	00	21.27	1.0403	-0164	.0003	0001	•0004	• 0025	0.0000
0	•498	313.186	00	8.40	•5672	0086	.0001	•0004	0008	•0038	0.0000

	TEST= 7	78 RUN=	56									
•					STA	BILITY AXIS	COEFFICIENTS			STAB	.PRESS.COEFF	:
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
982	•497	312.326	00	10	0150	.0173	.0028	-0000	.0007	865	.0039	3.1223
983	-496	311.706	00	.89	• 0544	.0176	.0087	•0002	.0008	3.094	.0039	3.3356
984	<b>.498</b>	313.125	00	1.92	• 1344	.0190	.0147	0001	.0007	7.071	.0040	3.1998
985	•497	312.507	00	3.05	• 1968	.0210	.0204	0001	•0006	9.352	.0039	3.0835
986	•497	312.510	.00	4.09	· 2625	.0244	•0261	0001	.0007	10.765	.0039	3.1223
987	.498	313.132	00	5.12	•3350´	.0283	.0309	0002	.0006	11.843	.0038	3.1611
988	•496	311.991	.00	6.19	• 4064	.0350	.0357	•0002	.0002	11.622	.0039	3.7235
989	•497	312.750	00	7.34	• 4849	.0512	.0384	•0002	.0001	9.477	.0038	16.6396
990	.498	313.450	00	8.45	•5582	.0744	.0443	•0003	.0004	7.499	.0038	37.7013
991	•498	313.709	.00	9.50	•6172	.0970	•0542	•0005	.0002	6.359	.0037	62.8359
992	•498	313.714	-00	9.53	• 6243	.0988	-0544	•0005	•0002	6.320	.0037	62.6423
993	•497	312.555	00	10.67	•6595	.1199	-0660	•0003	.0002	5.500	.0036	73.5029
994	•497	312.733	00	11.69	. <b>7</b> 028	.1435	.0756	•0003	.0002	4.898	.0036	83.9756
995	.498	313.454	.00	12.77	-7400	.1689	.0838	.0004	.0001	4.381	.0036	91.1513
996	.498	313.141	.00	15.01	.8120	.2244	.1006	.0010	0001	3.619	.0035	94.0604
997	•498	313.172	•00	17.19	•8528	.2742	-1102	.0011	0002	3.111	.0033	85.5271
998	.499	314.550	00	19.22	•8976	.3271	•1121	•0004	0001	2.744	.0030	93.4786
999	•499	314.638	00	21.27	• 9634	.3927	.1098	.0003	0002	2.453	.0023	94.4483
0	-498	313.186	00	8-40	•5623	.0744	.0434	.0002	.0004	7.562	.0038	39.9512

	TEST= 7	78 RUN=	57									
						BODY AX	IS COEFFICIEN	NTS		BODY	PRESS-COE	÷F
PCINT	MACH	ú	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
74	•932	740.028	01	26	0003	.0205	•0005	.0007	•0003		0061	0.000
75	.930	738.750	-•01	1.01	•1332	.0201	.0012	.0007	.0002		0061 (	00000
76	•931	739.669	00	2.22	•2574	.0209	.0022	•0006	0002	• (	0061 (	0.000
77	•931	739.557	00	3.45	•3756	.0211	.0013	.0005	.0003	•(	0061 (	0.000
78	.932	739.996	00	4.62	•4697	.0216	.0002	•0005	0003	• (	0060	0.000
79	.934	741.817	00	5.86	•5733	.0220	.0010	•0004	•0005	.(	060 (	0.000
80	•936	743.129	00	7.10	•6554	.0242	.0009	.0003	0001	• (	0060	0.000
81	<b>ددو.</b>	740.754	00	8.24	.7059	•0242	0043	0000	.0011	• (	059	0.000
82	• 938	744.655	00	9.44	.7879	•0256	0007	.0001	.0001	• 4	0059 (	0.000
83	.937	744.351	00	10.58	-8488	.0258	.0005	.0001	.0003	• (	057 (	0.000
84	•929	737.336	01	20	0048	.0182	.0011	.0008	.0007	•(	0061 (	•0000
	TEST= 7	78 RUN=	57		STAR	IIITY AXIS	COLFFICIENTS			STAR	.PRESS.COEI	: <b>F</b>
POINT	MACH	U	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	P8-1
74	.932	740.028	01	26	0002	.0205	•0056	•0005	•0007	012	•0061	15.3230
75	.930	738.756	01	1.01	.1328	.0224	0044	.0012	.0006	5.928	.0061	18.7999
76	.931	739.669	00	2.22	. 2564	.0309	0164	.0023	•0006	8.309	.0061	16.4306
77	.931	739.557	00	3.45	.3736	.0437	0238	.0013	•0005	8.557	.0061	21.6614
78	.932	739.996	00	4.62	• 4664	.0594	0231	.0003	•0005	7.855	.0060	36.3077
79	-934	741.81/	00	5.86	•5680	.0804	0272	.0010	.0003	7.064	•0060	62.6153
80	•936	743.129	00	7-10	•6474	.1050	0201	.0009	.0002	6.165	•0060	88.7691
81	.933	740.754	00	8.24	.6951	.1251	.0036	0043	.0006	5.557	•0059	116.4614
82	.938	744.655	00	9.44	• 7730	.1544	0004	0007	•0002	5.005	.0058	140.9229
83	•937	744.351	00	10.58	.8296	.1812	.0062	•0006	0000	4.579	.0057	183.3844
84	•929	737.336	01	20	0047	.0182	•0068	.0011	.0008	261	.0061	16.6153

	1521= 1	/8 RUN=	9 8									
							S COEFFICIEN				PRESS.COEF	F
PGINT	MACH	ú	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	C	AB	CAC
98	-801	602.149	01	27	0091	•0164	.0003	.0008	•0005	• 0	052 0	0.0000
99	.862	682.790	00	•92	.1008	.0154	.0006	.0007	0005	• 0	052 (	0.0000
100	.865	685.065	00	2.12	.2134	.0116	.0010	.0006	0005	•0	053 (	0.0000
101	.802	682.934	01	3.36	.3406	.0066	.0010	.0007	0001	.0	052 (	0:0000
102	.863	683.294	01	4.59	•4655	•0039	.0008	.0008	0004	.0	051 (	0.000
د 10	.802	682.424	00	5.80	•5708	.0051	•0008	.0004	0000	.0	051 (	0.0000
104	- 862	682.927	00	6.96	.6418	.0077	•0002	.0003	0004	• 0	051	0.0000
105	.864	684.718	00	8.11	.6649	.0128	0009	•0002	0002	.0	051	0.0000
106	-865	685.004	00	9-17	•6854	.0171	0006	.0003	0001	• 0	051 (	0.000
107	.865	085.394	00	10.29	.7186	.0199	.0009	.0004	0001	• 0	051	0.0000
108	·807	687.045	00	11.41	.7462	.0225	.0008	.0004	.0007	.0	050	0.0000
109	.800	686.397	00	12.52	.7829	.0242	.0003	.0003	.0008	•0	050	0.0000
110	.857	686.721	00	13.70	.8284	•0249	•0003	.0004	.0003	•0	1049	0.0000
111	. 807	686.679	00	16.03	.9152	.0258	.0004	.0003	.0005	• (	047	0.0000
112	.870	649.118	00	18.23	1.0048	.0266	.0004	.0007	0001	•0	043	0.0000
113	. 403	683.508	01	19	0156	.0158	.0007	.0008	.0013	• 0	052 (	0.0000
	TEST= 7	78 RUN=	58									
					STABI	LITY AXIS (	COEFFICIENTS			STAB	PRESS.COE	FF
PGINT	MACH	J	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
98	.861	682.149	01	27	0090	.0164	.0088	•0003	.0008	551	•0052	12.5230
99	.862	082.790	00	.92	.1005	.0170	.0117	.0006	.0007	5.910	•0052	12.9845
100	.865	685.065	00	2.12	.2128	-0194	.0143	.0010	.0006	10.953	.0053	18.2768
101	.862	682.934	01	3.36	.3396	•0265	.0129	.0010	.0007	12.810	.0052	20.0614
102	.803	683.294	01	4.59	•4637	.0412	.0053	•0008	.0008	11.255	.0051	24.0769
103	.862	682.424	00	5-80	•5674	-0628	.0090	.0008	.0004	9.037	.0051	59.6922
104	-802	082.927	00	6.96	.6361	•0854	.0249	.0003	.0003	7-445	.0050	83.5384
105	.864	684.718	00	8.11	• 6564	-1064	.0501	0008	.0003	6.167	.0050	115.8460
106	•805	685.004	00	9.17	.6739	-1261	.0691	0006	.0004	5.342	.0050	116.0768
107	.865	085.394	00	10.29	.7035	•1479	.0818	-0010	.0002	4.758	.0050	113.0768
108	.85/	687.045	00	11.41	.7270	.1697	.0895	.0008	•0002	4.285	•0049	120.9230
109	.800	686.397	00	12.52	. 7591	•1933	.0964	•0003	•0003	3.926	.0049	129.6922
110	. Bo 7	686.721	00	13.70	. 7995	. 2206	.1027	•0004	.0003	3.625	.0047	131.5383
111	.867	086.679	00	16.03	.8725	.2774	.1133	•0005	•0002	3.145	•0045	109.1537
112	.870	689.118	00	18.23	.9461	• 3396	•1125	•0006	.0005	2.786	.0040	125.9999
113	.863	683.508	01	19	0156	•0159	.0083	.0007	•0008	980	.0052	15.8460
												1712.00

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	59									
			-			BODY AXI	S COEFFICIEN	TS		BODY	PRESS.COE	FF
PCINT	MACH	Ų	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
127	-805	631.189	01	25	0114	-0160	.0005	.0008	.0005		0047	0.0000
128	.807	632.611	01	.91	-0447	.0152	.0008	.0008	.0006	• (		0.0000
129	.806	631,613	01	2.05	.1910	.0118	.0008	.0008	0001	. (		0.0000
130	-806	631.778	01	3.24	·2950	•0060	.0012	.0008	0001	• (	0048	0.0000
131	.8J6	631.824	00	4.41	.4004	0005	.0008	.0007	0004	• (	0047	0.0000
132	.805	630.972	00	5.61	•5089	0044	.0011	.0006	0002	• (	0047	0.0000
133	.806	632.417	00	6.81	•5928	0026	.0013	.0006	0002	• (	3047	0.0000
134	.806	632.193	~.00	7.93	.6385	.0031	•0004	.0005	0002	• (	0047	0.0000
135	.807	632.915	00	9.05	.6790	•0085	.0011	•0006	0004	• (	0047	0.0000
136	. 807	033.346	00	10.13	.7116	.0126	.0001	.0004	0001	• (	0047	0.0000
137	.807	632.708	00	11.25	.7408	.0164	.0005	.0004	.0002	• (	0046	0.0000
138	. 808	634.015	00	12.35	.7711	•0194	.0004	.0003	.0010	. (	0046	0.0000
139	.810	635.645	00	13.51	.8012	.0211	.0007	.0004	.0002	• (	0046	0.0000
140	.810	635.388	00	15.79	.8726	.0236	.0004	.0007	0014	٠.	0044	0.0000
141	.806	631.984	00	17.94	.9437	.0241	.0003	•0009	0006	• (	0040	0.0000
142	.811	636.932	00	20.06	1.0283	.0253	0001	.0011	0019	• (	0033	0.0000
143	.807	632.877	01	24	0115	.0158	.0004	.0008	.0006	• (	0048	0.0000
144	.806	631.379	01	25	0130	.0158	.0008	.0007	.0002	• (	0047	0.0000
	1EST= 7	78 RUN=	59									
					STAB	ILITY AXIS	OEFFICIENTS			STAB.	PRESS.COE	FF
POINT	MACH	ن	BETA	ALPHA	CL	CO	CPM	CLS	CNS	L/D	CDB	PB-1
127	.805	631.189	01	25	0113	.0160	.0076	.0005	.0008	708	.0047	13.3845
128	.807	632.611	01	.91	.0885	.0166	.0125	.0008	.0008	5.319	.0048	11.5999
129	.806	631.613	01	2.05	. 1905	.0186	.0164	.0009	.0008	10.256	.0048	13.7230
130	-806	631.178	01	3.24	• 2942	.0227	.0216	.0013	.0007	12.954	.0048	11.1691
131	.806	631.824	00	4.41	. 3992	.0304	.0263	.0008	.0007	13.153	.0047	13.3230
132	.805	630.972	00	5.61	• 5069	.0454	.0293	.0011	.0005	11.170	.0047	21.6614
133	.806	632.417	00	6.81	•5889	.0678	.0415	.0014	.0004	8.688	.0047	46.1538
134	-806	632.193	00	7.93	.6320	.0911	.0625	•0005	•0005	6.937	.0046	69.2307
135	.807	632.915	00	9.05	•6692	.1152	.0789	.0011	.0004	5.811	-0046	81.3845
130	-807	633.346	00	10.13	د698ء	.1376	.0924	.0002	.0003	5.076	.0046	92.9230
137	.807	632.708	00	11.25	•7233	.1606	.1044	•0006	.0003	4.503	.0045	97.8461
138	- 808	634.015	00	12.35	.7491	.1839	.1135	•0004	.0003	4.073	•0045	104.1537
139	-810	635.645	00	13.51	.7741	·2077	.1224	.0007	.0002	3.727	-0045	100.9230
140	.810	635.388	00	15.79	.8333	.2601	.1324	.0006	.0006	3.203	.0042	93.2307
141	.806	631.984	00	17.94	.8904	.3136	.1363	.0006	.0008	2.839	-0038	106.1537
142	.811	636.932	00	20.06	.9572	.3765	.1342	.0003	.0010	2.542	.0031	118.4614
143	.807	632.877	01	24	0114	.0159	.0082	.0004	.0008	722	.0048	10.8615
144	-806	631.379	01	25	0129	.0159	.0075	.0008	.0008	815	.0047	11.5076

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN= 6	60			9.00.4.4.1	S COEFFICIEN	TC		BONV	PRESS.COEF	F
			0.5.7.4		CNE							
POINT	MACH	Q 533	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		AB	CAC
158	.753	580.533	01	22	0145	•0159	-0004	.0008	.0007			•0000
159	.753	581.214	~.01	.88	.0745	.0152	.0003	•0008	-0001			•0000
160	•752	580.248	01	2.02	-1740	.0120	.0007	•0008	-0002			<b>.</b> 0000
161	-753	580.781	00	3.18	• 2652	.0069	•0009	•0008	0006			• 0000
162	.754	581.487	00	4.33	•3617	.0002	.0008	.0007	.0000	•0	0046 0	.0000
163	.753	581.139	00	5.49	•4571	0040	.0010	•0008	0009	• (	0045 0	•0000
164	•753	580.897	00	6.67	•5383	0028	.0018	.0010	0012	•0	0045 0	•0000
165	.754	582.107	00	7.81	•6037	0001	.0023	.0010	0013	• (	0045 0	.0000
166	.756	583.388	00	8.93	•6397	.0077	.0008	•0005	.0005	• (	0045 0	.0000
167	.755	582.603	00	10.05	•6870	.0100	•0006	•0005	.0001	• (	0045 0	.0000
168	.755	582.887	00	11.17	.7290	.0126	•0005	•0006	.0007	•0	0044 0	.0000
169	.755	583.160	00	12.23	.7575	.0154	.0006	-0006	.0001			.0000
170	.756	583.993	00	13.41	.7872	.0176	.0005	.0004	0002			.0000
172	.757	584.529	00	15.64	.8482	.0208	.0003	•0006	0007			.0000
173	.758	585.547	00	17.78	9146	.0222	•0004	•0008	0013			.0000
174	.756	584.023	00	19.90	•9956	.0243	-0002	-0009	0015			.0000
175	.755	583.088	00	22.02	1.0681	.0229	.0003	•0009	0009			0.0000
176	.753	580.768	01	22	0129	.0158	0001	•0009	-0011			.0000
110	• 175	300-100	- • 0 1	22	******	•0138		40009	-0011	• \	0040	
	TEST= 7	78 RUN=	60		CTAD	TITTY AVIC C	GEELCIENTS			CTIO	22566 225	-
DO NIT				41.004		BILITY AXIS C		C1 C	244		.PRESS.COEF	
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
158	MACH •753	Q 580•533	BETA 01	22	CL 0144	CD •0159	CPM •0075	.0004	.0008	L/D 905	CDB •0046	PB-1 11•9999
158 159	MACH •753 •753	Q 580.533 581.214	BETA 01 01	22 .88	CL 0144 .0743	CD •0159 •0163	CPM .0075 .0134	.0004 .0003	.0008 .0008	L/D 905 4.551	CDB •0046 •0046	PB-1 11.9999 10.0307
158 159 160	MACH •753 •753 •752	Q 580.533 581.214 580.248	BETA 01 01 01	22 .88 2.02	CL 0144 -0743 -1735	CD •0159 •0163 •0181	CPM .0075 .0134 .0181	.0004 .0003 .0008	.0008 .0008 .0008	L/D 905 4.551 9.563	CDB •0046 •0046 •0046	PB-1 11.9999 10.0307 11.8768
158 159 160 161	MACH •753 •753 •752 •753	Q 580.533 581.214 580.248 580.781	BETA 01 01 01 00	22 .88 2.02 3.18	CL 0144 -0743 -1735 -2644	CD •0159 •0163 •0181 •0216	CPM .0075 .0134 .0181 .0229	.0004 .0003 .0008 .0010	.0008 .0008 .0008 .0007	L/D 905 4.551 9.563 12.233	CDB •0046 •0046 •0046 •0046	PB-1 11.9999 10.0307 11.8768 12.2153
158 159 160 161 162	MACH •753 •753 •752 •753 •754	Q 580.533 581.214 580.248 580.781 581.487	BETA 01 01 01 00 00	22 .88 2.02 3.18 4.33	CL 0144 -0743 -1735 -2644 -3606	CD .0159 .0163 .0181 .0216 .0275	CPM .0075 .0134 .0181 .0229 .0294	.0004 .0003 .0008 .0010	.0008 .0008 .0008 .0007	L/D 905 4.551 9.563 12.233 13.102	CDB •0046 •0046 •0046 •0046 •0045	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538
158 159 160 161 162 163	MACH •753 •753 •752 •753 •754	Q 580.533 581.214 580.248 580.781 581.487 581.139	BETA 01 01 01 00 00	22 .88 2.02 3.18 4.33 5.49	CL 0144 -0743 -1735 -2644 -3606 -4554	CD .0159 .0163 .0181 .0216 .0275 .0398	CPM .0075 .0134 .0181 .0229 .0294 .0325	.0004 .0003 .0008 .0010 .0009	.0008 .0008 .0008 .0007 .0006	L/D 905 4.551 9.563 12.233	CDB •0046 •0046 •0046 •0046 •0045	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 15.9383
158 159 160 161 162 163 164	MACH •753 •753 •752 •753 •754 •753	Q 580.533 581.214 580.248 580.781 581.487 581.139 580.897	BETA 01 01 01 00 00 00	22 .88 2.02 3.18 4.33 5.49 6.67	CL 0144 .0743 .1735 .2644 .3606 .4554	CD •0159 •0163 •0181 •0216 •0275 •0398 •0598	CPM .0075 .0134 .0181 .0229 .0294 .0325 .0445	.0004 .0003 .0008 .0010 .0009 .0011	.0008 .0008 .0008 .0007 .0006 .0007	L/D 905 4.551 9.563 12.233 13.102 11.447 8.948	CDB •0046 •0046 •0046 •0045 •0045 •0045	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 15.9383 37.0769
158 159 160 161 162 163	MACH •753 •753 •752 •753 •754	Q 580.533 581.214 580.248 580.781 581.487 581.139 580.897 582.107	BETA 01 01 01 00 00	22 .88 2.02 3.18 4.33 5.49	CL 0144 -0743 -1735 -2644 -3606 -4554	CD .0159 .0163 .0181 .0216 .0275 .0398	CPM .0075 .0134 .0181 .0229 .0294 .0325 .0445 .0618	.0004 .0003 .0008 .0010 .0009 .0011 .0019	.0008 .0008 .0008 .0007 .0006 .0007	L/D 905 4.551 9.563 12.233 13.102 11.447	CDB •0046 •0046 •0046 •0046 •0045	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 15.9383
158 159 160 161 162 163 164	MACH • 753 • 753 • 752 • 753 • 754 • 753 • 754 • 756	Q 580.533 581.214 580.248 580.781 581.487 581.139 580.897	BETA 01 01 01 00 00 00	22 .88 2.02 3.18 4.33 5.49 6.67 7.81 8.93	CL 0144 .0743 .1735 .2644 .3606 .4554 .5350 .5981	CD .0159 .0163 .0181 .0216 .0275 .0398 .0598 .0820 .1068	CPM .0075 .0134 .0181 .0229 .0294 .0325 .0445 .0618	.0004 .0003 .0008 .0010 .0009 .0011	.0008 .0008 .0008 .0007 .0006 .0007	L/D 905 4.551 9.563 12.233 13.102 11.447 8.948	CDB •0046 •0046 •0046 •0045 •0045 •0045	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 15.9383 37.0769
158 159 160 161 162 163 164	MACH •753 •753 •753 •754 •753 •753	Q 580.533 581.214 580.248 580.781 581.487 581.139 580.897 582.107 583.388 582.603	BETA01010100000000	22 .88 2.02 3.18 4.33 5.49 6.67 7.81 8.93	CL 0144 .0743 .1735 .2644 .3606 .4554 .5350 .5981 .6308	CD .0159 .0163 .0181 .0216 .0275 .0398 .0598 .0820 .1068 .1297	CPM .0075 .0134 .0181 .0229 .0294 .0325 .0445 .0618 .0829	.0004 .0003 .0008 .0010 .0009 .0011 .0019	.0008 .0008 .0008 .0007 .0006 .0007	L/D 905 4.551 9.563 12.233 13.102 11.447 8.948 7.297	CDB • 0046 • 0046 • 0046 • 0045 • 0045 • 0045 • 0045	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 15.9383 37.0769
158 159 160 161 162 163 164 165	MACH • 753 • 753 • 752 • 753 • 754 • 753 • 754 • 756	Q 580.533 581.214 580.248 580.781 581.487 581.139 580.897 582.107 583.388	BETA010101000000000	22 .88 2.02 3.18 4.33 5.49 6.67 7.81 8.93	CL 0144 .0743 .1735 .2644 .3606 .4554 .5350 .5981	CD .0159 .0163 .0181 .0216 .0275 .0398 .0598 .0820 .1068	CPM .0075 .0134 .0181 .0229 .0294 .0325 .0445 .0618	.0004 .0003 .0008 .0010 .0009 .0011 .0019 .0024	.0008 .0008 .0008 .0007 .0006 .0007 .0008 .0007	L/D 905 4.551 9.563 12.233 13.102 11.447 8.948 7.297 5.904	CDB • 0046 • 0046 • 0046 • 0045 • 0045 • 0045 • 0045 • 0045	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 15.9383 37.0769 58.7692 78.6153
158 159 160 161 162 163 164 165 166	MACH • 753 • 753 • 754 • 753 • 754 • 753 • 754 • 756 • 756 • 755	Q 580.533 581.214 580.248 580.781 581.487 581.139 580.897 582.107 583.388 582.603	BETA010101000000000	22 .88 2.02 3.18 4.33 5.49 6.67 7.81 8.93	CL 0144 .0743 .1735 .2644 .3606 .4554 .5350 .5981 .6308	CD .0159 .0163 .0181 .0216 .0275 .0398 .0598 .0820 .1068 .1297	CPM .0075 .0134 .0181 .0229 .0294 .0325 .0445 .0618 .0829	.0004 .0003 .0008 .0010 .0009 .0011 .0019 .0024 .0008	.0008 .0008 .0008 .0007 .0006 .0007 .0008 .0007	L/D 905 4.551 9.563 12.233 13.102 11.447 8.948 7.297 5.904 5.202	CDB - 0046 - 0046 - 0046 - 0045 - 0045 - 0045 - 0045 - 0044 - 0044	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 37.0769 58.7692 78.6153 86.7691
158 159 160 161 162 163 164 165 166 167 168	MACH • 753 • 753 • 752 • 753 • 754 • 753 • 754 • 755 • 755	Q 580.533 581.214 580.248 580.781 581.487 581.487 580.897 582.107 583.388 582.603	BETA010101000000000	22 .88 2.02 3.18 4.33 5.49 6.67 7.81 8.93 10.05 11.17	CL 0144 0743 	CD .0159 .0163 .0181 .0216 .0275 .0398 .0598 .0820 .1068 .1297 .1536	CPM .0075 .0134 .0181 .0229 .0294 .0325 .0445 .0618 .0829 .0964 .1109	.0004 .0003 .0008 .0010 .0009 .0011 .0019 .0024 .0008	.0008 .0008 .0008 .0007 .0006 .0007 .0008 .0007 .0004	L/D 905 4.551 9.563 12.233 13.102 11.447 8.948 7.297 5.904 5.202 4.641	CDB .0046 .0046 .0046 .0045 .0045 .0045 .0045 .0044 .0044	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 15.9383 37.0769 58.7692 78.6153 86.7691 92.6153
158 159 160 161 162 163 164 165 166 167 168	MACH • 753 • 752 • 753 • 754 • 753 • 754 • 756 • 755 • 755	Q 580.533 581.214 580.248 580.781 581.487 581.139 580.897 582.107 583.388 582.603 582.683	BETA010101000000000	22 .88 2.02 3.18 4.33 5.49 6.67 7.81 8.93 10.05 11.17	CL 0144 - 0743 - 1735 - 2644 - 3606 - 4554 - 5350 - 5981 - 6308 - 6747 - 7128 - 7371	CD .0159 .0163 .0181 .0216 .0275 .0398 .0598 .0820 .1068 .1297 .1536	CPM .0075 .0134 .0181 .0229 .0294 .0325 .0445 .0618 .0829 .0964 .1109	.0004 .0003 .0008 .0010 .0009 .0011 .0019 .0024 .0008 .0006	.0008 .0008 .0008 .0007 .0006 .0007 .0008 .0007 .0004 .0004 .0004	L/D 905 4.551 9.563 12.233 13.102 11.447 8.948 7.297 5.904 5.202 4.641 4.201 3.815	CDB • 0046 • 0046 • 0046 • 0045 • 0045 • 0045 • 0044 • 0044 • 0043 • 0043 • 0042	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 15.9383 37.0769 58.7692 78.6153 86.7691 92.6153 95.6922 91.9999
158 159 160 161 162 163 164 165 166 167 168 169 170	MACH • 753 • 752 • 753 • 754 • 753 • 754 • 755 • 755 • 755 • 755 • 755	Q 580.533 581.214 580.248 580.781 581.487 581.139 580.897 582.107 583.388 582.603 582.603 582.687 583.160	BETA010100000000000	22 .88 2.02 3.18 4.33 5.49 6.67 7.81 8.93 10.05 11.17 12.23 13.41	CL 0144 .0743 .1735 .2644 .3606 .4554 .5350 .5981 .6308 .6747 .7128 .7371	CD .0159 .0163 .0181 .0216 .0275 .0398 .0598 .0820 .1068 .1297 .1536 .1755 .1997	CPM .0075 .0134 .0181 .0229 .0294 .0325 .0445 .0618 .0829 .0964 .1109 .1218	.0004 .0003 .0008 .0010 .0009 .0011 .0019 .0024 .0008 .0006 .0006	.0008 .0008 .0008 .0007 .0006 .0007 .0008 .0007 .0004 .0004 .0004 .0004	L/D905 4-551 9-563 12-233 13-102 11-447 8-948 7-297 5-904 5-202 4-641 4-201 3-815 3-262	CDB .0046 .0046 .0046 .0045 .0045 .0045 .0045 .0043 .0043 .0043 .0043	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 15.9383 37.0769 58.7692 78.6153 95.6922 91.9999 88.7691
158 159 160 161 162 163 164 165 166 167 168 169 170	MACH • 753 • 753 • 752 • 753 • 754 • 755 • 755 • 755 • 755 • 755	Q 580.533 581.214 580.248 580.781 581.487 581.139 580.897 582.107 583.388 582.603 582.603 583.160 583.993 584.529	BETA010101000000000	22 .88 2.02 3.18 4.33 5.49 6.67 7.81 8.93 10.05 11.17 12.23 13.41 15.64	CL 0144 .0743 .1735 .2644 .3606 .4554 .5350 .5981 .6308 .6747 .7128 .7371 .7616	CD .0159 .0163 .0181 .0216 .0275 .0398 .0598 .0820 .1068 .1297 .1536 .1755 .1997 .2486	CPM .0075 .0134 .0181 .0229 .0294 .0325 .0445 .0618 .0829 .0964 .1109 .1218 .1320 .1423 .1465	.0004 .0003 .0008 .0010 .0009 .0011 .0019 .0024 .0008 .0006 .0006	.0008 .0008 .0008 .0007 .0006 .0007 .0008 .0007 .0004 .0004 .0004 .0003 .0005	L/D905 4.551 9.563 12.233 13.102 11.447 8.948 7.297 5.904 5.202 4.641 4.201 3.815 3.262 2.876	CDB .0046 .0046 .0046 .0045 .0045 .0045 .0045 .0044 .0043 .0043 .0043 .0043	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 15.9383 37.0769 58.7692 78.6153 95.6922 91.9999 88.7691 93.9999
158 159 160 161 162 163 164 165 166 167 168 169 170 172	MACH • 753 • 753 • 752 • 753 • 754 • 756 • 755 • 755 • 755 • 755 • 757 • 758	Q 580.533 581.214 580.248 580.781 581.487 581.487 582.107 583.388 582.603 582.687 583.160 583.993 584.529	BETA010101000000000	22 .88 2.02 3.18 4.33 5.49 6.67 7.81 8.93 10.05 11.17 12.23 13.41 15.64	CL 0144 - 0743 - 1735 - 2644 - 3606 - 4554 - 5350 - 5981 - 6308 - 6747 - 7128 - 7371 - 7616 - 8812 - 8641 - 9279	CD .0159 .0163 .0181 .0216 .0275 .0398 .0598 .0820 .1068 .1297 .1536 .1755 .1997 .2486 .3004 .3618	CPM .0075 .0134 .0181 .0229 .0294 .0325 .0445 .0618 .0829 .0964 .1109 .1218 .1320 .1423 .1465 .1429	.0004 .0003 .0008 .0010 .0009 .0011 .0019 .0024 .0008 .0006 .0007 .0007 .0005	.0008 .0008 .0008 .0007 .0006 .0007 .0008 .0007 .0004 .0004 .0004 .0003 .0005 .0007	L/D905 4.551 9.563 12.233 13.102 11.447 8.948 7.297 5.904 5.202 4.641 4.201 3.815 3.262 2.876 2.565	CDB .0046 .0046 .0046 .0045 .0045 .0045 .0045 .0044 .0044 .0043 .0043 .0042 .0041 .0038	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 15.9383 37.0769 58.7692 78.6153 86.7691 92.6153 95.6922 91.9999 88.7691 93.9999
158 159 160 161 162 163 164 165 166 167 168 169 170 172 173 174	MACH • 753 • 752 • 753 • 754 • 753 • 754 • 756 • 755 • 755 • 756 • 757 • 758 • 758 • 758	Q 580.533 581.214 580.248 580.781 581.487 581.139 580.897 582.107 583.388 582.603 582.887 583.160 583.993 584.529 585.547 584.023	BETA010101000000000	22 .88 2.02 3.18 4.33 5.49 6.67 7.81 8.93 10.05 11.17 12.23 13.41 15.64 17.78	CL 0144 -0743 -1735 -2644 -3606 -4554 -5350 -5981 -6308 -6747 -7128 -7371 -7616 -8112 -8641	CD .0159 .0163 .0181 .0216 .0275 .0398 .0598 .0820 .1068 .1297 .1536 .1755 .1997 .2486 .3004	CPM .0075 .0134 .0181 .0229 .0294 .0325 .0445 .0618 .0829 .0964 .1109 .1218 .1320 .1423 .1465	.0004 .0003 .0008 .0010 .0009 .0011 .0019 .0024 .0008 .0006 .0006 .0007 .0005 .0005	.0008 .0008 .0008 .0007 .0006 .0007 .0008 .0007 .0004 .0004 .0004 .0003 .0005	L/D905 4.551 9.563 12.233 13.102 11.447 8.948 7.297 5.904 5.202 4.641 4.201 3.815 3.262 2.876	CDB .0046 .0046 .0046 .0045 .0045 .0045 .0045 .0044 .0043 .0043 .0043 .0043	PB-1 11.9999 10.0307 11.8768 12.2153 11.3538 15.9383 37.0769 58.7692 78.6153 95.6922 91.9999 88.7691 93.9999

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

STABILITY AXIS COEFFICIENTS

STAB.PRESS.COEFF

POINT	MACH	Ú	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
190	.702	529.017	01	23	0181	.0160	.0080	.0002	.0008	-1.135	.0044	9.0612
191	.701	528.470	01	• 80	•0086	.0163	.0124	.0001	.0008	4.202	•0044	9.6307
192		528.004	00	1.98	• 1582	.0177	.0191	.0009	.0006	8.917	•0044	10.0615
193	.702		00	3.13	· 2511	.0211	.0247	.0008	.0007	11.913	•0044	10.2153
194	• 701		00	4.21	• 3379	.0258	.0312	.0004	.0006	13.075	.0044	7.9999
195		528.959	00	5.36	<ul><li>4286</li></ul>	.0361	.0366	.0007	.0005	11.882	.0044	10.2461
196	.701		00	6.54	•5137	.0569	•0452	-0007	•0003	9.031	.0043	32.8461
197	• 703		00	7.68	• 5695	.0795	.0626	.0002	-0004	7.165	.0043	55.5384
198	.701		00	8.77	-6152	.1008	-0816	.0006	.0003	6.104	•0042	69.2307
199		529.596	00	9.87	•6578	.1231	.0981	•0005	.0003	5.345	•0042	78.1538
200		524.162	00	11.00	•6938	.1458	.1137	<b>.</b> 0004	.0004	4.759	•0042	80.1538
201		531.601	00	12.07	• 7253	• 1685	.1248	.0003	•0005	4.304	.0041	91.8461
202		531.293	00	13.25	• 7524	.1928	.1341	.0001	.0005	3.903	-0040	93.6922
203	•702		00	15.47	• 8034	.2416	.1476	•0003	•0005	3.325	.0039	87.6922
204	.703		00	17.59	8507	-2912	.1534	.0003	.0007	2.921	.0037	86.3076
205	• 704		00	19.69	•9011	.3466	.1491	.0000	.0008	2.600	.0030	98.3076
206		532.378	00	21.76	• 9520	<ul><li>4042</li></ul>	.1512	•0002	.0008	2.355	•0023	105.4614
207		520.632	01	25	0137	-0158	.0083	.0003	.0008	<b>864</b>	.0043	11.4918
208	.701	528.632	00	-83	• 0670	.0162	-0130	.0010	.0007	4.139	.0044	9.9692
	TEST= 7	78 KUN=	61			BONY AY	S COEFFICIEN	TS		BOO. <b>∀</b>	PRESS.COE	££
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
190		529.017	01		0182	.0159	•0002	.0008	.0010			0.0000
191	.701		01		.0689	.0153	•0001	•0008	.0004			0.0000
192	.701		00		.1587	.0123	•0009	.0006	.0004			0.0000
193	.732		00		.2519	.0073	.0008	.0008	0002			0.0000
194		528.351	00		.3389	.0009	.0003	.0006	0005			0.0000
195		528.959	00		.4301	0042	-0007	.0005	0001	• (	0044	0.0000
196	-701	528.825	00	6.54	.5168	0020	•0006	.0004	•0005	• (	0044	0.0000
197	•703	530.046	00	7.68	.5750	.0027	.0002	.0004	.0001			0.0000
198	.701	528.759	00	8.77	.6234	.0057	•0006	•0004	.0003	.(	0043	0.0000
199	• 732	529.596	00	9.87	•6692	.0085	•0005	.0003	0004			0.0000
200	.731	528.162	00		7089	.0107	•0003	•0005	•0005			0.0000
201	. 704		00		•7445	.0131	.0001	•0005	•0000			0.0000
202	.704	531.∠93	00		.7765	.0152	0000	•0005	0002			0.0000
203	•702		00		.8387	.0186	•0002	•0006	0012			0.0000
204	•703		00		.8990	.0204	•0000	-0007	0016			0.0000
205	-704	530.933	00		.9652	.0228	0003	.0008	0015			0.0000
206		532.378	00		1.0340	.0225	0001	•0008	0022			0.0000
207		528-632	01		~.0137	-0158	•0004	.0008	•0008			0.0000
208	-731	528.632	00	-83	•0672	•015≥	.0010	.0007	0003	• (	0044	0.0000

1531= 118 KUN= 61

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

						BODY AXI	S CUEFFICIENT	S		BODY PRESS.	COEFF
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
222	-292	120.181	00	07	0195	.0158	.0005	•0004	0007	• 0038	0.0000
223	.242	120.086	00	•89	.0569	.0163	•0005	.0007	0012	•0038	0.0000
224	•292	120.086	00	1.87	.1242	.0141	.0009	•0009	0021	.0038	0.0000
225	.292	120.087	00	2.87	-1813	.0110	.0004	.0006	0022	.0038	0.0000
226	.292	120.090	•00	3.89	.2678	.0064	.0008	•0004	0033	•0038	0.0000
227	.293	120.767	•00	4.90	•3331	0003	.0007	•0002	0037	• 0038	0.0000
228	-242	120.095	•00	5.94	-4018	0081	.0007	•0004	0042	.0037	0.0000
229	.242	120.109	•00	6.98	•4766	0110	.0002	•0002	0043	.0037	0.0000
230	.292	120.134	•00	8.06	-5512	0087	.0001	•0005	0049	•0037	0.000
231	.293	120.744	.00	9.14	•6319	0059	.0001	.0003	0059	• 0037	0.0000
232	.292	120.092	.00	10.27	.6617	0054	.0001	-0004	0065	-0036	0.000
233	.291	119.444	•00	11.30	.7113	0044	•0000	.0001	0073	•0036	0.000
234	.291	119.475	•00	12.44	•7474	0024	-0000	•0002	0078	•0035	0.000
235	-292	120.220	•00	14.60	.8241	.0019	0003	.0007	0088	-0033	0.000
236	.291	119.515	•00	16.69	.8829	.0062	0003	.0006	0096	•0032	0.000
237	- 29 2	120.170	.00	18.73	•9516	.0092	0001	•0005	0107	•0031	0.000
238	. 243	120.936	.00	20.80	1.0311	.0126	0002	.0008	0111	• 0025	0.000
239	.291	119.219	-00	06	0095	.0182	.0003	.0004	0065	.0038	0.000

	TEST= 7	78 RUN=	62									
					STA	BILLTY AXIS	COEFFICIENTS			STAB	PRESS-COEFF	:
POINT	MACH	C	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
222	-242	120.181	00	07	0195	.0158	.0110	.0005	•0004	-1.230	-0038	1.2461
223	.292	120.080	00	.89	•0567	.0172	.0158	.0005	.0006	3.292	•0038	2.3999
224	.292	120.080	00	1.87	•1237	.0181	.0199	.0009	.0008	6.825	.0038	1.8615
225	•292	120.087	00	2.87	• 1805	.0200	•0265	.0004	•0006	9.006	.0038	2.2614
226	. 292	120.090	•00	3.89	• 2667	.0246	.0350	.0008	.0004	10.851	•0038	1.7384
227	.243	120.767	•00	4.90	.3319	• 0282	•0389	.0008	.0001	11.778	.0038	1.2153
228	.292	120.095	•00	5.94	• 4005	.0335	•0432	.0007	-0003	11.960	.0037	1.0307
229	-292	120.109	•00	6.98	• 4744	.0470	.0478	.0002	•0002	10.087	.0037	6.1228
230	.272	120.134	•00	8.06	• 5469	.0687	•0555	.0002	-0004	7.964	.0037	18.2152
231	. 293	120.744	• 00	9.14	-6248	• 0945	.0760	.0001	•0003	6.608	.0036	27.4615
232	-242	120.092	•00	10.27	•6520	•1127	.0903	.0001	.0004	5.786	•0035	30.3077
233	. 291	119.444	• 00	11.30	•6984	•1351	•1092	.0000	.0001	5.171	•0035	32.6154
234	-241	114.475	•00	12.44	• 7304	. 1586	•1206	.0001	•0002	4.605	.0034	37.0769
235	-242	120.220	•00	14.60	•7970	.2096	.1463	0001	.0007	3.802	.0032	40.6153
230	- 241	119.515	-00	16.69	.8439	. 2595	.1656	0001	•0006	3.251	.0031	36.6153
237	- 29 2		•00	18.73	• 8983	.3142	.1813	.0001	.0005	2.859	•0029	31.7692
238	. 293	120.930	.00	20.80	• 9595	.3778	.1817	.0001	.0008	2.539	.0024	32.1538
239	.241	119.219	•00	06	0095	.0183	.0086	.0003	• 0004	520	•0038	2.4768

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	64									
							IS COEFFICIE	NTS		800	Y PRESS.CO	FF
POINT	MACH	۵	BETA		CNF	CAF	CLB	CNB	CSF		CAB	CAC
253	•497	311.732	00		0158	•0155	.0000	•0009	.0021		.0039	0.0000
254	•497	311.733	00	1.10	.0623	.0147	.0008	.0003	.0008		•0039	0.0000
255	• 497	311.206	01	2.16	-1396	.0126	.0006	•0009	.0027		.0039	0.0000
256	•497	312.010	00	3.24	-2199	.0083	.0000	.0008	•0025		•0039	0.0000
257	•497	311.924	00	4.29	•2864	.0023	•0000	•0007	•0020		.0039	0.0000
258	•497	311.932	00	5.37	.3673	0054	0001	•0004	.0038		.0039	0.0000
259	.497	311.962	00	6.51	•4404	0106	0004	•0005	.0035		.0038	0.0000
260	•497	311.510	00	7.58	•5334	0083	.0008	.0006	.0017		•0038	0.0000
261	•497	312.218	00	8.71	•5902	0048	.0014	.0008	•0026		.0038	0.0000
262	.497	311.685	00	9.75	-6485	0021	.0007	.0007	.0023		.0038	0.0000
263	•497	311.593	00	10.92	-6877	0008	.0004	.0005	.0018		.0037	0.0000
264	.447	311.685	00	11.95	.7306	.0014	.0004	.0006	.0012		.0037	0.0000
265	.498	312.940	00	13.10	.7633	.0040	.0004	.0006	•0006		•0036	0.0000
266	• 498	312.982	00	15.29	.8452	.0083	.0001	•0008	•0020		.0035	0.0000
267	.499	313.824	00	17.44	.9031	.0118	0002	•0011	.0015		.0034	0.0000
268	•497	312.094	00		•9633	.0144	•0002	•0006	.0007		.0031	0.0000
269	.499	314.209	00	21.51	1.0219	.0173	0009	•0012	.0016		.0024	0.0000
270	•497	311.642	01	.08	0122	.0153	.0001	.0009	.0043		.0039	0.0000
	TEST= 7	78 RUN=	64									
							COEFFICIENTS			STA	B.PRESS.COE	FF
POINT	MACH	<i>•</i>	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
253	•497	311.732	00	.05	0158	.0155	.0073	.0000	.0009	-1.019	•0039	5.8921
254	•497	311.733	00	1.10	.0620	.0159	.0136	.0008	.0007	3.896	•0039	4.7998
255	•497	311.206	01	2.16	•1390	•0178	.0187	•0006	.0009	7.806	.0039	5.0767
256	•497	312.010	00	3.24	-2191	.0208	.0264	.0001	.0008	10.555	.0039	5.3229
257	-497	311.924	00	4.29	- 2854	.0237	.0308	.0001	.0007	12.045	.0039	4.5383
258	• 497	311.932	00	5.37	• 3062	.0291	.0373	0000	.0004	12.599	.0039	3.9075
259	• 447	311.962	00	6.51	• 4388	• 0394	.0433	0003	.0006	11.142	.0038	6.4767
260	-497	311.510	00	7.58	•5299	.0621	•0506	.0008	-0005	8.529	•0038	26.6154
261	• 497	312.218	00	8.71	.5841	.0846	•0652	•0015	•0006	6.902	•0037	47.3846
262	. 447	311.685	00	9.75	.6395	.1077	.0860	.0008	.0006	5.935	.0037	59.9999
263	•497	311.593	00	10.92	•6754	•1296	.1055	.0005	.0004	5.213	•0036	58.9230
264	.447	311.685	00	11.95	.7145	.1526	.1191	•0005	.0005	4.683	•0036	64.4615
265	-498	J12.940	00	13.10	.7426	.1769	-1305	.0005	.0005	4.197	.0035	76.3076
266	-498	312.982	00	15.29	.8131	-2309	.1526	•0003	.0007	3.522	.0034	80.6153
267	. 499	313.824	00	17.44	.8580	.2820	.1667	•0002	.0011	3.043	.0033	71.8461
268	.497	312.094	00	19.49	.9033	.3350	.1722	•0004	.0005	2.696	•0029	72.3076
269	•499	314.209	00	21.51	.9443	• 3909	.1654	0004	.0014	2.416	.0023	84.7691
270	•497	311.642	01	•08	0122	.0153	.0063	.0001	•0009	796	.0039	5.0921

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN= 6	55									
							S COEFFICIEN	ITS .			PRESS-COE	F
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	(	CAB	CAC
324	• 8d4	701.784	01	-20	.2688	•0242	.0016	•0006	.0008	• 0	0055 (	0.000
325	.883	700.826	01	1.37	.3678	.0232	.0016	•0004	.0012	• (	0055 (	0.000
326	.883	700.575	01	2.53	•4567	.0214	.0018	-0003	.0013	• (	054 (	0.000
327	.883	700.784	00	3.71	•5433	-0188	•0015	•0003	.0010	. (	0055	0.0000
328	-883	700.549	00	4.86	•6362	.0151	0000	•0002	.0017	. (	0054	0.0000
329	-884	701.947	00	6.03	-7272	.0115	-0022	.0001	.0016	• (	0053	0.000
330	•884	701.847	00	7.23	.8101	.0068	.0013	•0002	.0017	. (	0053	0.0000
331	.843	700.534	00	8.42	•8782	.0038	.0008	.0001	.0013	• (	0052	0.000
332	- 883	700.910	00	9.56	•9360	.0020	.0005	.0001	.0018	• (	0052	0.0000
333	.887	703.957	00	10.68	•9595	.0040	0002	.0001	.0024	• (	0052	0.0000
334	-886	703.228	01	11.81	.9716	•0050	0009	.0004	.0010	• (	0052	0.0000
335	.883	700.463	01	- 26	•2674	.0231	.0014	.0006	.0009	. (	0055	0.0000
	TEST= 7	78 RUN=	65									
							COEFFICIENTS				<pre>.PRESS.COE</pre>	
POINT	MACH	Q	BETA	ALPHA	CL	CΩ	CPM	CLS	CNS	L/D	CDB	PB-1
324	-884	.701.784	01	• 20	. 2687	.0251	1235	.0016	.0006	10.704	•0055	16.3999
325	-883	700.826	01	1.37	.3672	.0320	1193	•0016	•0004	11.466	-0055	29.1538
326	.883	700.575	01	2.53	• 4553	-0415	1078	.0018	•0003	10.976	•0054	31.4615
327	- 883	700.784	00	3.71	.5410	.0538	1000	•0015	•0002	10.047	•0055	38.1538
328	- 883	700.549	00	4 • 86	.6326	.0689	0963	0000	•0002	9.176	•0054	37.0000
329	-834	701.947	00	6.03	.7219	.0878	0995	•0022	0001	8.219	•0053	43.6153
330	-884	701.847	00	7.23	.8028	.1087	0915	.0013	.0001	7.386	.0053	73.8461
331	.883	700.534	00	8.42	.8682	.1324	0724	.0008	0000	6.559	•0052	114.9230
332	. 883	700.910	00	9•56	•9227	· 1574	0535	.0005	.0001	5.864	•0052	238.1536
333	.887	703.957	00	10.68	• 9422	.1819	0190	0002	.0001	5.181	.0051	158.7691
334	• 886	703.228	01	11.81	•9500	-2038	.0163	0008	•0006	4.662	.0051	248.7690
335	-843	700.463	01	• 26	. 2673	• 0243	1210	•0014	•0006	11.009	•0055	15.3230

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	66			D20V 4V	is coefficien	TC		0004	20565 605	
							IS COEFFICIEN				PRESS.COE	
POINT	МАСН	<b>4</b>	BETA		CNF	CAF	CLB	CNB	CSF		CAB	CAC
386	-823	647.599	01	<b>-2</b> 5	.2432	.0199	.0009	.0007	.0010			0.0000
87د	•822	647.185	01	1.42	.3559	.0163	.0013	.0008	.0011			0.0000
388	.822	640.709	01	2.59	.4070	.0102	•0015	.0007	.0016			0.0000
389	-822	646.770	01	3.81	•5924	.0028	.0019	.0006	•0020			0.0000
390	-824	648.901	01	4.97	.6921	0024	•0022	•0004	-0022			0.0000
391	-824	648.480	01	6.14	.7763	0083	.0037	.0004	•0025	• 1		0.0000
392	-821	040.198	01	7.31	.8475	0135	.0021	.0002	.0030		0048 (	0.0000
393	•823	647.916	01	8.45	•9042	0134	.0010	.0001	.0031	• 1	0048 (	0.0000
394	-824	648.814	01	9.59	•9431	0098	.0021	•0004	.0021	• 1	0048 (	0.0000
395	.824	648.696	01	10.69	.9835	0078	.0029	.0008	.0028	• (	0048 (	0.0000
390	.825	649.742	01	11.82	1.0052	0055	.0042	.0004	.0030	• (	0047 (	0.000
397	.826	450.551	01	12.85	.9854	0021	.0078	.0002	.0045	•1	0047 (	0.000
398	.823	647.291	01	-27	.2417	.0195	.0013	.0008	.0017		0049 (	0.0000
	TEST= 7	78 RUN=	66									
							CUEFFICIENTS				.PRESS.COE	F <b>F</b>
PUINT	MACH	Ú	BETA	ALPHA	CF	CO	CPM	CLS	CNS	L/D	CDB	PB-1
386	-823	641.599	01	• 25	. 2431	.0210	1053	•0009	.0007	11.592	.0049	13-2307
387	.822	047.185	01	1.42	. 3554	.0251	1045	.0014	.0007	14.156	.0049	15.6614
388	.822	646.709	01	2.59	.4660	.0314	1051	-0015	.0006	14.862	•0049	18.6152
389	•822	640.770	01	3.81	•5909	•0422	1098	.0019	.0005	13.999	•0049	17.8768
390	.824	048.901	01	4.97	.6897	.0576	1059	.0022	.0002	11.972	•0049	34.0000
391	.824	648.986	01	6.14	.7727	.0747	0960	.0037	0000	10.339	-0048	46.7692
392	.821	046.198	01	7-31	<ul><li>8424</li></ul>	•0945	0780	.0021	0000	8.916	• 0048	66.4615
393	-843	647.916	01	8.45	.8964	.1196	0540	.0010	0001	7.498	.0048	212.7690
394	.824	646.814	01	9.59	.9315	<ul><li>1475</li></ul>	0195	.0021	.0001	6.314	-0047	185.0767
395	.824	648.696	01	10.69	•9679	.1748	.0022	.0030	.0002	5.537	.0047	360.9227
396	-825	649.742	01	11.82	.9850	-2005	.0258	•0042	0005	4.912	.0046	401.0765
397	.820	050.55t	01	12.85	.9612	.2172	.0560	.0076	0015	4.426	.0046	171-2306
348	-823	047.291	01	-27	.2416	.0207	1055	.0013	.0008	11-677	.0049	13.1384

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 KUN=	67									
							S COEFFICIEN			BODY	PRESS.COEF	F
POINT	MACH	a)	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	(	AB	CAC
412	• 704	596.665	01	. 17	-2231	.0194	.0014	.0007	.0004	• (	0047 (	.0000
413	•70d	595 <b>.</b> 788	01	1.29	•328I	.0160	.0018	.0007	.0007	• (	0047 (	.0000
414	•770	597.259	01	2.45	•4335	.0097	-0017	.0006	.0014	• (	0047	.0000
415	•770	591.258	01	3.60	•5396	.0004	.0013	.0005	.0013	•(	0047 (	.0000
416	-759	596.397	01	4.77	•6432	0112	.0016	.0005	.0018	• (	0047 (	.0000
417	-768	595.007	00	5.96	• 7547	0236	•0020	.0003	.0021	• (	0046 (	.0000
418	. 709	596.860	00	7.14	<b>-8487</b>	0304	.0006	.0002	.0013	• (	0046 (	.0000
419	.771	598.281	00	8.28	.8892	0287	0001	0001	.0018	• (	046 (	0.0000
420	• 169	597.059	01	9.39	• 9387	0269	.0009	.0005	.0012	• (	0046 (	.0000
421	• 771	598.497	00	10.51	• 9935	0226	.0007	.0005	.0006	•(	0046 (	0.000
423	-713	600.733	01	11.60	• 4954	0158	.0132	•0004	.0019	• (	0046 (	.0000
424	-770	596.944	01	• 15	-2249	.0194	.0013	.0007	.0005	• (	0047 (	0.000
	1EST= 7	78 KUN=	67		STAB	ILITY AXIS (	COEFFICIENTS			STAR	.PRESS.CDEI	- F
POINT	MACH	ن	BETA	ALPHA	CŁ	CD	CPM	CLS	CNS	L/D	CDB	PB-1
412	.769	596.665	01	.17	.2231	.0201	0987	•0014	• 0007	11.090	.0047	11.6922
413	• 768	595.788	01	1.29	.3277	.0235	0957	.0018	.0007	13.973	•0047	11.8768
414	.770	597.259	01	2.45	.4327	.0282	0934	•0018	•0006	15.344	.0047	13.7845
415	.710	597.258	01	3.60	•5385	.0342	0928	-0013	• 0005	15.734	•0047	14.3384
416	.709	596.397	01	4.77	.6419	.0423	0920	•0016	.0004	15-169	.0047	17.3229
417	.758	595.809	00	5.96	.7531	.0550	0897	•0020	•0001	13.703	.0046	20.5842
418	• 769	596.860	00	7.14	.8459	.0753	0768	.0006	-0002	11.229	.0046	61.6922
419	.771	298.481	00	8.28	.8841	• 0997	0387	0001	0001	8.864	•0046	142.6152
420	.769	597.059	01	9.39	.9305	.1267	0134	•0010	•0003	7.346	•0045	381.2304
421	.771	598.497	00	10.51	.9810	.1590	.0034	•0008	•0003	6.171	-0045	485.3841
423	.713	000.733	01	11.60	.9783	.1847	.0286	.0130	0023	5.297	.0045	209.8459
424	.770	546.944	01	-15	. 2249	.0200	0991	.0013	-0007	11.267	.0047	10.5845

	TEST= 7	78 RUN= 6	8								
						BODY AXI	S COEFFICIEN	15		BODY PRESS.	
POINT	MACH	٥	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
438	.717	544.323	01	.10	.2209	.0194	.0020	.0008	.0012	• 0044	0.0000
439	.716	543.402	01	1.23	.3206	.0160	•0015	.0007	-0010	.0045	0.0000
440	.717	544.482	01	2.32	•4154	.0100	.0017	.0007	.0016	• 0045	0.0000
441	.718	545.021	01	3.49	.5184	•0009	.0012	.0006	.0015	•0045	0.0000
442	.717	543.946	01	4.60	.6088	0100	.0017	-0007	.0019	.0045	0.0000
443	.717	544.120	01	5.75	.7020	0233	.0017	•0006	.0013	• 0045	0.0000
444	.717	543.716	01	6.94	.7980	0365	.0019	•0007	.0018	.0045	0.0000
445	.717	544.365	00	8.08	.8693	0396	0003	0003	.0028	.0044	0.0000
446	.718	545.222	00	9.19	.8927	0314	0016	0002	.0027	.0045	0.0000
447	.718	545.118	01	10.27	•9296	0281	.0045	-0005	.0017	.0044	0.0000
448	.717	544.359	00	11.39	.9561	0213	.0055	.0003	.0013	.0044	0.0000
449	.720	546.787	00	12.47	.9703	0128	.0061	.0000	.0026	.0043	0.0000
450	.718	545.442	00	13.58	.9679	0073	.0017	.0001	.0033	.0043	0.0000
451	.721	548-151	01	15.81	1.0070	0004	.0008	.0002	.0032	• 0042	0.0000
452	.720	547.380	01	17.92	1.0515	.0008	.0013	.0003	.0035	.0039	0.0000
453	.720	547.465	00	19.99	1.1026	.0038	.0011	.0003	.0020	.0033	0.0000
454	•722	548-626	00	22.09	1.1657	.0050	.0007	•0002	.0020	•0027	0.0000
455	.719	546.482	00	8.17	.8703	0380	•0002	0000	-0036	.0045	0.0000

	TEST= 7	78 RUN=	68									
					STAE	BILITY AXIS	COEFFICIENTS			STAB	.PRESS.COEF	F
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	ÇDB	PB-1
438	.717	544.323	01	. 10	. 2209	.0198	0941	.0020	.0008	11.166	.0044	8.9227
439	.710	543.402	01	1.23	.3202	.0229	0902	.0015	.0007	14.005	•0045	9.9381
440	.717	544-482	01	2.32	• 4147	.0269	0879	.0017	.0007	15.440	.0045	10.9230
441	.718	545.021	01	3.49	.5174	.0324	0848	.0012	.0005	15.945	.0045	11.1384
442	.717	543.946	01	4.60	.6077	.0389	0820	.0018	.0005	15.640	•0045	11.6922
443	.717	544.120	01	5.75	. 7008	.0471	0762	.0018	.0004	14.863	.0045	13.8768
444	.717	543.716	01	6.94	. 7465	.0602	0703	.0020	.0004	13.237	•0045	15.4460
445	.717	544.365	00	8.08	.8663	.0829	0469	0003	0003	10.447	.0044	74.9230
446	.718	545.222	00	9.19	.8863	.1115	0046	0016	.0001	7.948	•0044	168.6152
447	.718	545.118	01	10.27	.9197	.1381	•0206	.0045	0003	6.657	.0043	161.2306
448	.71/	544.359	00	11.39	.9415	. 1661	.0455	•0055	0008	5.602	•0043	169.2306
449	.720	546.787	00	12.47	•9502	.1971	.0677	.0060	0013	4.822	•0042	162.4614
450	-718	545.442	00	13.58	• 9420	.2202	.0938	.0016	0003	4.281	.0042	124-6153
451	.721	548-151	01	15.81	.9691	.2739	.1153	.0009	.0000	3.538	.0040	110.4614
452	.720	547.380	01	17.92	1.0003	.3243	.1329	.0013	0001	3.085	.0037	102.7691
453	•720	547.465	00	19.99	1.0348	.3805	-1345	.0011	0001	2.719	•0031	112.6153
454	.722	548.620	00	22.09	1.0783	.4430	.1367	.0007	0001	2.434	.0025	122.7691
455	.719	546.482	00	8.17	.8669	.0860	0470	.0002	0000	10.079	•0045	77.6922

	TEST = 7	78 RUN= 6	59									
						RXY ACOR	S COEFFICIEN	TS		BODY	PRESS.COE	÷F
POINT	MACH	ú	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	(	AB	CAC
469	.663	488.289	00	.18	-2074	.0191	.0013	.0006	•0004	• 0	042	0.000
470	.664	489.418	01	1.26	.3010	.0159	.0013	.0007	.0013			0.000
471	.667	491.755	00	2.34	.3936	.0101	•0016	.0007	.0006			0.0000
472	•605	489.979	01	3.45	•4914	.0015	.0015	.0007	.0015			0.0000
473	•665	489.500	01	4.55	•5790	0093	.0015	.0008	.0011			0.0000
474	•665	490.076	00	5.68	•6610	0215	.0019	.0007	.0000			0.0000
475	•665	489.539	01	6.81	.7462	0348	.0019	.0009	.0009			0.0000
476	•665	489.661	00	7.96	.8259	0410	.0020	•0005	.0016			0.0000
477	.666	491-190	00	9.07	.8742	0356	0009	0001	.0014			0.0000
478	•665	490.117	00	10.16	.8951	0305	.0014	.0004	0001			0.0000
479	.657	492.265	00	11.29	.9230	0212	.0018	.0002	.0015			0.0000
480	.667	491.928	00	12.33	•9397	0161	•0029	.0002	.0012			0.0000
481	•667	492.180	00	13.47	9604	0113	.0018	.0003	.0014			0.0000
482	•666	491.521	00	15.66	1.0016	0052	.0013	•0002	-0025			0.0000
483	•668	492.795	00	17.79	1.0418	0011	.0011	•0003	-0021			0.0000
484	•668	492.648	00	19-85	1.0897	•0030	•0009	.0001	-0035			0.0000
485	•667	492.395	00	21.87	1.1310	•0047	•0009	0001	•0034			0.0000
486	•667	491.757	01	8.00	.8246	0409	.0020	.0007	.0015			0.0000
400	•001	7710171	•01	0.00	*0240	.0407	.0020	•0001	•0017	• '	3042	0.0000
	TEST= 7	78 RUN=	69		674.0							
· · <del>-</del>							COEFFICIENTS				PRESS.COE	
POINT	MACH	ų,	BETA	ALPHA	CL 227	CD	CPM	CLS	CNS	L/D	CDB	PB-1
469	.663	488.289	00	-18	.2073	.0197	0906	.0013	•0006	10.506	•0042	8.6150
470	•664	489.418	01	1.26	.3006	•0225	0868	.0013	.0007	13.332	•0043	7-9228
471	•667	491.755	00	2.34	.3929	•0261	0836	.0016	.0006	15.041	•0043	9.6150
472	•665	489.979	01	3.45	• 4905	.0311	0810	.0015	•0006	15.772	.0043	9.5535
473	• 665	489.500	01	4.55	•5779	.0367	0766	.0015	•0006	15.748	.0043	9.0612
474	•665	490.076	00	5.68	•6599	•0440	0683	.0020	.0005	15.003	.0043	10.7842
475	•665	489.539	01	6.81	• 7451	•0539	0607	•0020	•0006	13.832	.0043	10.9996
476	-605	489.661	00	7.96	•8236	.0738	0467	•0020	.0002	11.161	•0042	42.0000
477	•666	491.190	00	9.07	.8689	.1027	0089	0009	.0000	8.460	.0042	112.6153
478	•665	490.117	00	10.16	-8864	•1278	.0211	.0014	.0002	6.934	.0041	136.8460
479	.657	492.265	00	11.29	• 90 9 3	.1599	•0505	.0018	0002	5.686	.0041	146.7691
480	-667	491.928	00	12.33	•9214	<ul><li>1850</li></ul>	.0767	.0029	0004	4.981	.0041	122.7691
481	•667	492.180	00	13.47	• 9366	•2127	.0991	.0018	0001	4.403	.0040	111.4614
482	-666	491.521	00	15.66	• 9658	• 2654	•1252	.0013	0002	3.639	.0038	105.2307
483	-668	492.795	00	17.79	•9923	.3173	•1395	.0011	0000	3.128	.0037	97.3845
484	•668	492.648	00	19.85	1.0239	•3729	.1403	.0009	0002	2.746	.0030	108.4614
485	• 667	492.395	00	21.87	1.0479	<ul><li>4256</li></ul>	.1387	.0007	0004	2.462	.0024	119.9999
486	•667	491.757	01	8.00	•8223	.0742	0463	.0021	.0004	11.078	-0042	41.5384

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 77	la RUN≃ '	70									
						BODY AX	IS COEFFICIEN				PRESS.COE	
POINT	MACH	Ú	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
500	.225	72.847	00	•05	-1937	•0204	.0016	.0012	0003		0036	0.0000
501	. 225	72.749	00	• 94	.2733	.0190	.0020	.0014	0010		0036	0.0000
502	.224	72.555	00	1.91	.3379	.0166	.0016	.0009	0008		0034	0.0000
503	.224	72.555	00	2.89	•4167	.0106	.0015	.0012	0015		0037	0.0000
504	.224	72.555	.00	3.90	•4965	.0021	.0015	.0012	0121		0037	0.0000
505	.225	73.243	.00	4.87	.5710	0070	.0014	.0007	0122	•	0036	0.0000
506	.225	73.245	.00	5.93	.6337	0174	.0013	.0009	0126		0036	0.0000
507	.224	72.560	•00	6.93	.7032	0284	.0021	.0011	0139	•	0037	0.0000
508	.224	72.460	.00	7.99	.7679	0403	•0020	.0006	0144		0037	0.0000
509	.224	72.360	•00	8.99	.8314	0444	.0001	0006	0134		0034	0.0000
510	.224	72.400	.00	10.04	.8940	0420	0006	0010	0135		0035	0.0000
511	•224	72.424	•00	11.09	.9243	0354	0006	0009	0145		0035	0.0000
512	.224	12.449	.00	12.16	.9545	0285	0006	0008	0155		0032	0.0000
	• 225	73.189	.00	14.34	1.0164	0171	.0001	•0001	0177		0030	0.0000
513		72.546	•00	16.36	1.0066	0105	.0001	•0002	0189		0028	0.0000
514	. 224		•00	18.38	1.1237	0065	.0001	•0006	0100		0024	0.0000
515	•224	72.495			1.1453	0024	.0000	•0006	0104		0022	0.0000
516	.224	72.440	•00	20.38	.7597	0383	•0002	•0006	0130		0035	0.0000
517	-223	71.582	•00	7.89		•0266	.0017	.0010	0100		0036	0.0000
518	.225	72.950	.00	22	•1786	•0200	.0017	•0010	0100	•	0030	0.0000
	1ESI= 71	78 RUN=	70									
							CUEFFICIENTS				.PRESS.COE	
POINT	MACH	J.	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
500	.225	12.847	00	• 05	<ul><li>1936</li></ul>	.0206	0757	.0016	.0012	9.398	• 0036	1.2461
501	•225	72.749	00	.94	.2729	.0235	0734	.0020	.0014	11.594	.0036	1.5846
502	.224	74.555	00	1.91	.3371	•027₺	0787	.0016	.0009	12.108	.0034	1.2000
j03	.224	72.555	00	2.89	.4157	.0316	0650	.0016	.0011	13.141	.0036	.8769
504	.224	74.555	•00	3.90	•4952	.0358	0513	.0015	.0011	13.830	.0036	1.0153
505	.225	73.243	.00	4.87	• 5695	.0415	0541	.0014	.0006	13.730	.0036	.8461
506	.225	73.245	•00	5.93	.6321	.0481	0480	.0014	.0008	13.136	•0036	1.0000
507	.224	72.560	•00	6.93	. 7015	.0567	0358	•0022	•0009	12.377	.0036	•9846
508	.224	72.466	•00	7.99	. 7660	.0668	0287	.0021	.0003	11.466	.0036	1.7384
509	.224	72.380	.00	8.99	.8281	.0860	0161	.0001	0006	9.633	.0034	11.6922
510	.224	72.400	.00	10.04	.8876	.1145	.0023	0008	0009	7.749	.0034	26.3077
511	.224	72.424	.00	11.09	.9138	.1431	.0343	0008	0008	6.387	•0034	33.3846
512	.224	72.449	•00	12.16	.9391	.1732	.0662	0008	0007	5.422	•0032	38.3846
513	.225	73.189	•00	14.34	9889	.2351	.1169	.0001	.0001	4.206	.0029	39.0769
514	.224	72.546	-00	16.36	1.0264	- 2903	.1491	.0001	.0002	3.535	.0027	37.7692
515	•224	72.495	•00	18.38	1.0084	.3481	.1764	•0002	.0005	3.069	•0023	31.6923
516	•224	72.440	.00	20.38	1.0745	• 3966	.1884	.0003	.0006	2.709	.0020	26.5384
517	.223	71.582	.00	7.89	.7577	.0664	0253	.0003	•0006	11.415	.0034	1.6615
518	.225	72.950	•00	22	.1787	.0259	0770	.0016	.0010	6.906	•0036	.7538

	TEST= 7	78 KUN= 7	'1			BUDY AXI	S CUEFFICIEN	TS		BODY PRESS.	COEFF
POINT	MACH	ú	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
532	• 424	207.293	00	-11	.1935	.0196	-0015	.0009	.0027	.0039	0.0000
533	•455	261.418	00	1.21	.2709	.0168	.0013	.0008	.0025	.0039	0.0000
534	-455	208.019	00	2.20	.3517	.0116	•0009	.0009	.0022	.0040	0.0000
5 35	.455	207.509	00	3.27	•4299	.0046	•0009	.0007	.0018	.0040	0.0000
5 36	. 455	267.570	00	4.31	.5072	0047	.0006	.0008	.0016	•0040	0.0000
537	• 455	267.664	00	5.36	.5933	0156	.0011	.0007	.0032	.0040	0.0000
538	• 455	267.5/8	00	6.49	•6623	−.0288	.0013	.0009	•0026	.0039	0.0000
539	• 422	201.501	00	7.52	.7261	0417	•0004	.0007	.0028	•0039	0.0000
540	• 495	267.541	00	8.65	•7955	0486	•0004	0006	.0049	.0039	0.0000
541	• 495	268.265	00	9.71	.8516	0447	0008	0003	.0049	.0039	0.0000
542	•425	260.378	00	10.82	.8891	0357	.0004	•0003	.0028	.0038	0.0000
543	• 475	267.840	00	11.89	.9159	0289	.0014	.0004	.0036	.0038	0.0000
544	•450	260.595	00	13.02	.9546	0238	•0014	.0005	.0026	.0037	0.0000
545	• 45 o	268.632	00	15.21	1.0112	0153	.0008	.0002	.0045	.0036	0.0000
546	-450	268.828	01	17.34	1.0506	0102	.0008	.0004	•0063	•0035	0.0000
547	.456	268.846	01	19.35	1.0991	0061	.0008	.0006	.0056	.0032	0.0000
548	•470	269.607	00	21.42	1.1444	0020	.0008	.0003	•0054	.0026	0.0000
549	.424	267.020	00	.16	.1894	.0193	-0014	-0009	•0028	.0039	0.0000

	1ES1= 7	18 RUN=	71									
					STAB	ILITY AXIS	COEFFICIENTS			STAB	.PRESS.COEF	F
PUINT	MACH	Ú	BETA	ALPHA	CL	Cυ	CPM	CLS	CNS	L/D	CDB	P8-1
532	.424	267.293	00	-11	. 1935	•0199	0808	.0015	.0009	9.707	.0039	4.4306
533	• 455	207.478	00	1.21	. 2705	•0225	0786	.0013	.0008	12.035	.0039	4.1229
534	<b>455</b>	598.014	00	2.20	.3510	• 0251	0727	.0009	.0008	13.976	.0040	4.0306
535	. 495	267.569	00	3.27	• 4289	•0291	0691	.0009	.0007	14.747	•0040	4.6306
536	• 425	267.570	00	4.31	•5061	•0335	0653	.0007	.0007	15.120	.0040	4.2768
537	• 455	267.664	00	5.36	• 5922	•0399	0575	•0012	•0006	14.841	.0040	4.7075
538	<ul><li>455</li></ul>	267.578	00	6.49	.6614	•0463	0516	•0014	.0007	14.299	.0039	4.2768
534	. 425	261.587	00	7.52	• <b>7</b> 253	.0537	0414	•0005	.0007	13.498	.0039	4.7383
540	- 455	261.541	00	8.65	. 7938	•0716	0306	.0003	0006	11.091	.0039	9.1381
541	• 455	268.265	00	9.71	• 8469	• 0996	0055	0008	0002	8.504	.0038	63.0769
542	• 455	268.378	00	10.82	.8799	.1319	•0295	-0004	.0002	6.672	.0037	87.6922
543	- 455	267.846	00	11.89	•9022	-1604	.0617	-0014	.0001	5.626	.0037	91.9999
544	- 450	268.595	00	13.02	.9354	.1919	.0890	-0014	.0002	4.873	.0036	98.9230
545	.450	200.632	00	15.21	•9798	·2505	.1271	.0009	0000	3.912	.0035	102-4614
546	•450	268.828	01	17.34	1.0059	•3033	-1510	•0009	.0001	3.316	.0033	98.0768
547	•450	268.840	01	19.35	1.0390	-3584	.1682	.0010	.0003	2.899	.0031	95.7691
548	• 456	269.607	00	21.42	1.0661	-4160	.1695	.0008	.0000	2.563	.0025	98.0768
549	• 424	267.020	-:00	•16	-1894	•0198	0830	.0014	.0009	9.563	.0039	4.6460

	1651= /	18 KUN=	12								
						BODA VXI	S COEFFICIENT	rs		BODY PRESS.	COEFF
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
586	-881	698.677	00	09	0349	.0170	.0004	.0007	0014	.0054	0.0000
587	-882	700.019	00	1.24	-1385	.0167	.0002	.0008	0019	•0055	0.0000
588	.883	700-429	00	2.65	.3153	.0154	.0002	.0007	0013	• 0054	0.0000
589	.882	700.153	00	3.98	<b>4540</b>	.0149	0006	.0007	0019	•0054	0.0000
590	.883	700.711	00	5.16	•5576	.0160	0014	•0006	0024	• 0053	0.0000
591	.881	700-126	00	6.38	•6492	.0188	0036	•0006	0025	•0052	0.0000
592	.886	704.442	.00	7.62	.7246	.0193	0032	.0005	0027	• 0052	0.0000
593	.884	102.629	00	8.80	. 8003	.0195	0013	.0006	0024	•0050	0.0000
594	.886	704.331	•00	9.95	-8604	.0204	.0024	.0002	0018	•0050	0.0000
595	.888	705.299	.00	11.14	.8993	.0209	.0005	.0000	0007	•0050	0.0000

	TEST= 7	78 RUN=	72		STA	BILITY AXIS	COEFFICIENTS			STAB	.PRESS.COEF	F
POINT	MACH	Ü	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	COB	PB-1
586	.881	698.677	00	09	0349	.0170	.0120	.0004	.0007	-2.045	.0054	12.9697
587	.882	700.019	00	1.24	.1381	.0197	.0077	•0002	.0008	7.021	•0055	16.3972
588	-88-	700.429	00	2.65	.3142	.0300	0059	.0002	.0007	10.481	.0054	18.9889
589	.882	700.153	00	3.98	.4519	.0464	0108	0006	.0007	9.748	.0053	20.9084
590	.883	700.711	00	5.16	.5539	.0660	0081	0013	.0007	8.387	.0052	40.3771
591	.881	700.126	00	6.38	.6431	.0908	•0000	0035	.0010	7.084	.0052	79.2450
592	.886	704.442	.00	7.62	.7157	.1152	.0039	0031	.0009	6.211	.0051	93.5735
593	-884	702.629	00	8.80	·7879	.1416	.0132	0012	.0007	5.563	.0050	152.3911
594	-856	704.331	.00	9.95	. 8440	-1688	.0249	.0024	0002	5.001	.0049	157.6679
595	-888	705-299	-00	11.14	.8783	.1943	.0360	.0005	0001	4.521	.0049	200.3085

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

		•										
	TEST= 7	78 RUN=	73									
						BODY AXI	S COEFFICIEN	TS		BODY	PRESS.COEI	· F
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	ε	AB	CAC
609	-823	648.065	01	16	0379	.0158	.0000	.0008	.0001	-0	049 (	0.000
610	.823	648.064	01	16	0377	.0156	.0002	.0008	0001	.0	048 (	0.0000
611	.822	647.727	01	1.08	.0959	.0146	0002	.0007	0001	• 0	048	0.000
612	.823	648.950	00	2.39	.2401	.0097	0003	•0006	0007	•0	048 (	0.000
613	.822	647.682	00	3.70	.3853	.0031	0003	.0006	0012	• 0	048	0.000
614	- 823	648.457	00	4.98	•5274	.0002	0008	•0005	0012	•0	048	0.0000
615	-822	648.345	00	6.29	•6502	.0005	0021	•0005	0013	• 0		0.0000
616	.822	648.368	00	7 - 44	.7281	.0021	0004	•0006	0018	•0		0.0000
617	- 824	649.700	•00	8.60	•7624	.0063	0009	-0000	0010			0.0000
618	-824	650•L85	•00		.7921	.0101	0014	0000	0001			0.0000
619	- 825	651.305	•00		.7905	•0150	0003	0000	0005			0.0000
620	-825	650.974	•00		.7830	.0224	0007	-0005	0024			0.0000
621	•822	647.233	00	16	0381	.0158	0004	.0008	0007	• (	0048	0.0000
	TEST= 7	78 RUN=	73									
						ILITY AXIS C		2. 2			PRESS COE	
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
609	د82.	648.065	01	16	0378	.0159	.0085	•0000	.0008	-2.379	•0049	5.7852
610	-823	648.064	01	16	0377	.0157	.0091	•0002	.0008	-2.393	•0048	11.5712
611	- 822	647.727	01	1.08	• 0956	.0164	.0153	0002	.0007	5.815	-0048	11.1599
612	-823	648.950 647.682	00	2.39	.2395	•0197 •0280	.0227	~.0003	.0006	12.149	-0048	12.3390
613	•822 •823	648.457	00	3.70 4.98	• 1843 • 164		.0284	0003	•0006	13.707	-0048	15.8213
614	•822		00		•5254	•0460 •0717	.0291	0008	•0006	11.420	-0048	19.2631
615 616	.822	648.345 648.368	00 00	6.29 7.44	•6462 •7217	.0964	.0282	0020 0003	•0008	9.008	.0047	48.9454
617	-824	649.700	•00	8.60	•7529	•1202	.0410	0009	.0007 .0002	7.483 6.263	•0046 •0046	125.5859 162.3294
618	-824	650.185	•00	9.68	•7791	.1431	.0588	0014	•0002	5.444	•0045	192.4935
619	-825	651.305	•00	10.76	.7738	.1623	.0741	0003	.0002	4.769	•0044	198.6632
620	•825	050.974	•00	11.74	.7620	.1813	.0901	0006	-0006	4.203	•0044	199.4858
621	•822	647.233	00	16	0381	.0160	.0950 .0085	0004	.0008	-2.387	•0048	11.2696
361	2022	·	•00	-10			.0000	•0004	•0000	2.501	-0040	1102030

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	1521= 1	18 KUN=	14									
							S CUEFFICIEN				PRESS-COE	FF
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	+	CAB	CAC
635	.769	597.093	01	09	0353	.0153	0000	.0008	.0001			0.0000
636	.770	597.535	00	1.13	.0872	.0144	.0003	.0007	0004			0.0000
637	.705	593.584	00	2.35	.2085	.0104	0005	.0006	0013	•	0046	0.0000
638	.772	600.104	00	3.60	.3279	.0036	0006	.0005	0015		0046	0.0000
639	•77U	598.169	00	4.86	·4528	0041	0009	•0005	0016	•1	0046	0.0000
640	.771	599.162	00	6.18	.5801	0097	0003	•0006	0024	• (	0046	0.0000
641	.770	598.402	00	7.34	.6707	0085	.0010	•0006	0013	. (	0045	0.0000
642	.771	594.909	.00	8.50	.7122	0028	0004	•0002	0008	•1	0045	0.0000
643	.770	598.808	•00	9.51	.7302	.0055	0012	•0002	0018	•	0044	0.0000
644	.771	594.071	•00	10.61	.7342	.0137	0023	0000	0008	•	0043	0.0000
645	.771	544.514	•00	11.70	.7621	.0206	0014	.0004	0022	•	0043	0.0000
640	.771	599.747	•00	12.77	. 7824	.0243	0014	.0004	0025		0042	0.0000
647	.772	599.901	•00	13.87	.8044	.0266	0015	.0005	0027		0041	0.0000
648	.774	001.759	•00	16.14	.8599	.0275	0013	.0001	0026	• (	0038	0.0000
649	.776	604-193	•00	18.35	.9524	.0272	0010	.0004	0027			0.0000
650	.774	601.652	•00	20.50	1.0199	.0256	0007	.0001	0025		0025	0.0000
651	. 769	596.658	00	08	0313	.0155	.0001	.0008	0012			0.0000
	TEST= 7	78 RUN=	74		5740	CLITY AVIC C	OFFEREIENTS			5740	22565 605	
-0.41.7						ILITY AXIS C		61.6	64.6		.PRESS.COE	
POINT	MACH	503.00	BETA	ALPHA	CL	CU	CPM	CLS 0000	CNS	L/D	CDB	PB-1
635	-769	597.093 597.535	01	09	0352 .0869	•0154	.0072		.0008	-2.288	.0046	10.0357 9.9809
636	•77U	591.535 593.584	00	1.13		-0161	.0156	.0003	•000 <b>7</b>	5.403	.0047	
637	• 765		00	2.35	.2079	•0189	.0244	0004	-0007	10.986	.0046	9.4325
638	•772	600.164	00	3.60	.3270	•0242	.0338	0006	•0006	13.528	•0046	10.2277
639	.770	598.169	00	4.86	•4515	•0343	.0435	0008	•0006	13.172	• 0046	12.3116
640	.771	599.162	00	6.18	.5778	.0527	.0505	0002	•0006	10.958	.0045	19.8795
641	•770	598.402	00	7.34	.6663	•0773	.0610	.0010	.0005	8.624	.0045	77.7368
642	.771	598.909	•00	8.50	. 7048	-1025	.0779	0004	•0002	6.876	.0044	139.8445
643	.770	598-808	•00	9.51	.7193	.1261	.0887	0011	.0004	5-704	.0043	179.7429
644	-771	599.071	•00	10.61	.7192	-1487	.0932	0023	•0004	4.838	.0043	194.1388
645	.771	599.514	•00	11.70	.7421	• 1747	.1000	0013	.0007	4.248	•0042	227.8663
646	.771	599.747	•00	12.77	. 7577	•1966	.1036	0013	-0007	3.854	.0041	257.8920
647	•772	599.901	•00	13.87	.7745	-2187	.1085	0013	•0008	3.542	•0040	262.8277
648	•774	601-759	.00	16.14	.8184	. 2655	.1200	0012	•0005	3.083	.0036	185.0899
649	•770	604.193	•00	18.35	. 8954	.3256	.1195	0008	.0007	2.750	.0030	170.2828
650	-774	601-652	-00	20.50	•9463	-3812	.1238	0006	•0004	2.483	•0024	201-5424
651	•709	590.658	00	08	0312	·0155	.0075	.0001	.0008	-2.009	•0046	9.5422

MACH

BETA ALPHA

CNF

POINT

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

CAF

BODY AXIS COEFFICIENTS

CLB

CNB

CSF

BODY PRESS.COEFF

CAB

CAC

674 - 7.17	POTMI	MACH	Q	DETA	ALFRA	CIAL	CAF	CLO	CND	CSF	· ·	AD	CAL
675 - 7.17 543,880 -00 2.18	673	•7L7	543.173	00	18	0260	•0151	.0000	•0007	0000	•0	044 0	.0000
676 .117 543.275 -00 3.39 .3058 .00440001 .00050002 .0045 0.0000 677 .118 544.547 -00 4.57 .41630036 .0000 .00050017 .0044 0.0000 678 .716 543.090 -00 5.78 .528401050003 .00030002 .0044 0.0000 679 .118 544.399 .00 6.98 .61560107 .0003 .00040019 .0044 0.0000 680 .717 543.723 -00 8.10 .65880016 .0019 .00080028 .0043 0.0000 681 .717 543.72300 8.10 .65880016 .0019 .00080028 .0043 0.0000 682 .719 545.415 .00 10.26 .7226 .0114002300000014 .0042 0.0000 682 .719 545.4900 10.26 .7226 .0114002300000014 .0042 0.0000 685 .719 545.349 .00 10.26 .7226 .0114002300000014 .0042 0.0000 685 .719 545.349 .00 11.38 .7521 .01710014 .0004 .0015 .0042 0.0000 686 .718 545.006 .00 13.59 .7954 .02210015 .00030019 .0041 0.0000 686 .718 545.006 .00 13.59 .7954 .02210015 .00030019 .0041 0.0000 688 .720 541.00 0.17.98 .9161 .02260015 .00030017 .0004 .0000 688 .720 541.00 0.17.98 .9161 .02260015 .00010024 .0040 0.0000 688 .720 541.00 0.17.98 .9161 .02260015 .00010024 .0037 0.0000 689 .721 547.44 .00 22.20 1.0582 .02270021 .00010024 .0037 0.0000 689 .721 547.344 .00 22.07 .9338 .02550006 .00010024 .0037 0.0000 689 .721 547.344 .00 22.20 1.0582 .0237001000010028 .0025 0.0000 690 .721 547.344 .00 22.20 1.0582 .0237001000010028 .0025 0.0000 677 .78946 676 .717 543.43000 .478 .185 .0044 .0057 .0057 .0060 .00010032 .0017 0.0000 677 .78946 676 .717 543.43000 5.78 .5288 .0225 .0025 .0025 .0000 .0007 1.706 .0044 7.8278 677 .718 544.54700 5.78 .4152 .0266 .0045 .0051 .0001 .0004 .0007 5.606 .0044 7.8278 677 .718 544.54700 5.78 .5288 .0428 .0555 .0006 .0001 .0005 13.589 .0044 7.8278 677 .718 544.54700 5.78 .5288 .0428 .0555 .0002 .0003 .0003 .0033 .12.297 .0043 .12.797 .0043 .12.7977 679 .716 544.539 .00 5.78 .5288 .0428 .0555 .0002 .0003 .0003 .0003 .12.297 .0044 .8867 .0003 .00	674	.717	543.793	00	•97	.0873	.0141	0000	.0007	0000	•0	044 0	.0000
677	675	.717	543.880	00	2.18	.1965	.0104	0001	•0006	0014	•0	044 0	.0000
078   078   078   078   070   070   070   077   077   070   077   070   077   070   077   070   077   070   077   070   077   070   077   070	676	.717	543.275	00	3.39				.0005		• 0	045 0	• 0000
689 -719 -718	677	.718	544.547	00	4.57	.4163	0036	.0000	•0005	0017	•0	044 0	•0000
0.00	678	.716	543.090	00	5.78	•5284	0105	0003	•0003	0002	• 0	044 0	•0000
681	679	.718	544.359	•00	6.98		0107	.0003	.0004	0019	•0	043 0	.0000
682 719 545-415 .00 10-26 .7226 .0114002300000014 .0042 0.0000 684 .718 545-14900 11.38 .7521 .01710014 .00040015 .0042 0.0000 685 .719 545-389 .00 12-43 .7746 .02050015 .00030019 .0041 0.0000 685 .719 545-389 .00 12-43 .7746 .02050015 .00030019 .0041 0.0000 687 .719 545-389 .00 15-79 .8404 .02570021 .00010024 .0040 0.0000 687 .719 540-216 .00 15-79 .8404 .02570021 .00010024 .0037 0.0000 688 .720 547-20 .0010 .000 15-79 .8404 .02570021 .00010024 .0037 0.0000 688 .720 547-304 .00 20.07 .9838 .02550006 .00110028 .0025 0.0000 690 .721 547-344 .00 22-20 1.0582 .02370010000100010028 .0025 0.0000 690 .721 547-344 .00 22-20 1.0582 .02370010000100010032 .0017 0.0000 690 .721 547-344 .00 22-20 1.0582 .02370010000100010032 .0017 0.0000 690 .721 547-344 .00 22-20 1.0582 .02370010000100010032 .0017 0.0000 690 .721 547-344 .00 22-20 1.0582 .02370010000100010032 .0017 0.0000 690 .721 547-344 .00 22-20 1.0582 .02370010000100010032 .0017 0.0000 690 .721 543-39300 .971 .0371 .0155 .01570000 .0007 5.606 .0044 7.8804 674 .717 543-79300 .971 .0371 .0155 .01570000 .0007 5.606 .0044 7.7867 675 .711 543-27500 3.39 .3050 .0224 .03500000 .0007 5.606 .0044 7.8878 677 .718 544-54700 4.57 .4152 .0296 .0152 .0096 .0000 .0005 13.589 .0044 7.8878 679 .718 544-54700 5.78 .528 .0288 .0288 .05550002 .0003 12-297 .0043 12-7777 678 .718 544-54700 4.57 .4152 .0296 .0458 .0058 .0003 .0003 12-297 .0043 12-7777 678 .0044 .0068 .717 543-72300 8.10 .6525 .0912 .0764 .0019 .0005 7.153 .0043 12-7777 678 .0042 .0068 .0074 .0091 .0005 7.153 .0043 12-7777 688 .719 545-139 .0068 .0074 .0069 .0068 .0007 .0007 .0004 .0005 7.153 .0042 .712-2007 688 .719 545-139 .0042 .0565 .1169 .08660013 .0007 4.444 .0011 .0665 .0042 .0046 .718 545-339 .0042 .712-2007 .0063 .0064 .0069 .0007 .0066 .0069 .0072 .0063 .0064 .0069 .0072 .0063 .0064 .0069 .0072 .0063 .0064 .0069 .0072 .0063 .0064 .0069 .0072 .0063 .0064 .0	680	.717	543.723	00	8.10	<b>.</b> 6588	0016	.0019	.0008	0028	•0	043 0	.0000
684 718 545-14900 11.38 .7521 .01710014 .00040015 .0042 0.0000 685 .719 545.389 .00 12.43 .7766 .02050015 .00030019 .0041 0.0000 686 .718 545.389 .00 12.43 .7766 .02050015 .00030019 .0041 0.0000 686 .718 545.389 .00 13.59 .7954 .02310014 .00030024 .0040 0.0000 687 .719 540.215 .00 15.79 .8404 .02570021 .00010024 .0037 0.0000 688 .720 547.02000 17.98 .9161 .02600010 .00040017 .0031 0.0000 689 .721 547.307 .00 20.07 .9388 .02550006 .00010028 .0025 0.0000 690 .721 547.344 .00 22.20 1.0582 .02370010001000010028 .0025 0.0000 690 .721 547.344 .00 22.20 1.0582 .02370010001000010032 .0017 0.0000 673 .717 543.17300180260 .0152 .0089 .0000 .0007 -1.706 .0044 7.8964 674 .717 543.43400 2.18 .1959 .0178 .02660001 .0006 10.979 .0044 7.7867 675 .717 543.27500 3.39 .3050 .0224 .03500000 .0007 5.606 .0044 7.8876 676 .717 543.27500 3.39 .3050 .0224 .03500000 .0005 13.589 .0044 7.8878 679 .718 544.54700 4.57 4.152 .0296 .0151 .0001 .0005 14.020 .0044 8.8697 679 .716 544.359 .00 6.99 .0123 .0042 .0688 .0055 .0002 .0003 12.297 .0043 12.7977 688 .716 544.359 .00 6.99 .0123 .0042 .0688 .0003 .0003 .0003 .9.531 .0043 .003 .003 .003 .003 .003 .003 .00	681	.718	544.621	.00	9.20	•6953	•0058	0013	0001	0004	• C	1042 (	0.000
ABS	682	-719	545.415	•00	10.26	.7226	.0114	0023	0000	0014	• C	042 0	.0000
686 .71	684						.0171		•0004	0015	• 0	042 0	.0000
687 -719 540-216 -00 15.79 .8404 -02570021 -00010024 -0037 0.0000 689 .721 547.92000 17.98 .9161 0.02600010 0.00040017 0.0031 0.0000 689 .721 547.944 .00 20.07 .9838 .02550006 .00010028 .0025 0.0000 690 .721 547.944 .00 22.20 1.0582 .0237001000010032 .0017 0.0000 690 .721 547.944 .00 22.20 1.0582 .0237001000010032 .0017 0.0000 690 .721 547.944 .00 22.20 1.0582 .0237001000010032 .0017 0.0000 690 .721 547.944 .00 22.20 1.0582 .0237001000010032 .0017 0.0000 690 .00010032 .0017 0.0000 690 .00010032 .0017 0.0000 690 .00010032 .0017 0.0000 690 .00010032 .0017 0.0000 690 .0001 .0	685	•719	545.389				.0205	~.0015	.0003	0019	•0	041 (	•0000
688 -720 547.020 -000 17.98	686	•718	545.096	.00	13.59		•0231	0014	.0003	0024	• (	0040	.0000
## TEST= 778 RUN= 75    TEST= 778 RUN= 75	687						.0257	0021	.0001	0024	•(	037 (	0.000
TEST= 778 KUN= 75    STABILITY AXIS COEFFICIENTS   STAB.PRESS.COEFF   CLS   CNS   L/D   CDB   CD													0.000
TEST= 778 RUN= 75  STABILITY AXIS COEFFICIENTS  POINT MACH U BETA ALPHA CL CD CPM CLS CNS L/D CDB P8-1 673 .717 543.17300180260 .0152 .0089 .0000 .0007 -1.706 .0044 7.8964 674 .718 743.79300 .97 .0871 .0155 .01570000 .0007 5.606 .0044 7.8964 675 .717 543.484000 2.18 .1959 .0178 .02460011 .0006 10.979 .0044 7.6496 676 .717 543.27500 3.39 .3050 .0224 .03500000 .0005 13.589 .0044 7.8278 677 .718 544.54700 4.57 .4152 .0296 .0451 .0001 .0005 14.020 .0044 8.8697 678 .710 543.29000 5.78 .5268 .0428 .05550002 .0003 12.297 .0043 12.7777 679 .718 544.399 .00 6.98 .6123 .0642 .0548 .0003 .0003 9.531 .0043 53.0585 680 .717 543.72300 8.10 .6525 .0912 .0764 .0019 .0005 7.153 .0043 141.2156 681 .718 544.621 .00 9.20 .6655 .1169 .08460013 .0001 5.863 .0042 172.2007 682 .719 543.414900 11.38 .7340 .1652 .10680013 .0007 4.444 .0041 166.5810 685 .719 543.389 .00 12.43 .7350 .1867 .11360014 .0006 4.027 .0040 152.1851 686 .718 543.090 .00 13.59 .7678 .2093 .12030012 .0006 3.669 .0039 164.52.1851 686 .718 543.090 .00 13.59 .7678 .2093 .12030012 .0006 3.669 .0039 164.52.1851 686 .719 543.289 .00 12.43 .7350 .1867 .11360014 .0006 4.027 .0040 152.1851 688 .720 547.02000 15.79 .8017 .2534 .13040020 .0007 3.164 .0036 150.9511 688 .720 547.02000 15.79 .8017 .2534 .13040020 .0007 2.807 .0030 142.7249 689 .721 547.367 .00 2.007 .9153 .3615 .13350008 .0007 2.807 .0030 12.7327											•0	0025 (	0.0000
POINT   MACH   U   BETA   ALPHA   CL   CD   CPM   CLS   CNS   L/D   CDB   PB-1	690	-721	547.444	•00	22.20	1.0582	•0237	0010	0001	0032	•0	017 (	0.0000
POINT MACH Q BETA ALPHA CL CD CPM CLS CNS L/D CDB P8-1 673 -717 543-17300180260 .0152 .0089 .0000 .0007 -1.706 .0044 7.8964 674 .717 543-79300 .97 .0871 .0155 .01570000 .0007 5.606 .0044 7.7867 675 .717 543-84000 2.18 .1959 .0178 .02460001 .0006 10.979 .0044 7.6496 676 .717 543-84000 2.18 .1959 .0178 .02460001 .0006 10.979 .0044 7.8278 677 .718 543-27500 3.39 .3050 .0224 .03500000 .0005 13.589 .0044 7.8278 677 .718 543-309 .00 4.57 .4152 .0296 .0451 .0001 .0005 14.020 .0044 8.8697 679 .718 543-309 .00 6.98 .5123 .0642 .0548 .05550002 .0003 12.297 .0043 12.7777 679 .718 544-359 .00 6.98 .6123 .0642 .0648 .0003 .0003 9.531 .0043 53.0585 680 .717 543.72300 8.10 .6525 .0912 .0764 .0019 .0005 7.153 .0043 141.2156 681 .714 544-621 .00 9.20 .6855 .1169 .08460013 .0001 5.863 .0042 172.2007 682 .719 545-14900 10.26 .7090 .1399 .09600023 .0004 5.066 .0042 176.8637 684 .718 545-14900 11.38 .7340 .1052 .10680013 .0007 4.444 .0041 166.5810 685 .719 545-389 .00 12.43 .7520 .1867 .11360014 .0006 4.027 .0040 152.1851 686 .718 545-090 .00 13.59 .7678 .2093 .12030012 .0006 3.669 .0039 164.5246 687 .719 545-389 .00 15.79 .8017 .2534 .13040020 .0007 3.164 .0036 150.9511 688 .720 547.02000 17.98 .8633 .3075 .13350008 .0007 2.807 .0030 12.274 .0030 142.7249 689 .721 547.367 .00 15.79 .8017 .2534 .13040020 .0007 3.164 .0036 150.9511 688 .720 547.02000 17.98 .8633 .3075 .13350008 .0007 2.807 .0030 12.7249 689 .721 547.367 .00 20.07 .9153 .3615 .13330005 .0003 2.532 .0023 159.1774		TEST= 7	78 RUN=	75		STAB	ILITY AXIS O	DEFFICIENTS			STAB	PRESS.COEF	: F
673	POINT	MACH	Q	BETA	ALPHA				CLS	CNS			
674	673	•717	543.173	00	18	0260	.0152	.0089					
675	674	.717	543.793	00	•97	.0871	.0155		0000	.0007	5.606		7.7867
677	675	•717	543.830	00	2.18	•1959	.0178		0001	.0006			7.6496
677	676	-71/	543.275	00	3.39	• 3050	•0224	.0350	0000	• 0005	13.589	.0044	7.8278
676	677	.718	544.547	00	4.57	•4152	• 0296		•0001	.0005	14.020	-0044	8.8697
679	678			00	5.78	•5268	• 0428		0002	-0003	12.297	•0043	12.7777
681				•00					• 0003	.0003	9.531	.0043	53.0585
682								.0764	.0019	• 0005	7.153	.0043	141.2156
684								.0846					172.2007
685													
686  •718  545•096  •00  13•59  •7678  •2093  .1203  -•0012  •0006  3•669  •0039  164•5244  687  •719  546•216  •00  15•79  •8017  •2534  .1304  -•0020  •0007  3•164  •0036  150•9511  688  •720  547•020  -•00  17•98  •8633  •3075  .1335  -•0008  •0007  2•807  •0030  142•7249  689  •721  547•307  •00  20•07  •9153  •3615  .1333  -•0005  •0003  2•532  •0023  159•1774													166.5810
687													
688 •720 547.02000 17.98 •8633 •3075 .13350008 •0007 2.807 •0030 142.7249 689 •721 547.367 •00 20.07 •9153 •3615 .13330005 •0003 2.532 •0023 159.1774													
689 .721 547.367 .00 20.07 .9153 .3615 .13330005 .0003 2.532 .0023 159.1774							2534	7 20 h	0020	. 0.007	3.164	0026	150 0511
111 1111 1111 1111													
13830010 .0003 2.302 .0016 178.0977		.720	547.020	00	17.98	.8633	.3075	·1335	0008	.0007	2.807	.0030	142.7249
	689	•720 •721	547.020 547.367	00 .00	17.98 20.07	•8633 •9153	•3075 •3615	.1335 .1333	0008 0005	.0007	2.807 2.532	.0030 .0023	142.7249 159.1774

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	1EST= 7	78 KUN=	76									
						RODA WXI	S COEFFICIEN	NTS		BODY	PRESS.COE	FF
POINT	MACH	۵	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
704	•665	489.530	00	15	0240	.0152	.0003	.0008	0003		0043	0.0000
705	•605	490.095	00	1.04	.0830	-0143	.0001	.0007	.0000		0042	0.0000
706	- 663	488.008	00	2.15	.1814	.0110	0002	.0006	0010		0043	0.0000
707	-665	489.232	00		.2838	.0053	.0002	•0006	0013			0.0000
708	-604	488.855	00		.3864	0023	0002	•0005	0007			0.0000
709	.665	490.128	00		.4878	0087	0001	.0004	0007			0.0000
710	.665	489.807	00		.5717	0067	0002	.0006	0003			0.0000
711	.666	490-497	00		.6332	0004	.0026	•0008	0023		0041	0.0000
712	.666	490.875	00		.6709	.0064	.0011	.0005	0015			0.0000
713	.666	491.067	.00		.7077	.0103	0020	•0000	0009			0.0000
714	.666	491.267	.00		.7397	.0137	0016	.0003	0019			0.0000
715	.665	490.417	.00		.7688	.0169	0012	.0005	0029			0.0000
716	•666	491.195	00		.7921	.0203	0015	.0004	0016			0.0000
717	.607	491.500	•00		.8297	.0239	0016	.0005	0021			0.0000
718	.667	491.930	•00		.8912	.0248	0012	.0005	0032			0.0000
719	.661	492.222	.00		.9545	.0247	0013	.0005	0038			0.0000
720	.668	493.129	•00		1.0230	.0236	0013	•0001	0015			0.0000
721	.664	489.214	01		0241	.0151	.0003	.0008	.0012			0.0000
	TEST= 7	78 RUN=	76									
						ILITY AXIS C					PRESS.COE	
POINT	MACH	ų .	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
704	• 665	489.530	00	15	0239	.0153	•0093	-0003	•0008	-1.567	.0043	6.7722
705	•665	490.095	00	1.04	.0827	•0158	.0165	•0001	.0007	5.253	.0042	6.9505
706	• 66 3	488.008	00	2.15	.1809	.0177	.0 <u>2</u> 55	0002	•0006	10.191	•0043	6.9230
707	-665	489.232	00	3.33	.2830	.0217	.0356	-0003	•0006	13.016	.0042	6.7037
708	•664	488.855	00	4.48	.3054	.0279	.0450	0002	.0005	13.798	•0042	7.1287
709	.665	490.128	00	5.66	• 4863	.0395	.0550	0001	•0004	12.323	•0042	8.3077
710	-665	489.807	00	6.84	.5684	.0014	.0646	0001	•0006	9.261	•0042	55.8005
711	•666	490.497	00	7.94	.6271	.0871	.0723	•0027	.0004	7.197	.0041	119.2792
712	.655	490.875	00	9.04	6615	.1118	.0826	•0011	•0003	5.920	•0040	171.5167
713	•606	491.007	•00	10.12	.6949	.1345	.0964	0019	•0004	5.169	•0040	173.1619
714	.666	491.267	•00	11.24	.7228	.1576	.1100	0016	•0006	4.587	•0039	153.4190
715	-665	490.417	•00	12.32	.7475	.1805	.1200	0011	.0007	4.140	.0039	157-1208
716	-666	491.195	00	13.45	.7656	- 2040	.1269	0014	.0008	3.754	.0038	142.3136
717	.607	491.500	-00	15.64	.7926	•2466	.1396	0014	• 0009	3.214	.0035	120-9254
718	•667	491.930	•00	17.76	.8412	• 2955	.1422	0010	•0008	2-846	•0030	125.0385
719	•667	492.222	.00	19.86	.8893	.3475	.1414	0010	•0009	2.559	•0023	143.1362
720	668	493.129	•00	21.97	•9399	-4046	.1422	0012	•0005	2.323	-0016	167.4036
721	.664	489.214	01	12	0241	.0151	.0085	•0003	•0008	-1.591	•0042	6.9916

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	1621= 11	B KUN= 1										
							S COEFFICIEN	ITS		80DY	PRESS.COEF	FF
POINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	С	AB	CAC
735	.224	72.544	00	•02	0167	.0101	0003	.0007	.0002	.0	036 (	0.0000
736	-225	73.234	00	1.01	.0768	.0110	0004	-0010	0009	•0	036	0.0000
737	.225	73.235	00	1.98	.1391	.0091	0001	•0012	0021	•0	036 (	0.0000
738	.224	72.549	00	2.99	-2192	•0071	0001	.0008	0032	•0	037 (	0.0000
739	.225	73.141	.00	3.98	.3115	•0020	0002	.0004	0041	• 0	036	0.0000
740	• 225	73.045	.00	4.99	.3904	0043	•0005	•0006	0057			0.0000
741	-225	73.048	00	6.02	<b>.</b> 4668	0130	0002	•0009	.0036			0.0000
742	•225	72 <b>.</b> 958	-00	7.03	• 5465	0162	0003	•0005	0073			0.0000
743	- 225	72.977	•00	8.10	•6240	0116	0007	.0008	0080			0.0000
744	.225	72.901	.00	9.11	.7027	0050	0011	.0010	0085			0.0000
745	. 225	72.823	•00	10.16	.7505	.0002	0011	•0005	0093			0.0000
746	.225	72.843	•00	11.17	.7813	.0058	0011	.0006	0098			0.0000
747	-225	72.960	.00	12.23	.7947	-0101	0015	.0007	0102			0.0000
748	.226	73.470	.00	7.98	.6196	0089	0010	.0008	0076	• 0	036	0.0000
	TEST= 7	78 RUN=	77		STAG	ILITY AXIS (	OEEETC LENTS			CTAD	PRESS.COE	E E
POINT	MACH	J	BETA	ALPHA	CL	CD CD	CPM	CLS	CNS	L/D	CD8	PB-1
735	-224	72.544	00	•02	0167	•0101	.0075	0003	.0007	-1.658	•0036	•4524
736	•225	73.234	00	1.01	.0766	.0124	.0075 .0144	0004	.0010	6.180	•0036	•0548
737	.225	73.235	00	1.98	.1387	.0139	.0247	0000	•0012	9.942	•0036	0.0000
738	.224	72.549	00	2.99	.2186	.0185	.0336	0001	.0008	11.814	.0036	•4661
739	-225	73.141	•00	3.98	.3107	.0236	.0330 .0345	0001	•0004	13.188	.0036	.0137
740	.225	73.045	-00	4.99	.3893	.0296	.0432	.0006	.0006	13.133	.0036	•0411
741	.225	73.048	00	6.02	• 4656	.0361	.0520	0001	•0009	12.905	.0036	.0137
742	.225	72.958	•00	7.03	•5443	.0508	.0654	0002	.0005	10.714	.0036	2.7418
743	• 225	72.977	.00	8.10	•6194	.0765	.0732	0006	.0008	8.100	.0036	14.2310
744	-225	72.901	•00	9.11	•6946	.1063	.0757	0009	.0012	6.535	•0034	33.7276
745	-225	72.823	-00	10.16	.7387	-1325	0871	0010	.0007	5.573	.0034	45.6550
746	-225	72.843	.00	11.17	• 7654	.1570	.0946	0010	•0008	4-874	•0034	44.1468
747	. 225	72.960	•00	12.23	• 7745	-1783	.1148	0013	.0010	4.344	.0032	41.8161
748	• 226	73.470	-00	7.98	.6148	•0772	.0729	0009	•0009	7.966	•0036	14-9713

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 1	78 RUN= 1	78								
						RODA VXI		BODY PRESS.	COEFF		
PUINT	MACH	Q	BETA	ALPHA	CNF	CAF	CLB	ÇNB	CSF	CAB	CAC
749	.450	268.647	00	22	0221	.0163	0001	.0007	.0001	• 0039	0.0000
750	.455	263.013	00	.81	.067₺	.0158	.0007	.0008	0017	• 0039	0.0000
751	.456	268.739	00	1.85	.1561	.0131	0004	.0007	0020	•0039	0.0000
752	.425	267.475	•00	2.94	.2379	•0087	0003	.0006	0032	•0038	0.0000
753	.455	268.112	•00	4.00	.3223	.0020	0006	.0006	0040	•0038	0.0000
754	.456	268.750	.00	5.09	.4064	0070	0007	.0006	0050	.0038	0.0000
756	-427	269.586	•00	6.18	.4854	0142	0007	.0003	0034	•0038	0.0000
751	•457	270.191	•00	7.30	•5685	0132	0004	.0010	0049	•0038	0.0000
758	.424	260.575	00	8.37	.6408	0046	.0002	.0008	0036	•0038	0.0000
759	455	267.929	•00	9.42	.6844	.0016	.0002	•0006	0042	•0037	0.0000
760	.456	268.659	.00	10.59	.7324	.0071	0006	.0008	0045	•0036	0.0000
761	.455	268.187	•00	11.66	.7414	.0106	0011	.0005	0044	•0035	0.0000
762	-450	268.815	.00	12.76	.7722	.0137	0018	-0004	0046	•0035	0.0000
763	-457	269.512	•00	14.89	-8105	.0176	0014	.0005	0033	•0034	0.0000
704	.457	270.312	.00	16.94	. 8576	.0210	0007	.0007	0046	.0031	0.0000
765	.450	268.923	00	7.30	.5708	0135	0005	.0012	0022	.0038	0.0000

	1EST= 7	78 KUN=	78									
					STAI	BILITY AXIS (	STAB.PRESS.COEFF					
TOLOG	MACH	Q	BETA	ALPHA	CL	CJ	CPM	CLS	CNS	L/D	CDB	PB-1
749	.450	268.647	00	22	0220	.0164	.0070	0001	.0007	-1.343	.0039	4.9489
750	.455	268.013	00	.81	•067₺	.0167	.0159	.0007	.0008	4.043	•0039	4.3458
751	.456	268.739	00	1.85	• 1556	.0181	.0234	0003	•0008	8.595	.0039	4.4143
752	.455	267.475	.00	2.94	.2372	.0209	.0333	0003	.0007	11.366	•0038	4.6199
753	. 450	260.112	.00	4.00	.3214	.0245	.0410	0006	•0006	13.138	.0038	4.5925
754	. 456		.00	5.09	· 4054	.0291	.0474	0006	.0007	13.911	.0038	4.7296
756	.457	269-586	.00	6.18	.4841	.0382	.0570	0007	•0004	12.678	.0037	5.1820
757	.457	270.191	.00	7.30	• 5656	.0591	.0691	0002	.0010	9.563	.0037	18.1663
758	.454	266.575	00	8.37	.6346	.0887	.0755	.0003	.0008	7.151	.0037	66.3574
759	.455	267.929	.00	9.42	.6749	.1136	.0824	.0002	•0006	5.939	•0036	106.1173
760	.456		.00	10.59	.7186	.1410	.0969	0004	•0009	5.074	•0036	119.5534
761	•455	268.187	.00	11.66	.7240	.1602	.1118	0010	.0007	4.518	.0035	123.9407
762	-450	268.815	•00	12.76	.7501	. 1840	.1283	0017	•0008	4.078	•0034	112.1498
763	.457	269.512	•00	14.89	.7787	.2253	.1489	0012	•0009	3.457	.0033	80.6163
764	457	270.312	•00	16.94	.8143	. 2699	.1564	0005	.0009	3.017	.0029	74.3096
765		268 923	00	7.30	.5079	.0592	0695	0003	-0012	9.594	.0037	20.0172

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7					BODY AXIS COEFFICIENTS				BODY PRESS-COEFF				
POINT	MALH	Q	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	C	AB	CAC		
801	.881	696.667	00	09	0053	•0154	•0004	.0007	0006	•0	054	0.000		
802	•882	697.882	01	•98	.0818	.0145	•0006	•0007	0004	• (	055	0.000		
803	.865	698.531	01	•99	.0837	.0145	.0011	.0007	0009	•(	055	0.000		
804	-831	696.924	01	2.10	.1792	.0111	•0009	.0007	0004	• (	054	0.000		
805	. ರರ೨	098.661	01	3.27	·2689	.0060	•0009	.0007	0003	•(	055	0.000		
806	.881	697.037	01	4.38	.3587	0001	•0015	•0007	0005	.(	054	0.000		
807	.883	698.444	01	5.54	.4668	0030	.0018	.0010	0014	.(	054	0.000		
808	-882	698.039	01	6.72	.5502	0004	•0021	.0007	•0002	• (	054	0.000		
809	.834	699.576	00		•6306	•0022	.0014	•0005	•0004	• (	0053	0.000		
810	.880	095.966	00	9.04	•6690	•0009	.0011	•0004	0002	• (	0052	0.000		
811	• 885	700.673	01		•7464	•0067	•0037	.0007	0008			0.000		
812	.865	700.876	00		.7449	.0136	-0003	•0002	0003	• (	0051	0.000		
813	- 885	700.688	00	12.43	.7718	•0154	-0001	•0002	0008	. (	0050	0.0000		
814	.884	699.700	00		.8020	-0165	.0005	.0003	•0005	- (	0049	0.000		
815	- 884	699.321	01	06	0055	.0150	•0002	.0007	0004		0054	0.0000		
	TES1= 7	78 KUN=	79											
						SILITY AXIS C				STAB	PRESS-COE	FF		
POINT	MACH	Ų	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1		
801	.881	696.667	00	09	0053	•0154	• 0056	.0004	-0007	345	.0054	9.772		
802	.882	697.882	01	-98	.0816	.0159	.0044	.0006	.0007	5.143	•0055	065		
803	.863	698.531	01	•99	.0834	.0159	.0057	.0011	.0007	5.248	•0055	9.925		
804	•881	690.924	01	2.10	.1787	.0176	.0066	.0009	.0007	10.138	.0054	10.365		
805	.883	098.661	01	3.27	.2681	.0213	.0107	.0010	.0007	12.560	.0055	13,439		
806	-881	697.037	01	4.38	. 3577	.0273	.0110	.0015	•0006	13.113	.0054	17.294		
867	.883	098.444	01	5.54	• 4649	.0421	.0101	.0019	•0009	11.055	.0054	21.181		
908	-882	648.039	01	6.72	• 5464	.0639	.0263	.0022	•0005	8.546	.0054	35.575		
809	.884	694.576	00	7.91	.6243	.0889	.0527	.0014	.0003	7.019	.0053	30.250		
810	.880	695.966	00	9.04	• 6606	.1060	.0859	.0012	•0002	6.235	.0051	44.140		
811	. 885	700.673	01	10.20	.7334	.1387	.1112	.0038	.0001	5.287	.0051	49.850		
		700.876	00	11.33	•7277	.1596	.1621	.0004	.0002	4.561	.0050	F7 0//		
812	. 865													
812 813	.885	100.688	00	12.43	• 7504	.1812	.1892	.0001	.0002	4.142	.0049	57.866 51.607		
812														

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN=	80									
							S CUEFFICIEN				PRESS-COE	
POINT	MACH	Q	BETA		CNF	CAF	CFR	CNB	CSF		CAB	CAC
830	.821	643.981	01	21	0099	.0154	0001	.0008	.0009			0.0000
831	.820	642.917	01	- 85	.0759	.0147	•0006	.0009	.0006	• (	0049	0.0000
832	.821	644.551	01	1.98	.1646	.0114	•0009	.000B	.0006	• !	0049	0.0000
833	-823	645.630	01	3.10	.2454	.0066	.0008	8000.	.0007	•	0049	0.0000
834	.822	645.176	01	4.20	.3290	.0005	.0014	.0009	.0015	•	0048	0.0000
835	-822	645.558	01	5.36	.4232	0029	.0014	•0005	.0019	•	0048	0.0000
836	.823	645.915	01	6.49	.5035	0018	.0015	•0006	.0015	•	0048	0.0000
837	-822	645.304	01	7.67	•5823	0023	.0018	.0007	.0007		0047	0.0000
838	-823	646.198	01	8.84	.6462	.0008	.0044	.0012	0013		0047	0.0000
839	.823	047.505	01	9.96	•6898	.0057	.0018	•0006	.0011	•	0046	0.0000
840	-825	649.066	01	11.12	.7335	.0076	•0019	.0005	•0026		0045	0.0000
841	-826	649.904	01	12.20	.7698	.0100	•0005	.0004	.0021	• 1	0044	0.0000
842	•825	649.351	00	13.36	.7995	.0128	.0003	•0004	-0018		0043	0.0000
843	-822	645.692	01	21	0114	.0153	.0004	.0009	•0006		0048	0.0000
	TEST= 7	78 KUN=	80			ILITY AXIS C				C7.11	22544 225	
		_				STAB-PRESS-COEFI						
PUINT	MACH	Q	BETA	ALPHA	CL	CO	CPM	CLS	CNS	L/D	CDB	PB-1
830	-851	643.981	01	21	0099	.0154	.0057	0001	.0008	640	.0048	9.3550
831	-820	042.917	01	•85	.0750	.0158	-0061	•0006	.0009	4.795	•0049	9.1134
832	-821	644.551	01	1.98	.1641	.0171	.0084	.0009	.0008	9.617	•0049	8.6083
833	-823	645.630	01	3.10	• 2447	.0198	.0141	.0009	.0008	12.334	.0048	9.6404
834	.822	645.170	01	4.20	.3281	•0246	.0188	.0014	•0008	13.337	•0048	11.1337
835	-822	645.558	01	5.36	.4216	.0366	.0170	.0014	•0004	11-527	•0048	18.8093
836	•823	645.915	01	6.49	• 5004	•0551	.0353	.0016	.0004	9.075	•0048	26.4074
837	-822	645.304	01	7.67	•5774	.0755	.0632	.0019	-0004	7.651	.0047	31.1289
838	د 82ء	646.198	01	8.84	•6384	.1001	.1015	•0045	•0005	6.378	•0046	38.9801
839	-823	647.505	01	9.96	∙67ძ5	-1249	.1434	.0019	.0003	5.432	•0046	40.4075
840	-825	649.066	01	11.12	.7183	.1469	•1699	•0020	.0002	4.825	-0044	46.7761
841	•826	649.904	01	12.20	. 7503	•1725	.1971	•0005	•0002	4.350	.0043	47.1055
842	-825	649.351	00	13.36	.7744	.1972	•2202	.0003	.0003	3.930	•0042	47.9839
843	-822	645.692	01	21	0113	.0153	•0051	.0004	.0009	738	•0048	9.5087

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	1EST= 7	78 RUN=	31									
							S COEFFICIEN				PRESS.COE	
POINT	MACH	Q	BETA	ALPHA	C NF	CAF	CLB	CNB	CSF		AB	CAC
857	.768	595.007	00	10	0141	.0151	.0005	.0008	0006			0.0000
858	.769	595.526	01	• 95	.0644	-0146	.0007	.0008	.0006			0.0000
859	•769	595.170	00	2.03	.1488	.0117	.0006	.0007	0003	• (		0.0000
860	. 769	595.702	01	3.18	.2326	-0070	.0005	.0007	0001	• (		0.0000
861	.770	596.243	00	4.23	.3086	.0011	•0005	•0005	0000	. (	046	0.0000
862	.769	596.039	00	5.34	.3914	0040	.0010	•0004	.0010	• (	0046	0.0000
863	.770	596.695	00	6.49	.4765	0028	.0012	.0005	.0008	• (	3046	0.0000
864	.770	596.837	01	7.63	•5494	.0001	.0022	•0010	.0004	. (	0046	0.0000
865	.770	596.739	01	8.79	.6183	•0005	.0051	•0014	0014	• (	0045	0.0000
866	.770	597.018	Oi	9.89	•6668	.0024	.0045	-0010	.0007	• (	0044	0.0000
867	.770	596.748	00	11.07	.7134	.0052	.0006	•0004	.0018	• (	0044	0.0000
868	.771	598-102	01	12.18	.7552	.0068	.0006	.0004	.0024	• (	0043	0.0000
869	.772	598.369	00	13.35	• 7944	.0087	.0003	•0004	.0022		0041	0.0000
870	.772	599.011	00	15.61	.8710	•0115	.0003	•0005	.0014	. (	0040	0.0000
871	.770	596.476	01	10	0145	.0151	0000	•0009	.0010		0046	0.0000
	TEST= 7	78 RUN=	81									
						ILITY AXIS C	STAB.PRESS.COEFF					
TAIO9	MACH	Q	BETA	ALPHA	CL	Çõ	CPM	CLS	CNS	L/D	CDB	PB-1
857	.708	595.007	00	10	0140	•0152	.0048	•0005	.0008	926	•0046	8.8718
858	. 769	545.526	01	• 95	•0642	-0156	.0059	.0007	.0008	4.108	.0047	8.9597
859	.769	595.170	00	2.03	.1483	•0169	.0072	.0007	.0007	8.768	.0047	8.7401
860	. 769	5 95 • 702	01	3.18	.2318	•0198	-0146	• 0005	.0007	11.681	.0047	8.3228
861	.770	596.243	00	4.23	. 3077	• 0239	.0210	•0005	.0005	12.898	.0046	8.7181
862	<b>.</b> 769	590.039	00	5.34	.3901	•0324	.0204	•0010	.0003	12.023	.0046	12.9564
863	.770	596.695	00	6.49	.4738	.0511	.0312	.0012	.0004	9.266	.0046	40.7369
864	.770	596.837	01	7.63	• 5446	•0731	.0664	.0023	.0007	7.451	.0046	36.2350
865	.770	596.739	01	8.79	.6110	• 0950	.0950	.0052	.0006	6.432	.0044	40.4075
866	.770	597.018	01	9.89	•6565	·1169	.1288	.0046	.0002	5.617	.0043	46.7761
867	•770	596.748	00	11.07	.6991	•142L	.1735	.0007	.0003	4.921	.0043	40.5173
868	.771	598.102	01	12.18	. 7368	-1660	.1980	•0007	.0003	4.439	.0042	43.5918
869	•772	598.369	00	13.35	•7709	.1918	.2210	•0004	.0003	4.019	.0040	46.5565
870	•772	599.011	00	15.61	.8358	• 2455	.2595	.0004	.0004	3.405	.0038	54.9015
871	.770	596.476	01	10	0145	•0151	.0046	0000	.0009	959	•0046	9.0036

	TEST= 7	70 RUN=	82									
							S COEFFICIE				PRESS.COE	
POINT	MACH	ų .	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
885	• 717	542.995	01	10	0110	.0151	.0007	.0009	•0005			0.0000
886	• 717	542.698	01	•97	.0680	.0144	.0002	• 0009	-0011			0.0000
887	.716	542.322	01	2.04	-1457	.0116	•0004	•0009	.0011			0.0000
888	-717	542.872	01	3.14	-2208	•0072	-0007	.0009	.0010			0.0000
889	.716	<b>342.509</b>	01	4.21	.2961	.0011	.0007	•0008	.0010			0.0000
890	•717	543.099	01	5.29	•3777	0047	-0011	•0006	•0022			0.0000
891	.717	542.791	01	6.42	•4620	0046	.0018	.0008	.0017	•	0044	0.0000
892	./17	543.152	01	7.57	•5366	0026	.0043	.0018	0009			0.0000
893	•717	543.069	01	8.72	•6043	0010	.0048	.0015	0006	•	0043	0.0000
894	.718	544.30L	01	9.82	<b>-</b> 6580	0004	•0063	.0015	0000	•		0.0000
895	.719	545.786	01	11.00	• 7037	•0026	.0008	.0007	.0021		0041	0.0000
896	•718	544.412	01	12-11	-7511	.0041	•0005	•0005	.0031		0040	0.0000
897	.713	544.678	01	13.24	• 7944	·U054	•0004	•0005	.0028	•	0039	0.0000
898	<b>.7</b> 21	540.800	00	15.51	-8761	.0074	.0002	.0004	.0020	•	0038	0.0000
899	•720	546.751	00	17.69	•9440	.0085	0002	•0005	.0017	•	0036	0.0000
900	.721	547.688	00	19.75	•9956	•0089	.0001	-0005	.0007		0035	0.0000
902	.717	243.014	01	07	0116	.0147	•0003	.0011	•0022	•	0044	0.0000
	IEST= 7	78 KUN=	82		27.11							
DOLLIT	14.5.0.1		05.74	8 4 D 1 1 4		ILITY AXIS C		a. r			.PRESS.COE	
POINT	MACH	ų Lieta nas	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
885	-717	542.995	01	10	0110	.0152	.0047	.0007	•0009	725	•0044	7.7519
886	•717	242.698	01	•97	.0678	.0156	.0077	.0002	•0009	4.356	•0044	7.5982
887	-710	542.322	01	2.04	-1452	.0168	.0101	.0004	.0009	8.645	•0045	7.2468
888	• 7 L 7	542.872	01	3.14	.2201	•0192	.0146	.0007	•0008	11.439	•0045	8.1691
889	•710	542.509	01	4.21	. 2952	•0229	.0221	.0008	•0008	12.920	-0044	8.0813
890	•717	543.099	01	5.29	• 3766	•0302	.0254	.0012	.0005	12.482	•0044	11.1996
891	•717	542.791	01	6.42	• 4596	.0471	.0281	.0019	•0005	9.754	•0044	26.5172
892	•717	543.152	01	7.57	•5323	•0682	.0555	.0045	.0012	7.810	•0043	23.1682
853	• 71.7	543.009	01	8.72	• 5974	•0406	.0868	•0049	.0008	6.593	•0042	30.8546
894	•718	544.361	01	9.82	.6485	.1118	.1176	.0065	•0004	5.798	•0042	46.9957
895	•719	545.786	01	11.00	• 6903	.1308	.1702	.0009	-0005	5.047	•0041	35.6860
896 0117	•718	544.412	01	12.11	• 7335	.1616	.1963	.0006	•0004	4.539	•0039	43.4820
897	-718	544.678	01	13.24	• 7720	.1872	.2179	•0005	•0004	4.123	•0038	50.2898
898	• 721	540.800	00	15.51	.8422	• 2414	.2617	.0003	.0003	3.489	-0036	59.9524
899	• 720	546.751	00	17.69	.8968	•2949	. 2974	0001	•0006	3.041	.0034	65.3328
900												
902	•721 •717	547.688 543.014	00 01	19.75 07	•9340 -•0115	•3448 •0147	.3277 .0053	.0003 .0003	.0005 .0011	2•709 -•784	•0033 •0044	57•9760 7•8397

TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 KUN= 8	83									
						ROUA VXI	S CUEFFICIEN	TS		BOOY	PRESS.COEF	=
PUINT	MACH	Q)	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		AB	CAC
916	.604	408.513	00	13	0172	-0151	.0002	*000B	0003			.0000
917	-665	484.645	00	•90	.0592	-0145	.0004	.0008	0003			.0000
913	-605	489.017	00	1.93	.1381	•0122	.0005	.0007	0002			.0000
919	-664	488.542	00	3.05	.2121	.0077	.0005	.0007	0002			•0000
920	• 605	404.082	00	4.11	.2829	-0020	•0005	.0006	0001			.0000
921	•604	488.497	00	5.16	.3578	0044	.0007	.0004	.0013			.0000
922	-600	490.696	00	6.29	•4446	0056	.0014	.0005	0005			.0000
923	•664	4ರರ.ರ೨೮	01	7.40	.5177	0038	.0037	.0014	0029			.0000
924	• 66 p	489.568	01	8.62	<b>-</b> 5886	0037	.0065	•0020	0043			•0000
925	.050	490.956	01	9.70	.6504	0027	.0075	.0018	0044			• 0000
926	-656	490.033	00	10.87	.6968	-0010	.0006	.0003	.0001			-0000
927	• 66 5	484.341	00	11.99	.7369	-0017	•0005	.0002	0003			•0000
928	•666	470.120	00	13.10	.7865	•0025	.0002	.0003	•0010			•0000
929	• 508	492.119	00	15.45	.8708	•0040	.0004	.0002	.0012			•0000
930	•000	490.642	00	17.57	.9515	.0053	.0000	.0003	-0007			•0000
931	-667	491.907	00	19.69	1.0053	•0059	0002	.0003	.0000			.0000
932	-601	491.639	00	21.71	1.0612	• 0054	.0007	.0003	.0004			•0000
933	• 66 2	489.727	00	14	0173	.0153	0001	.0008	0001	• 1	0042 0	•0000
	1EST= 7	78 RUN=	83		CTAN	ILITY AVIC (	COEFFICIENTS			CT 1.0	DD CEE COEE	<b>.</b>
PUINT	MACH	۵	bETA	ALPHA	CL	CD CD	CPM	CLS	CNS	L/D SIAB	PRESS.COEF	
916	• 004	488.513	00	13	0171	•0152	•0025	•0002	•0008	-1.128	CDB •0042	PB-1 6∙8954
917	•605	489.645	00	•90	.0590	.0157	•0055	.0002	.0008	3.752	•0042 •0042	7.0492
918	•665	489.017	00	1.93	.1376	.0168	.0078	•0005	.0007	8.195	•0042	7.0711
919	•604	488.542	00	3.05	.2114	-0189	.0132	.0006	.0007	11.167	•0043	7.0272
920	•665	489.682	00	4.11	-2821	.0222	.0202	•0005	.0006	12.699	•0042	7.0272
921	.604	488.497	00	5.16	. 3567	.0278	.0248	.0007	•0003	12.816	•0042	8.3448
922	.606	490.090	00	6.29	•4426	.0431	.0243	.0015	.0003	10.259	.0042	15.4821
923	•604	488.838	01	7.40	.5139	.0629	.0475	.0039	.0009	8.177	.0041	27.8897
924	•665	484.508	01	8.62	-5825	.0846	.0750	.0067	.0010	6.888	.0041	23.3329
925	•666	490.956	01	9.70	.6416	.1069	.1041	.0077	.0005	6.004	•0040	46.0075
926	-656	490.038	00	10.87	•684l	-1324	•166l	.0006	.0002	5.169	•0039	31.4037
927	• 665	484.341	00	11.99	.7205	.1547	•1903	.0005	.0001	4.656	.0038	39.6389
<b>5</b> 28	•666	490.120	00	13.10	• 7655	.1807	.2116	.0002	.0002	4.236	.0037	50.7290
929	• 00 0	492.119	00	15.45	.8383	-2358	• 2585	.0004	.0000	3.555	.0035	64.0702
9 30	•600	490.642	00	17.57	.9055	.2923	-3000	.0001	.0003	3.098	•0032	68.6820
931	• 667	491.907	00	19.69	• 9446	• 3444	• 3358	0001	.0004	2.743	•0030	61.5997
932	•60 <i>1</i>	491.639	00	21.71	•9839	•3976	• 3536	.0008	.0000	2-475	•0028	54.1879
933	•605	489.727	00	14	0173	.0154	.0024	0001	.0008	-1.127	.0042	7.0272

#### TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	1631- 1	78 RUN=	84			BODY AX	IS COEFFICIEN	ITS			PRESS-COEF	
PGINT	MACH	۵	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF		CAB	CAC
947	.225	72.741	00	04	0162	.0128	-0000	.0007	.0001			.0000
948	.225	12.841	00	•96	•047♂	.0134	.0003	.0008	0002	•	0034 0	.0000
949	.225	72.841	00	1.90	.1115	.0112	.0003	.0010	0002	• 1	0034 0	.0000
950	.224	72.253	00	2.93	.1929	•0086	.0002	.0013	.0001	•	0034 0	.0000
951	.224	72.255	00	3.93	.2577	.0045	.0002	.0008	.0003		0034 0	.0000
952	.224	72.157	00	4.92	.3068	0021	.0009	.0008	0003		0034 0	.0000
953	•224	72.062	•00	5.97	.3736	0082	.0026	.0002	0017	- 0	0034 0	.0000
954	.224	72.071	00	7.00	.4518	0109	.0026	.0004	0013		0034 0	.0000
955	.224	72.082	00	8.05	.5119	0123	.0007	.0008	.0003		0035 0	.0000
956	224	72.101	00	9.10	.6059	0097	.0032	.0015	0028			.0000
957	•224	72.115	00	10.23	.6339	0091	.0028	.0016	0030			.0000
958	•224	72.131	00	11.22	.6757	0071	0012	.0006	0004			.0000
959	.224	72.148	00	12.39	.7366	0098	0001	.0007	0021			.0000
960	•225	72.878	•00	14.50	•8502	0105	0001	•0003	0031			.0000
961	•223	72.224	•00	16.01	.8996	0127	•0000	•0004	0040			.0000
962		71.481	•00	18.62	•9995	0149	.0000	0001	0050	-		.0000
	•223	71.533	•00	20.62	1.0841	0121	0001	.0001	0056			.0000
963	•223		•00	20.62	1.0605	0129	0001	.0001	0055			.0000
964	•224	72.021				.0158	•0000	.0007	0002			.0000
965	-224	71.958	00	03	0006	•0136	•0000	•0007	•0002	• '		•0000
	TEST= 7	78 KUN=	84									
						ILITY AXIS					PRESS.COEF	
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
947	-225	72.741	00	04	0162	<b>-</b> 0128	0070	.0000	-0007	-1.266	.0034	•603
948	• 225	72.841	00	• 96	•0476	.0142	.0005	.0003	•0008	3.350	•0034	1.416
949	<b>~225</b>	72.841	00	1.90	.1110	.0149	.0079	.0003	.0010	7.468	•0034	2.086
950	.224	72.253	00	2.93								
,,,		14.4233	00		•1922	.0184	.0103	.0003	.0013	10.446	-0034	1.460
951	-224	72.255	00	3.93	• 1922 • 2568	.0221	.0122		.0007	11.629	.0034	1.460 1.010
								.0003		11.629 12.662	•0034 •0034	1.460 1.010 .790
951	-224	72.255	00	3.93	. 2568	.0221	.0122	.0003	.0007 .0008 0001	11.629 12.662 12.140	•0034 •0034 •0034	1.460 1.010 .790 1.537
951 952	•224 •224	72•255 72•157	00 00	3.93 4.92	• 2568 • 3058	.0221 .0242	.0122 .0191	.0003 .0002 .0009	.0007 .0008 0001 .0001	11.629 12.662 12.140 10.152	.0034 .0034 .0034 .0034	1.460 1.010 .790 1.537 3.843
951 952 953	•224 •224 •224	72.255 72.157 72.062	00 00 .00	3.93 4.92 5.97	• 2568 • 3058 • 3724	.0221 .0242 .0307	.0122 .0191 .0216	.0003 .0002 .0009 .0026	.0007 .0008 0001 .0001	11.629 12.662 12.140 10.152 8.543	•0034 •0034 •0034	1.460 1.010 .790 1.537 3.843 5.490
951 952 953 954	•224 •224 •224 •224	72.255 72.157 72.062 72.071	00 00 .00 00	3.93 4.92 5.97 7.00	• 2568 • 3058 • 3724 • 4497	.0221 .0242 .0307 .0443	.0122 .0191 .0216 .0181	.0003 .0002 .0009 .0026	.0007 .0008 0001 .0001 .0007	11.629 12.662 12.140 10.152 8.543 6.954	.0034 .0034 .0034 .0034 .0034	1.460 1.010 .790 1.537 3.843 5.490 9.201
951 952 953 954 955	•224 •224 •224 •224 •224	72.255 72.157 72.062 72.071 72.082	00 00 00 00	3.93 4.92 5.97 7.00 8.05	.2568 .3058 .3724 .4497 .5085	.0221 .0242 .0307 .0443 .0595	.0122 .0191 .0216 .0181 .0247	.0003 .0002 .0009 .0026 .0026	.0007 .0008 0001 .0001	11.629 12.662 12.140 10.152 8.543 6.954 6.036	.0034 .0034 .0034 .0034	1.460 1.010 .790 1.537 3.843 5.490 9.201
951 952 953 954 955 956	•224 •224 •224 •224 •224 •224	72.255 72.157 72.062 72.071 72.082 72.101	00 00 00 00 00	3.93 4.92 5.97 7.00 8.05 9.10	. 2568 . 3058 . 3724 . 4497 . 5085 . 5998	.0221 .0242 .0307 .0443 .0595	.0122 .0191 .0216 .0181 .0247 .0677	.0003 .0002 .0009 .0026 .0026 .0008	.0007 .0008 0001 .0001 .0007 .0010 .0011	11.629 12.662 12.140 10.152 8.543 6.954 6.036 5.336	.0034 .0034 .0034 .0034 .0034 .0032	1.460 1.010 .790 1.537 3.843 5.490 9.201 11.924
951 952 953 954 955 956 957	•224 •224 •224 •224 •224 •224	72.255 72.157 72.062 72.071 72.082 72.101 72.115	00 00 00 00 00 00	3.93 4.92 5.97 7.00 8.05 9.10 10.23	.2568 .3058 .3724 .4497 .5085 .5998	.0221 .0242 .0307 .0443 .0595 .0862 .1036	.0122 .0191 .0216 .0181 .0247 .0677	.0003 .0002 .0009 .0026 .0026 .0008 .0034	.0007 .0008 0001 .0001 .0007 .0010	11.629 12.662 12.140 10.152 8.543 6.954 6.036	.0034 .0034 .0034 .0034 .0034 .0034	1.460 1.010 .790 1.537 3.843 5.490 9.201 11.924 12.473
951 952 953 954 955 956 957 958	.224 .224 .224 .224 .224 .224 .224 .224	72.255 72.157 72.062 72.071 72.082 72.101 72.115 72.131	00 00 00 00 00 00	3.93 4.92 5.97 7.00 8.05 9.10 10.23 11.22	.2568 .3058 .3724 .4497 .5085 .5998 .6255	.0221 .0242 .0307 .0443 .0595 .0862 .1036	.0122 .0191 .0216 .0181 .0247 .0677 .0903 .1299	.0003 .0002 .0009 .0026 .0026 .0008 .0034 .0031	.0007 .0008 0001 .0001 .0007 .0010 .0011	11.629 12.662 12.140 10.152 8.543 6.954 6.036 5.336	.0034 .0034 .0034 .0034 .0034 .0032	1.460 1.010 .790 1.537 3.843 5.490 9.201 11.924 12.473
951 952 953 954 955 956 957 958 959	.224 .224 .224 .224 .224 .224 .224 .224	72.255 72.157 72.062 72.071 72.082 72.101 72.115 72.131 72.148	00 00 00 00 00 00 00	3.93 4.92 5.97 7.00 8.05 9.10 10.23 11.22 12.39	.2568 .3058 .3724 .4497 .5085 .5998 .6255 .6042	.0221 .0242 .0307 .0443 .0595 .0862 .1036 .1245	.0122 .0191 .0216 .0181 .0247 .0677 .0903 .1299	.0003 .0002 .0009 .0026 .0026 .0008 .0034 .0031	.0007 .0008 0001 .0001 .0007 .0010 .0011 .0008	11.629 12.662 12.140 10.152 8.543 6.954 6.036 5.336 4.859	.0034 .0034 .0034 .0034 .0034 .0034 .0032 .0032	1.460 1.010 .790 1.537 3.843 5.490 9.201 11.924 12.473 13.439
951 952 953 954 955 956 957 958 959	.224 .224 .224 .224 .224 .224 .224 .224	72.255 72.157 72.062 72.071 72.082 72.101 72.115 72.131 72.134 72.148	00 00 00 00 00 00 00 00	3.93 4.92 5.97 7.00 8.05 9.10 10.23 11.22 12.39 14.50	.2568 .3058 .3724 .4447 .5085 .5998 .6255 .6042 .7215	.0221 .0242 .0307 .0443 .0595 .0862 .1036 .1245 .1485 .2027	.0122 .0191 .0216 .0181 .0247 .0677 .0903 .1299 .1652 .2152	.0003 .0002 .0009 .0026 .0026 .0008 .0034 .0031 -00011	.0007 .0008 0001 .0007 .0010 .0011 .0008 .0007	11.629 12.662 12.140 10.152 8.543 6.954 6.036 5.336 4.859 4.073	.0034 .0034 .0034 .0034 .0034 .0032 .0032 .0032	1.460 1.010 .790 1.537 3.843 5.490 9.201 11.924 12.473 13.439 19.435 26.846
951 952 953 954 955 956 957 958 959 960	. 224 . 224 . 224 . 224 . 224 . 224 . 224 . 224 . 225 . 224	72.255 72.157 72.062 72.071 72.082 72.101 72.115 72.131 72.148 72.878 72.224	00 00 00 00 00 00 00 00	3.93 4.92 5.97 7.00 8.05 9.10 10.23 11.22 12.39 14.50 16.61	.2568 .3058 .3724 .4497 .5085 .5998 .6255 .6042 .7215 .8257	.0221 .0242 .0307 .0443 .0595 .0862 .1036 .1245 .1485 .2027 .2450	.0122 .0191 .0216 .0181 .0247 .0677 .0903 .1299 .1652 .2152	.0003 .0002 .0009 .0026 .0026 .0008 .0031 0011 .0000 0000	.0007 .0008 0001 .0001 .0007 .0010 .0011 .0008 .0007 .0003	11.629 12.662 12.140 10.152 8.543 6.954 6.036 5.336 4.859 4.073 3.534	.0034 .0034 .0034 .0034 .0034 .0032 .0032 .0032 .0032	1.460 1.010 .790 1.537 3.843 5.490 9.201 11.924 12.473 13.439 19.435 26.846 12.737

. 3623

.0158

. 9968

-.0006

.3279

.0049

-.0001

.0000

.0001

.0007

2.751

-.039

.0016

.0037

30.0860

-8125

.00 20.67

-.03

-.00

72.021

71.958

-224

-224

964

965

# TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 RUN= 8	5									
						BODY AXI:	S CUEFFICIEN	TS		BODY	PRESS-COEF	F
POINT	MACH	ð	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	C	AB	CAC
979	• 455	267.071	00	.14	0089	.0147	.0006	.0007	0007	.0	038 0	.0000
980	455	266.981	00	1.20	.0649	.0140	.0003	•0009	0003	.0		.0000
981	.455	267.076	00	2.16	.1348	.0119	.0002	.0008	0001	• 0	038 0	.0000
982	.455	267.713	00	3.21	.1955	.0081	•0004	.0007	0002			.0000
983	•455	267.085	00	4.21	.2701	.0029	.0006	.0008	0003			•0000
984	.455	267.089	00	5.25	.3272	0043	.0007	.0003	0003			•0000
985	.455	267.108	.00	6.37	.4021	0110	.0016	0003	.0018			•0000
986	•455	267.060	00	7.43	.4840	0137	.0012	0002	.0024			•0000
987	.455	267.758	00	8.49	.5512	0122	.0023	.0011	0016			•0000
988	456	267.923	00	9.61	.6115	0102	•0051	.0016	0047			•0000
989	•455	267.380	00	10.75	.6778	0065	.0021	•0008	0006			.0000
990	•455	266.907	00	11.79	.7193	0059	.0003	.0004	.0028			•0000
991	456	268-254	00	12.93	.7616	0064	.0001	•0006	.0024			•0000
992	• 456	268 - 345	00	15.14	.8626	0067	•0002	•0002	.0013			•0000
993	•458	269.900	00	17.31	.9449	0067	.0001	.0002	.0030			•0000
994	•456	268.736	00	19.35	1.0191	0063	.0002	.0003	.0022			•0000
995	457	269.048	00	21.40	1.0953	0056	÷0000	.0003	.0013			•0000
996	456	267.885	00	.11	0131	•0144	.0006	.0007	0007			•0000
	TEST= 7	73 RUN=	85		STAB	ILITY AXIS C	OFFFICIENTS			STAB	.PRESS.COEF	·F
POINT	MACH	ů,	BETA	ALPHA	CL	CD	CPM	CLS	CINS	L/D	CDB	PB-1
979	455	267.071	00	•14	0089	.0147	.0040	-0006	.0007	606	.0038	3.1952
980	• 455	266.981	00	1.20	.0646	.0153	.0082	.0003	•0009	4.209	•0038	3.2940
981	•455	267.076	00	2.16	.1342	.0170	.0109	.0002	.0008	7.885	.0038	3.5246
982	•455	267.713	00	3.21	.1948	.0191	.0147	•0005	.0007	10.209	.0038	3.4697
983	• 455	267.085	00	4.21	.2091	.0227	.0237	•0006	.0007	11.847	.0038	3.3050
984	.455	267.089	00	5.25	.3262	.0256	.0259	•0008	.0003	12.720	.0038	3.4697
985	• 455	267.108	.00	6.37	.4008	.0337	.0260	.0016	0005	11.903	.0038	5.2375
986	•455	267.060	00	7.43	.4818	.0490	.0274	.0012	0003	9.833	.0037	9.0036
987	.455	267.758	00	8.49	•5469	.0693	.0482	.0025	.0007	7.890	.0036	15.6799
988	.456	201.923	00	9.61	•6046	.0921	.0799	.0052	.0007	6.568	.0036	19.1387
989	.455	267-380	00	10.75	.6672	.1200	.1322	.0022	•0004	5.558	-0035	36.6742
990	.455	266.907	00	11.79	.7054	.1412	.1685	•0004	•0004	4.994	•0034	24.0469
991	.450	268.254	00	12.93	.7437	.1641	.1918	•0002	•0004	4.533	.0033	30.8546
991	• 456 • 456	268.345	00	15.14	•8344	.2189	• 2405	•0003	•0003	3.812	•0030	48.0937
992	• 458	269.900	00	17.31	.9041	.2748	. 2869	•0001	•0002	3.290	•0027	51.7172
993	• 456	268.736	00	19.35	.9636	.3317	.3264	.0003	•0002	2.905	•0025	52.4858
995	• 45 0 • 45 7	269.048	00	21.40	1.0219	.3944	.3736	.0001	•0002	2.591	•0023	51.9368
995	• 42 /					• J744	• 3 ( 30	* OOOI	• 0002	C = 37 I	•0022	<b>フェ・ブラロ</b> の
	. 456	267.885	00	-11	0132	.0143	.0023	.0006	.0007	918	.0038	3.4038

TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 KUN=	86									
							IS COEFFICIE				PRESS.COE	
TAIOS	MACH	۵	RETA	ALPHA	CNF	CAF	CFB	CNB	CSF		CAB	CAC
37	-801	645.170	01	24	0064	.0170	0008	.0007	•0026			0.0000
38	. 883	690.956	01	•95	.1198	.0159	0003	.0007	.0026			0.0000
39	.883	697.290	01	3.40	.3967	• 0086	0003	.0007	.0027	•	0054	0.0000
40	-882	696.642	01	4.63	.5168	.0081	.0002	.0012	.0019	•	0053	0.0000
41	.834	698.284	01	5.78	.6066	.0093	•0006	•0009	.0019	•	0053	0.0000
42	• 885	699.065	01	0.98	•6805	•0115	0028	.0004	.0031		0053	0.0000
43	• 833	697.134	01	8.16	.7415	.0126	.0004	.0006	.0024		0052	0.0000
44	-885	698.843	01	9.27	.7648	.0159	.0028	.0007	.0024	•	0051	0.0000
45	.879	694.126	01	2.11	•2499	.0115	0004	.0007	.0031	•	0053	0.0000
46	-883	090.861	01	32	0031	.0173	0006	.0008	•0034	• 1	0054	0.0000
	TE5T= 7	78 RUN=	86									
_							COEFFICIENTS				.PRESS.COE	
POINT	MALH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
37	•891	695.176	01	24	0064	.0171	.0058	0008	.0007	373	•0054	10.3887
36	.863	696.956	01	•95	.1195	.0179	•0062	0002	.0007	6.669	.0054	12.2953
39	•883	697.290	01	3.40	• 3955	.0322	0069	0002	.0007	12.295	.0054	23.3444
40	-882	696.642	01	4.63	.5144	.0497	0138	•0003	.0012	10.345	•0052	20.4111
41	•884	598.284	01	5.78	•6026	.0703	0078	.0007	•0009	8.570	•0053	39.3555
42	• ४४5	699.065	01	6.98	.6741	.0941	.0129	0027	.0007	7.160	•0052	78.8332
43	.883	697.134	01	8.16	.7322	.1176	.0366	.0005	.0005	6.224	.0051	99.9165
44	• 885	698.843	01	9.27	.7523	.1389	.0670	•0029	.0002	5.415	.0051	134.9331
45	.879	694.126	01	2.11	. 2493	.0207	.0058	0003	.0007	12.046	.0053	17.9666
46	•843	690.881	01	32	0030	.0173	.0062	0006	.0008	175	•0054	10.4865

TEST= 770 RUN= 87

### TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	76 KUN= 8	8 7									
						BODY AXI	S CUEFFICIEN	TS		BODY	PRESS-COE	F
PUINT	MACH	J	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	(	CAB	CAC
60	.759	593.553	01	.03	0051	.0165	0006	.0008	.0015	.(	0046	0.000
61	.758	593.127	01	2.33	.2006	.0115	0008	.0009	.0017	•(	0046	0.000
62	.759	593.641	01	2.26	.1966	.0117	0007	.0008	.0017	.(	0046	0.0000
63	.770	594.770	01	3.52	.2974	.0053	0002	.0007	.0019	. (	0046	0.0000
64	• 709		00	4.61	.3969	0023	0000	.0007	.0011	. (	0046	0.0000
65	.769	593.532	01	5.83	•5058	0078	.0004	.0014	0000	. (	0046	0.0000
66	.770	594.864	01	7.05	•5921	0090	.0012	.0012	.0010			0.0000
67	.770	594.711	00	8.12	.6508	0051	0002	.0005	.0013			0.0000
68	.772	596.530	01	9.29	.6918	.0010	0001	.0006	.0025			0.0000
69	.771	595.984	01	10.42	.7273	•0059	.0038	.0010	.0008			0.0000
70	.712	596.772	01	11.51	.7819	.0090	.0119	.0016	.0003			0.0000
71	.7/1	596.071	01	12.62	.8221	.0112	.0138	.0015	.0017			0.0000
12	.712		00	13.73	.8108	.0172	.0000	.0004	.0014			0.0000
73	.772	590.527	00	15.93	.8708	.0202	0005	.0005	.0024			0.0000
74	.773	597.142	00	18.14	•9258	.0210	0009	•0006	.0012			0.0000
75	•110	594.942	01	1.10	.0898	.0151	0005	•0008	.0021			0.0000
76	.758	592.441	01	06	0052	.0164	0006	•0008	.0015			0.0000
77		593.714	01	2.25	.1931	.0114	0001	•0008	.0024			0.0000
	TEST= 7	78 KUN=	87									
	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		· ·		STAR	ILITY AXIS C	DEFEICIENTS			STAB	PRESS.COE	FF
POINT	MACH	ų.	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
60	.709	593.253	01	•03	0051	.0165	•0057	0006	.0008	312	•0046	12.2953
61	.768	593.127	01	2.33	.1999	.0196	.0147	0008	.0009	10.178	.0046	9.1665
62	. 709	593.641	01	2.26	.1960	.0194	.0142	0007	•0009	10.105	.0046	8.7754
63	.770	594.770	01	3.52	. 2965	.0236	.0192	0001	.0007	12.584	.0046	8.8976
64	.709	593.925	00	4.61	. 3958	.0296	.0247	.0000	.0007	13.376	.0046	10.4865
65	.769	593.532	01	5.83	•5040	.0436	.0319	•0006	.0014	11.556	• 0046	16.3530
66	.770	594.864	01	7.05	.5887	.0638	.0442	.0013	.0010	9.234	.0045	29.5166
67	.770	594.711	00	8.12	.6449	.0869	.0708	0001	-0005	7.423	.0045	68.3221
68	.772	590.530	01	9.29	• 6825	.1126	.1023	0000	.0006	6.059	.0044	71.6221
69	.771	595.984	01	10.42	.7143	.1374	.1172	.0039	.0003	5.199	.0044	112.7498
70	•772	590.172	01	11.51	.7644	.1648	.1175	•0120	0008	4.638	•0044	92.5832
71	.771	596.071	01	12.62	. 7998	.1905	.1287	.0138	0015	4-198	•0042	99.1832
72	•772	596.453	00	13.73	.7836	.2091	-1648	.0001	.0004	3.747	.0042	112.5665
73	.772	596.527	00	15.93	.8318	. 2584	.1800	0004	•0006	3.219	.0040	73.8832
74	.773	597.742	00	18.14	.8733	.3082	.1827	0007	.0008	2.833	.0038	77.7332
75	.773	594.942	01	1.10	•0895	.0168	.0100	0005	.0008	5.326	.0046	9.2643
76	.758	592.441	01	06	0052	.0164	.0064	0006	.0008	314	.0046	8.7510
77	.759	593.714	01	2.25	.1925	.0189	.0131	0001	.0008	10.165	.0046	9.4354
												· - · - <del>-</del> ·

# TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

	TEST= 7	78 KUN= 8	38								
						BODY AXI	S COEFFICIEN	rs		BODY PRESS.	COEFF
POINT	MACH	٥	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
92	.717	541.400	01	• 05	0121	.0161	0007	•0009	.0018	• 0043	0.0000
93	.717	541.406	01	1.17	.0859	.0153	0005	.0008	.0024	.0044	0.0000
94	.717	542.190	01	2.29	.1753	-0115	0002	*0008	.0029	.0044	0.0000
95	.717	541.668	01	3.40	.2813	.0062	0008	•0008	•0028	•0044	0.0000
96	.717	541.687	01	4.59	.3643	0016	0008	.0007	.0022	.0044	0.0000
97	.716	541.293	01	5.70	.4647	0081	0005	.0009	.0014	.0043	0.0000
98	.716	541.111	01	6.87	.5480	0060	.0004	.0011	.0011	•0043	0.0000
99	.718	542.826	01	8.03	.6083	0002	.0028	.0012	.0019	.0043	0.0000
100	.717	541.849	01	9.18	.0751	.0018	.0098	.0020	•0002	.0043	0.0000
101	.718	542.169	01	10.32	.7221	.0038	.0116	.0021	.0005	.0042	0.0000
102	.719	543.513	01	11.39	.7720	.0065	.0135	•0020	.0008	.0042	0.0000
103	.718	542.670	01	12.43	.7739	.0128	.0008	.0007	.0033	.0042	0.0000
104	.718	542.997	00	13.62	.7930	.0147	0005	.0004	.0027	.0041	0.0000
105	.720	544.530	00	15.78	.8528	.0182	0007	• 00 0 5	.0022	.0041	0.0000
106	.720	544.629	01	17.92	.9211	.0193	0007	.0007	.0030	.0039	0.0000
107	.721	545.405	01	20.03	.9660	.0211	0005	.0013	.0001	-0032	0.0000
108	.721	545.895	01	22.09	1.0443	.0198	0007	.0011	0002	• 0026	0.0000
109	.718	542.155	01	5.59	•4659	6081	0003	.0011	.0038	.0044	0.0000

	TEST= 7	78 RUN=	88									
					STA	BILITY AXIS		i			.PRESS.COEF	
POINT	MACH	J	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
92	.717	541.400	01	• 05	0121	.0161	• 0056	6007	.0009	<b></b> 752	.0043	7.9321
93	.717	541.406	01	1.17	•0856	.0170	.0103	0005	.0008	5.027	•0044	8.0299
94	.717	542.190	01	2.29	.1747	.0185	.0142	0001	.0008	9.432	•0044	8.1887
95	.717	541.663	01	3.40	· 2805	.0229	.0206	0008	.0008	12.267	.0044	8.3232
96	.717	541.687	01	4.59	.3633	.0276	.0260	0007	.0008	13.164	.0044	8.5554
97	.710	541.293	01	5.70	•4632	.0381	.0326	0004	.0010	12.171	.0043	10.7798
98	-716	541.111	01	6.87	• 5448	•0596	.0471	.0006	.0010	9.136	.0043	38.0722
99	.718	542.826	01	8.03	•6024	.0848	.0735	•0029	•0008	7.105	.0043	52.0666
100	.717	541.849	01	9.18	•666l	-1094	.0899	.0100	.0004	6.089	•0042	57.9332
101	-718	542.169	01	10.32	.7098	.1331	.1034	.0118	.0000	5.333	• 0042	122.8331
102	.719	543.513	01	11.39	.7556	.1587	.1186	.0136	0007	4.759	.0041	92.9498
103	.718	542.670	01	12.43	.7530	.1791	.1569	.0009	•0005	4.205	.0041	131.5109
104	.718	542.997	00	13.62	.7672	.2010	.1709	0004	.0005	3.818	•0040	77.6110
105	.720	544.530	00	15.78	.8157	.2495	.1852	0005	.0006	3.270	.0039	70.0332
106	.720	544.629	01	17.92	.8705	.3018	.1937	0005	•0009	2.884	.0037	69.2999
107	.721	545.405	01	20.03	•9003	.3507	.1841	0000	.0014	2.567	.0030	82.3165
108	.721	545.895	01	22.09	.9002	.4112	.1912	0002	.0013	2.335	.0024	92.5832
109	-718	542.155	01	5.59	• 4645	.0373	•0328	0002	.0011	12.452	-0044	10.2909

# TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

							S COEFFICIEN	rs		BODY PRESS.	COESF
POINT	MACH	Ú	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	CAB	CAC
123	-664	487.154	00	04	0108	-0165	0007	.0008	.0020	.0041	0.000
124	-665	487.720	01	1.08	.0804	.0155	0001	.0007	.0023	•0042	0.000
125	•662	484.982	00	2.22	.1697	.0122	0006	.0007	.0023	.0042	0.000
126	-663	486-119	01	3.37	-2641	.0063	0004	.0007	.0030	.0042	0.000
127	-664	486.779	00	4-41	•3540	0010	.0000	•0007	.0020	.0042	0.000
128	-665	487.378	00	5.49	•4411	0083	.0002	-0006	.0027	.0042	0.000
129	•665	487.620	01	6.73	.5398	0071	.0006	.0011	.0016	.0041	0.000
130	•665	487.799	01	7.88	.5952	0031	•0038	.0015	.0009	.0041	0.000
131	•665	487.498	01	8.96	.6549	0003	.0088	.0020	.0000	.0041	0.000
132	-665	488.160	01	10.04	.7050	.0019	.0119	•0022	.0009	•0040	0.000
133	.666	488.378	01	11.16	.7599	.0043	.0139	•0020	.0014	.0040	0.000
134	•664	487.143	00	12.20	•7629	.0110	0002	•0004	.0026	•0039	0.000
135	.660	489.546	00	13.46	.7909	.0130	0006	.0003	.0025	.0039	0.000
136	.666	488.903	00	15.59	-8492	.0163	0007	.0005	.0019	.0038	0.000
137	•667	490.487	00	17.83	•9084	.0177	0009	•0005	•0029	.0037	0.000
138	•667	489.798	01	19.85	•9586	.0207	0007	-0011	.0013	•0031	0.000
139	-669	492.501	01	21.89	1.0299	.0199	0003	.0009	.0019	• 0025	0.000
140	•665	488.530	01	6.75	.5318	0073	-0006	1100.	.0016	.0041	0.000

	TEST= 7	78 KUN=	89									
					STAE	BILITY AXIS	COEFFICIENTS			STAB	PRESS.COEFF	:
POINT	MACH	Q	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
123	-664	487.154	00	04	0108	.0165	.0056	0007	.0008	656	.0041	6.3188
124	• 665	487.720	01	1.08	.0861	.0171	.0113	0001	.0007	5.021	.0042	6.8199
125	•662	484.982	00	2.22	.1691	.0187	.0138	0006	.0007	9.023	•0042	6.7710
126	• 663	486.119	01	3.37	. 2633	.0218	.0209	0004	.0007	12.059	.0042	6.5510
127	664	486.779	00	4-41	<b>.</b> 3531	.0263	• 0266	-0001	.0007	13.433	.0042	6.7710
128	- 665	487.378	00	5.49	•4399	•0339	.0338	•0003	•0006	12.963	.0041	7.1132
129	-665	487.620	01	6.73	.5370	•0562	.0464	-0007	.0010	9.552	.0041	25.3611
130	•665	487.799	01	7.88	•5900	•0785	.0668	•0039	.0010	7.512	.0041	39.9055
131	•665	487.498	01	8.96	.6470	•1017	.0860	•0090	.0006	6.360	•0040	48.3999
132	•605	488.166	01	10.04	•6939	.1249	-1015	-0121	.0001	5.557	.0039	61.2332
133	•666	488.378	01	11.16	• 7447	•1514	.1159	.0140	0007	4.920	•0039	76.6332
134	-664	487-143	00	12.20	<b>.</b> 7434	<ul><li>1720</li></ul>	.1579	0001	.0005	4.322	.0038	78.9554
135	.666	487.546	00	13.46	•7662	• 1967	.1705	0005	.0005	3.894	.0038	73.1499
136	•066	488.903	00	15.59	.8136	.2439	-1883	0006	.0007	3.336	.0037	71.4999
137	•667	490.487	00	17.83	.8594	• 2949	.1999	0007	.0008	2.914	.0035	66.9165
138	•607	489.798	01	19.85	.8946	• 3449	.1903	0003	.0013	2.594	•0029	80.6665
139	.664	492.501	01	21.89	.9482	• 4026	.1944	•0000	.0009	2.355	.0023	91.2998
140	-665	488.530	01	6.75	•5290	• 0552	• 0455	-0007	.0010	9.587	.0041	24.1388

# TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

						RODA VXI	S COEFFICIEN	TS		BODY PRESS.	COEFF
POINT	MACH	7	BETA	ALPHA	CNF	CAF	CLB	CNB	CSF	ÇAB	CAC
154	-821	642.514	01	09	0068	.0165	0008	.0008	.0016	.0048	0.0000
155	-822	643.009	01	1.04	.0991	.0154	0008	.0007	•0022	• 0048	0.0000
156	.820	641.678	01	2.18	.2073	.0111	0004	•0007	.0024	•0048	0.0000
157	.822	643.668	01	3.40	.3251	.0042	0002	.0007	.0016	.0047	0.0000
158	.822	643.248	01	4.57	•4363	0026	0003	.0008	•0022	.0047	0.0000
159	•822	043.042	01	5.19	•5555	0062	.0008	.0010	.0017	• 0047	0.0000
160	.823	044.562	01	7.02	.6510	0037	.0019	-0010	.0010	.0047	0.0000
161	.823	644.305	00	9.24	.7168	•0072	.0016	•0006	.0015	.0046	0.0000

	IEST= 7	78 RUN=	90									
					STA	BILITY AXIS	COEFFICIENTS			STAB	.PRESS.COEF	F
PUINT	MACH	ų.	BETA	ALPHA	CL	CD	CPM	CLS	CNS	L/D	CDB	PB-1
154	.821	642.514	01	09	0067	.0166	.0057	0008	.0008	408	•0048	9.5576
155	•822	643.009	01	1.04	.0988	.0172	.0085	0007	.0007	5.749	.0048	9.2887
156	.820	641.678	01	2.18	.2067	.0190	-0102	0004	.0007	10.869	•0048	9.5820
157	.822	643.008	01	3.40	.3243	.0235	•0150	0001	.0007	13.823	•0047	12.4909
158	-822	643.248	01	4.57	.4351	•0322	.0170	0003	.0008	13.514	.0047	16.1575
159	-822	043.042	01	5.79	• 5533	.0499	•0206	•0009	.0009	11.084	.0047	23.3444
160	.825	644.502	01	7.02	•6466	.0758	.0370	.0020	.0007	8.525	.0046	54.5110
161	.823	644.305	00	9.24	. 7063	.1222	.0980	.0017	.0003	5.782	.0046	100.6498

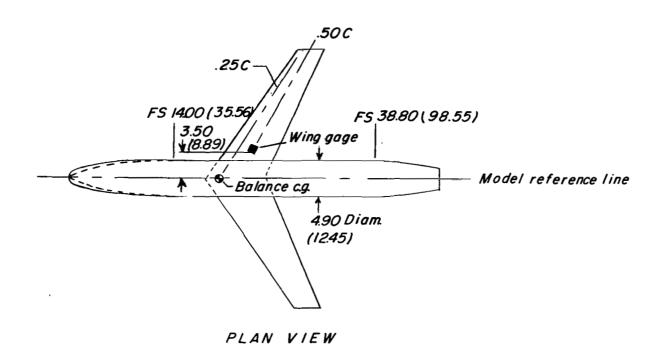
TABLE III. - BUFFET AND STATIC AERODYNAMIC RESULTS - Continued

## BODY AXIS COEFFICIENTS  ## BODY PRESS  ## CAB  ## CAF CLB CNB CSF CAB  ## CAB  ## CAF CLB CNB CSF CAB  ## CAB  ## CAF CLB CNB CSF CAB  ## CAB  ## CAB  ## CAF CLB CNB CSF  ## CAB  ## CAB	
175	OEFF
176	CAC
177	0.0000
178	0.0000
179	0.0000
180	0.0000
181	0.0000
182	0.0000
183	0.0000
184 .450 261.57300 10.77 .700400090001 .0003 .0016 .0035	0.0000
	0.0000
	0.0000
185 .45° 267.28° .00 13.02 .7866 .00310005 .0005 .0004 .0034	0.0000
186 .456 268.09200 17.33 .9165 .00960009 .0006 .0015 .0031	0.0000
187 .456 267.64400 21.26 1.0185 .01620008 .0009 .0010 .0025	0.0000
TEST= 778 RUN= 91	
STABILITY AXIS COEFFICIENTS STAB.PRESS.	COEFF
POINT MACH Q BETA ALPHA CL CD CPM CLS CNS L/D CC	
175 .450 268.14200 .000011 .0175 .00300004 .0008065 .00	
176 454 200.14900 1.09 .0637 .0174 .00710002 .0006 3.658 .00	
177 •456 207.41800 2.14 .1491 .0189 .01360005 0.005 7.901 .00	
178	
179 .456 207.33300 4.26 .3037 .0248 .02620001 .0007 12.266 .00	
180 -456 267.97100 5.36 .3848 .0291 .03060001 .0005 13.244 .00	
181 -456 267.98300 6.39 .4703 .0363 .03850003 .0006 12.959 .00	
182 .409 .0001 .0008 9.409 .00	37 13.8842
183 -450 207.49000 8.64 .6014 .0807 .0653 .0028 .0012 7.450 .00	
184 -450 261-57300 10-77 .6883 .1300 .12730000 .0003 5.294 .00	
185 •456 267•280 •00 13•02 •7657 •1803 •16450004 •0006 4•248 •00	
186	
187 -450 267.64400 21.26 .9433 .3843 .21220005 .0011 2.454 .00	33 55.1221

# TABLE III.- BUFFET AND STATIC AERODYNAMIC RESULTS - Concluded

## BODY AXIS COEFFICIENTS ## BODY PRESS-COEFF CAB	•
188	-
188     .223     71.565     .00     .05    0163     .0183    0004    0000     .0004     .0035     0.00       189     .224     72.254     .00     1.00     .0637     .0192    0000     .0002    0003     .0037     0.00       190     .224     72.254     .00     1.97     .1275     .0166     .0003     .0004    0011     .0037     0.00       191     .225     72.942     .00     2.97     .2054     .0116     .0002    0001    0016     .0036     0.00       192     .225     72.845     .00     3.98     .2838     .0067    0005     .0002    0016     .0036     0.00       193     .225     72.846     .00     4.98     .3468    0011    0002    0002     .0077     .0034     0.00       194     .226     73.538     .00     6.10     .4681    0101    0003     .0002     .0066     .0034     0.00       195     .226     73.542     .00     7.17     .4995    0163    0003     .0003     .0065     .0034     0.00	
189     .224     72.254     .00     1.00     .0637     .0192    0000     .0002    0003     .0037     0.00       190     .224     72.254     .00     1.97     .1275     .0166     .0003     .0004    0011     .0037     0.00       191     .225     72.942     .00     2.97     .2054     .0116     .0002    0001    0016     .0036     0.00       192     .225     72.845     .00     3.98     .2838     .0067    0005     .0002    0016     .0036     0.00       193     .225     72.846     .00     4.98     .3468    0011    0002    0002     .0077     .0034     0.00       194     .226     73.538     .00     6.10     .4681    0101    0003     .0002     .0066     .0034     0.00       195     .226     73.542     .00     7.17     .4995    0163    0003     .0003     .0065     .0034     0.00	
191	
192	
193	
194 .226 73.538 .00 6.10 .468101010003 .0002 .0066 .0034 0.00 195 .226 73.542 .00 7.17 .499501630003 .0003 .0065 .0034 0.00	
195 .226 73.542 .00 7.17 .499501630003 .0003 .0065 .0034 0.00	
196 .225 72.871 .00 8.20 .56830124 .0000 .00030040 .0034 0.00	
197 .225 72.912 .00 10.27 .723200410001 .0003 .0036 .0034 0.00	
198 •225 72.848 •00 12.50 •7849 -•0031 -•0002 •0005 •0023 •0032 0•00	
199 .224 72.201 .00 14.73 .8486 .002000120000 .0023 .0030 0.00	
200 .223 71.550 .00 16.67 .9143 .00510022 .0002 .0025 .0029 0.00	
201 .221 70.264 .00 20.75 1.0665 .00920014 .0006 .0000 .0022 0.00	00
TEST= 778 KUN= 92 STABILITY AXIS COEFFICIENTS STAB.PRESS.COEFF	
	PB-1
pagni nach d bein nerna	.6722
TO THE STATE OF TH	1.0755
TOY THE THE TAX TO THE	1.1733
The state of the s	1.0022
1/2 4000 1007/0 400	1.0633
1/2 4227 121012	1.3078
1/3	1.2589
177	2.7011
175 4220 15572	11.4153
170 12012 12012	21.2055
131 1223 124312 100 10011	21.6944
170	23.8333
1))	22.2444
200	18.7000

TEST= 778 RUN= 92



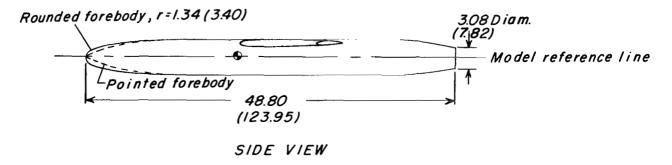


Figure 1.- Sketches of typical buffet model. All linear dimensions are in inches (cm).

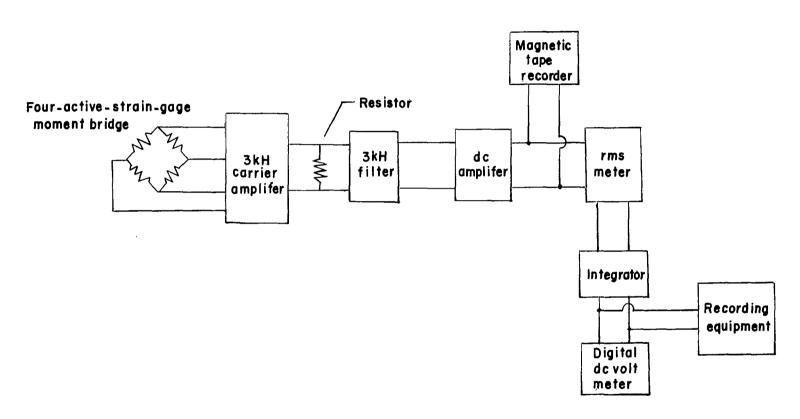
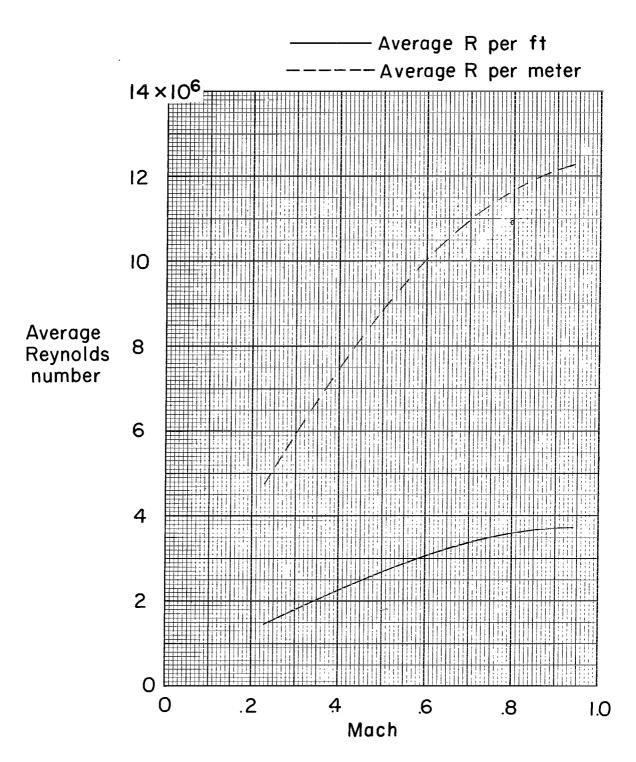
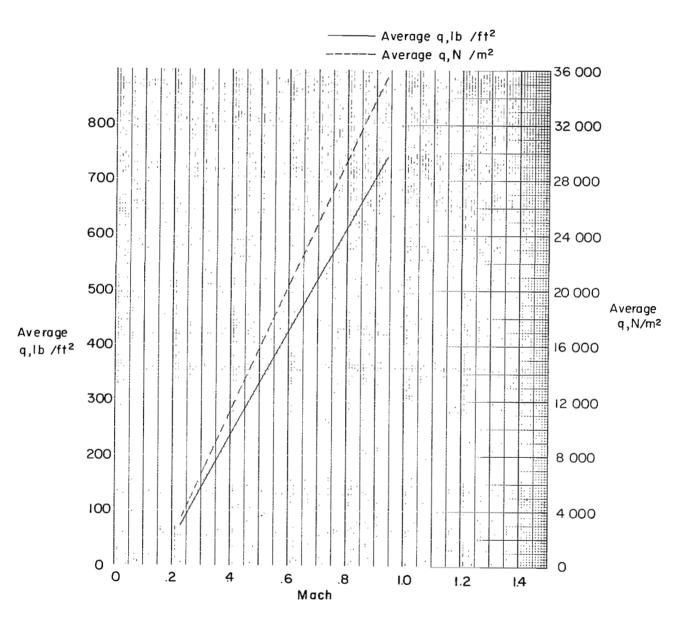


Figure 2.- Schematic drawing of wing-bending-gage electronic equipment and wiring arrangement.



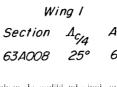
(a) Variation of Reynolds number with Mach number.

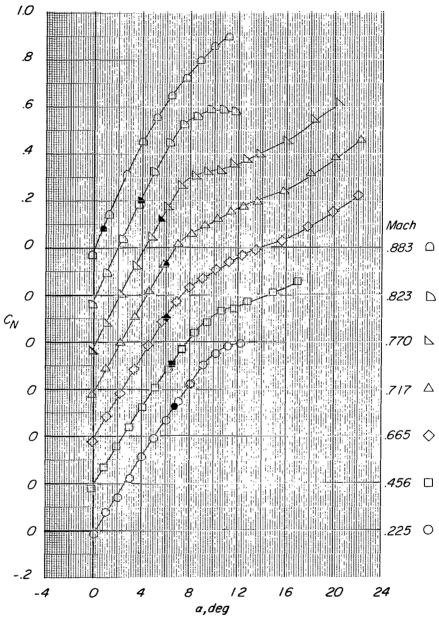
Figure 3.- Average test conditions.



(b) Variation of dynamic pressure  $\, {\bf q} \,$  with Mach number.

Figure 3.- Concluded.



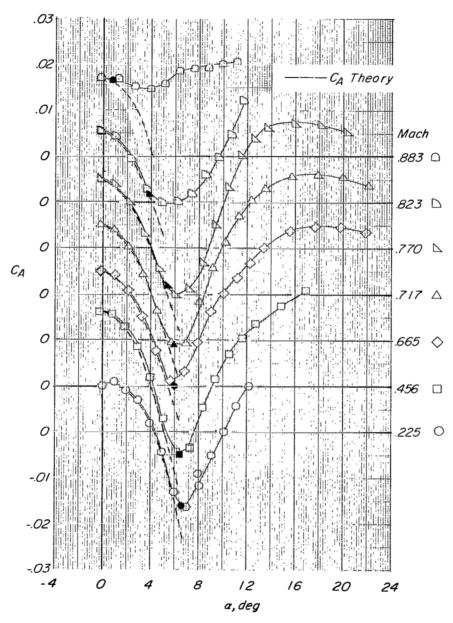


(a)  $C_N$  versus  $\alpha$ .

Figure 4.- Static longitudinal aerodynamic and buffet characteristics of the wing 1 configuration at Mach numbers from 0.23 to 0.88.

Rounded forebody; transition grit on. (Solid symbols indicate buffet onset.)





(b)  $C_{\mbox{\scriptsize A}}$  versus  $\alpha$ .

Figure 4.- Continued.

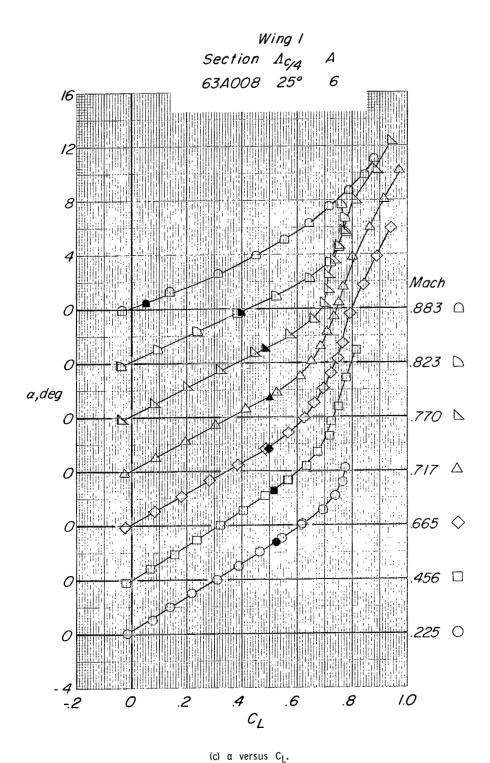
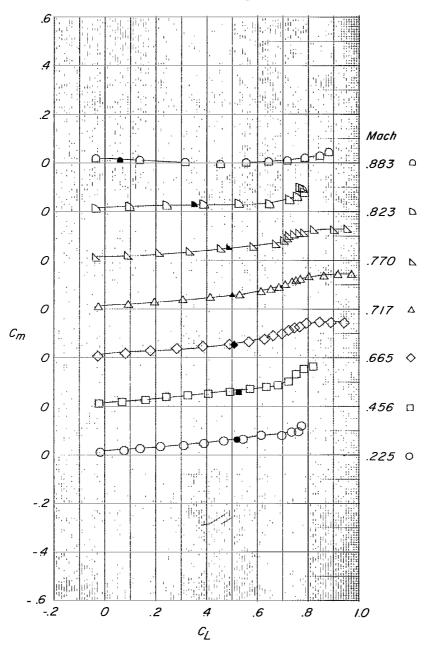
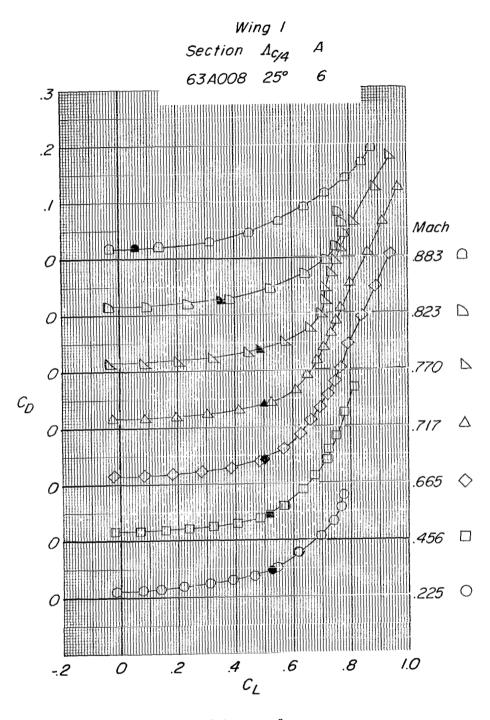


Figure 4.- Continued.

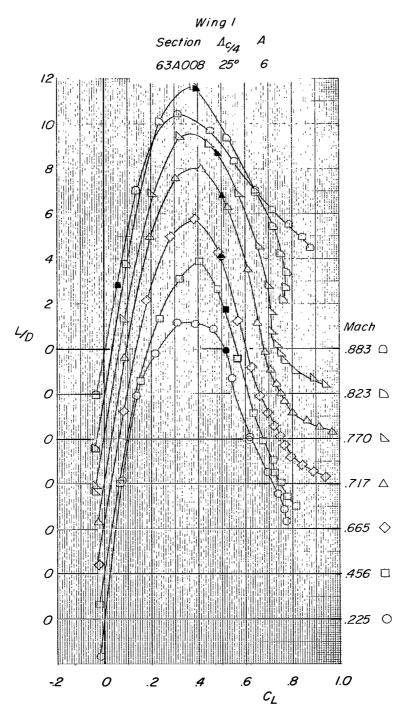
Wing I Section A<sub>C/4</sub> A 63A008 25° 6



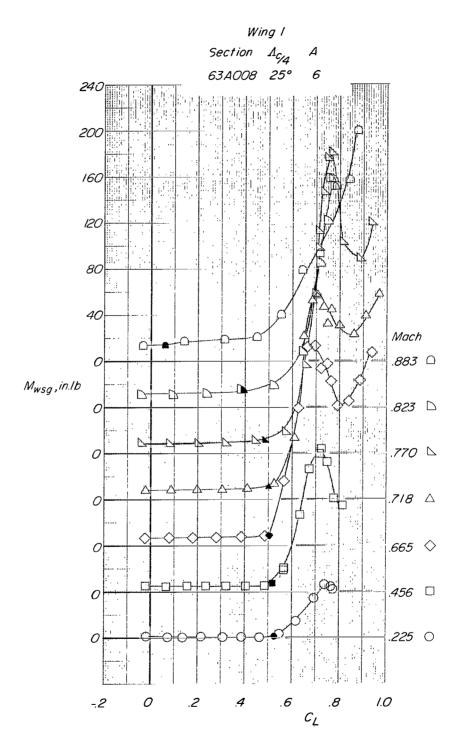
(d)  $C_{\text{m}}$  versus  $C_{\text{L}}$ . Figure 4.- Continued.



(e)  $C_D$  versus  $C_L$ . Figure 4.- Continued.



(f) L/D versus  $C_L$ . Figure 4.- Continued.



(g)  $M_{WSg}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 4.- Concluded.

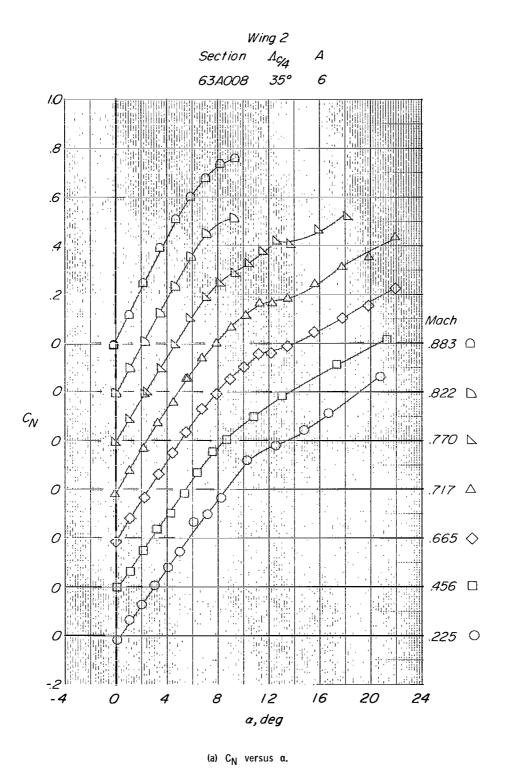
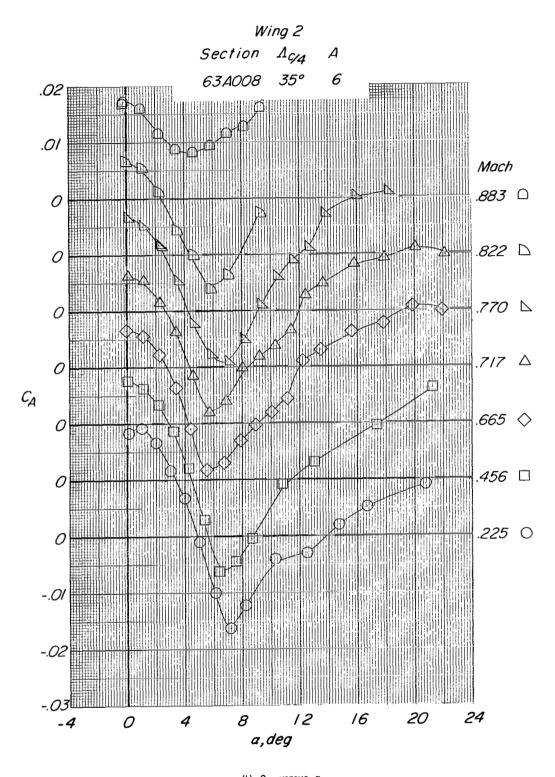


Figure 5.- Static longitudinal aerodynamic and buffet characteristics of the wing 2 configuration at Mach numbers from 0.23 to 0.88. Rounded forebody; transition grit on.



(b) C<sub>A</sub> versus α.Figure 5.- Continued.

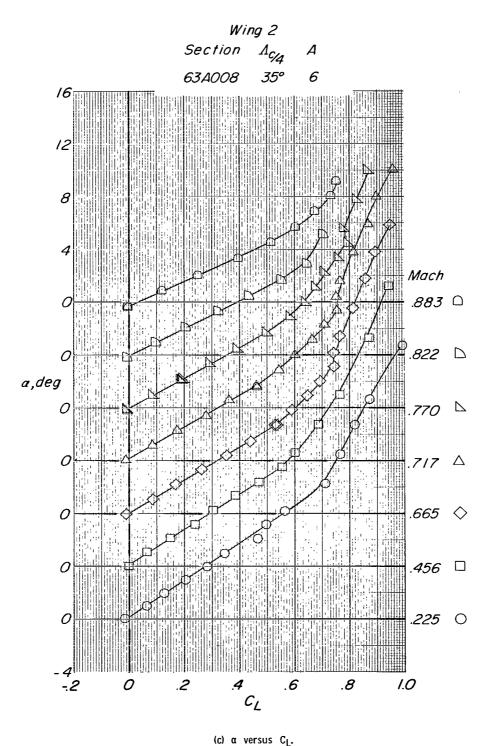
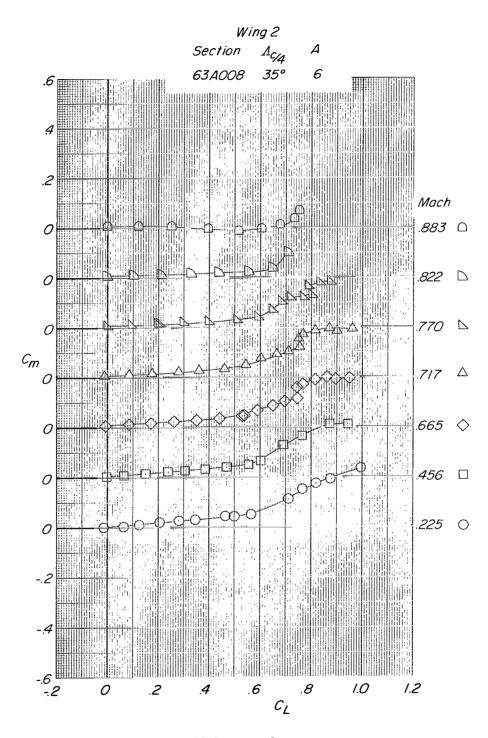


Figure 5.- Continued.



(d)  $C_{\rm m}$  versus  $C_{\rm L}$ . Figure 5.- Continued.

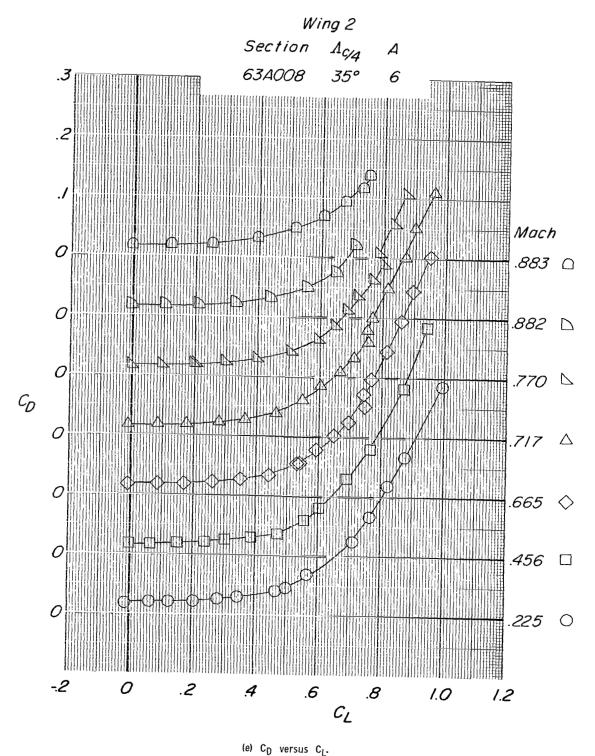
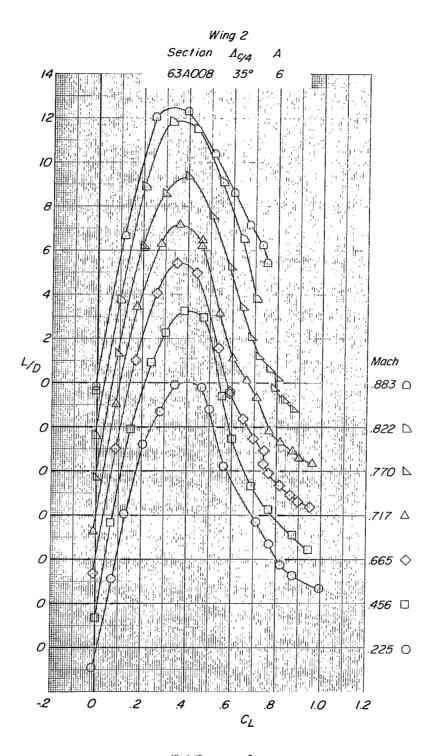
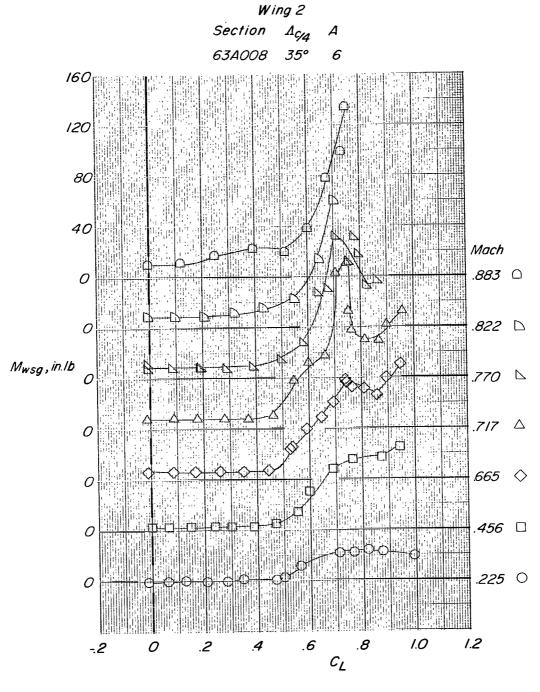


Figure 5.- Continued.



(f) L/D versus  $C_L$ .

Figure 5.- Continued.



(g)  $M_{WSg}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 5.- Concluded.

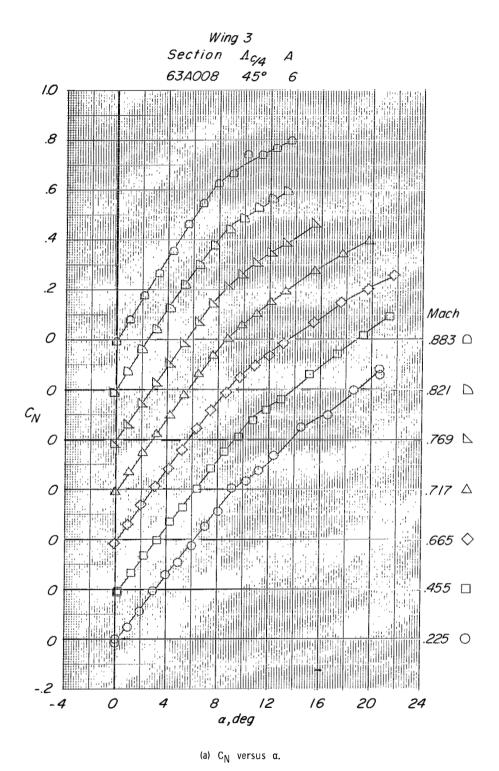
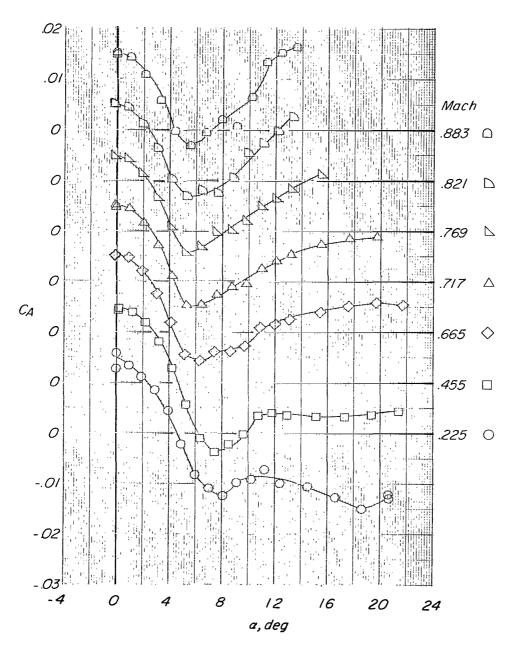
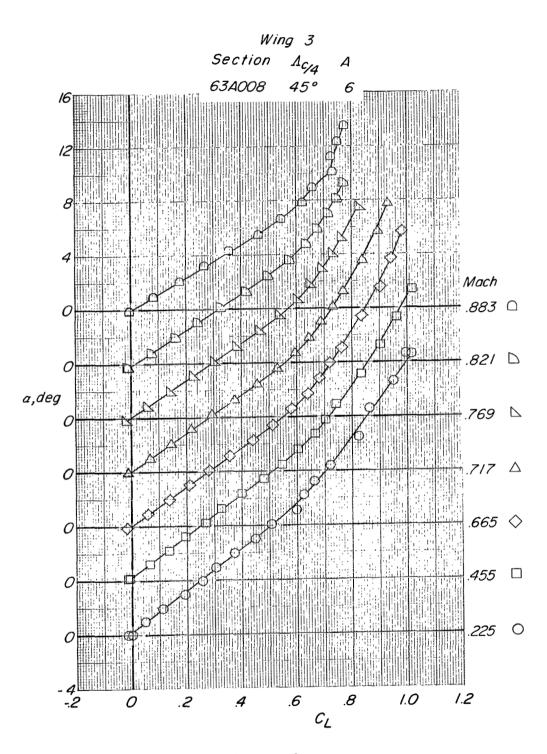


Figure 6.- Static longitudinal aerodynamic and buffet characteristics of the wing 3 configuration at Mach numbers from 0.23 to 0.88. Rounded forebody; transition grit on.

Wing 3 Section  $A_{6/4}$  A 63A008 45° 6

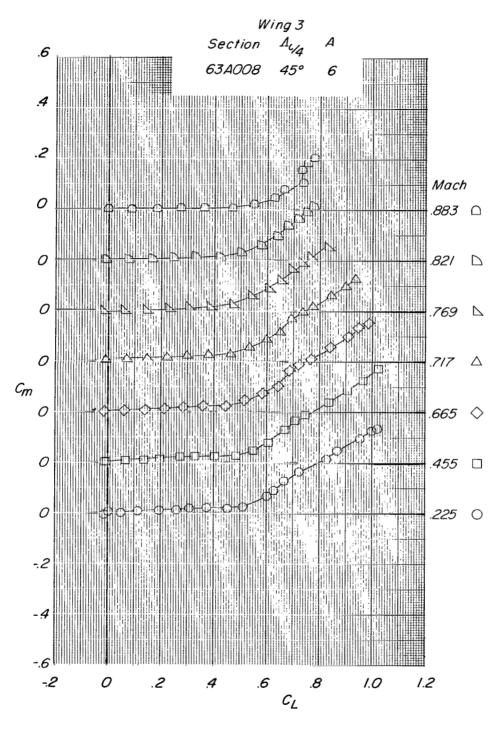


(b) C<sub>A</sub> versus α. Figure 6.- Continued.

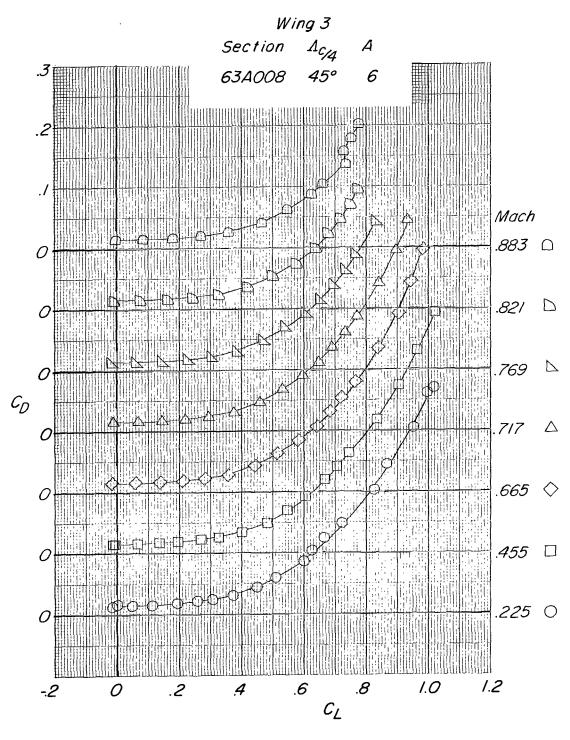


(c)  $\alpha$  versus  $\boldsymbol{C}_L.$ 

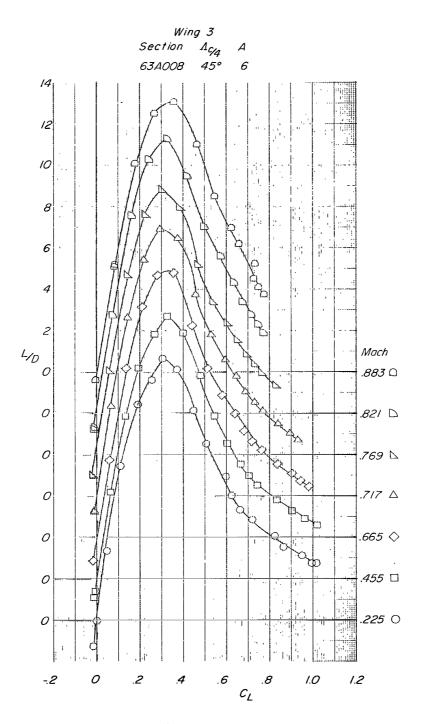
Figure 6.- Continued.



(d)  $C_{m}$  versus  $C_{L}$ . Figure 6.- Continued.

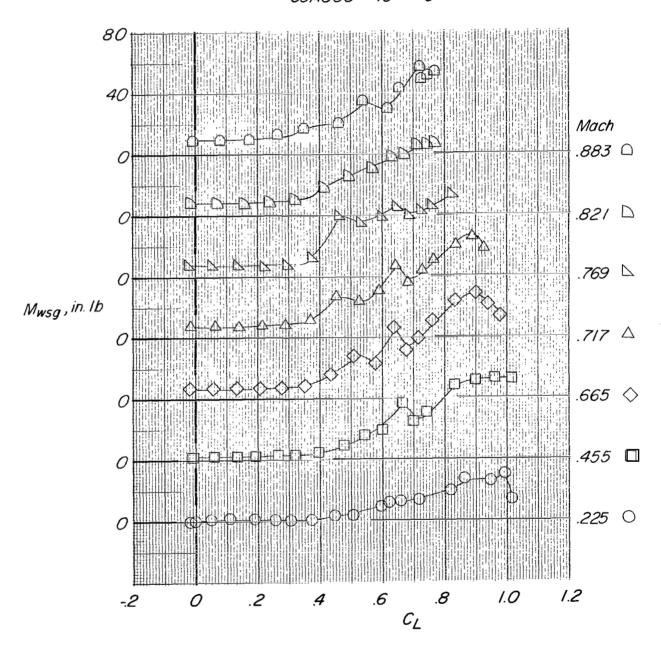


(e)  $C_D$  versus  $C_L$ . Figure 6.- Continued.



(f) L/D versus  $C_L$ . Figure 6.- Continued.

Wing 3
Section  $\Lambda_{\text{C/4}}$  A
63A008 45° 6



(g)  $M_{WSG}$  versus  $C_L$ . (1 in. 1b = 0.113 m-N.) Figure 6.- Concluded.

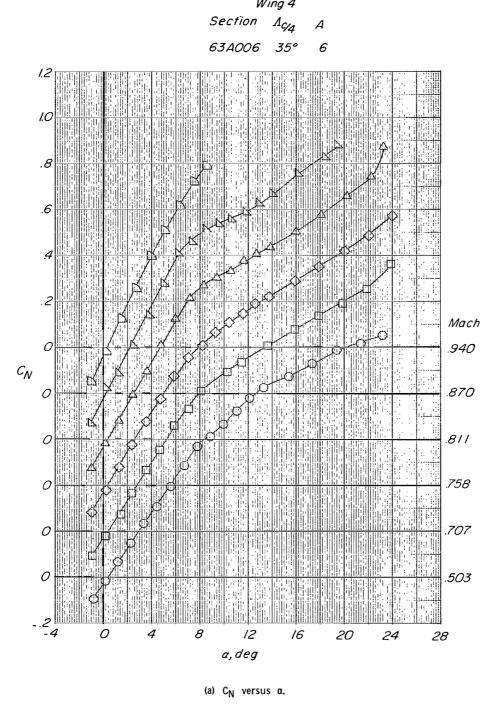
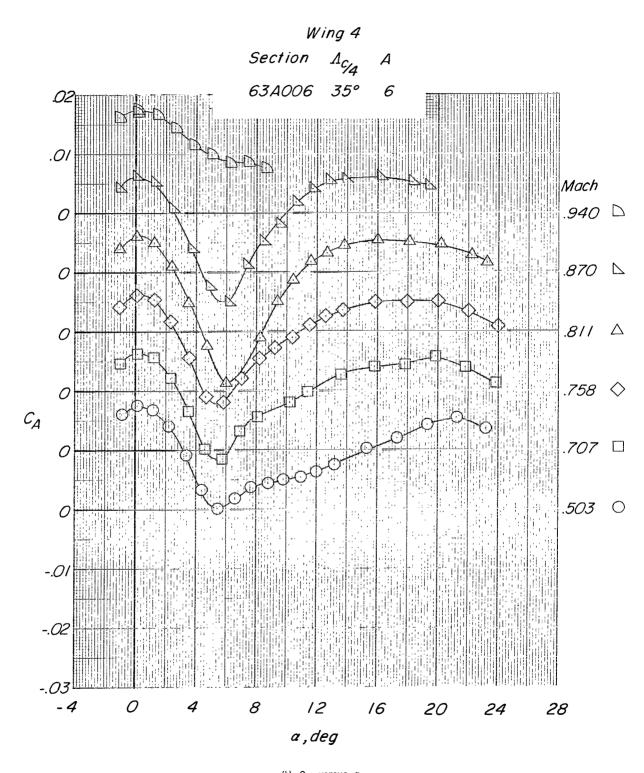


Figure 7.- Static longitudinal aerodynamic and buffet characteristics of the wing 4 configuration at Mach numbers from 0.50 to 0.94. Rounded forebody; transition grit on.



(b)  $C_A$  versus  $\alpha$ . Figure 7.- Continued.

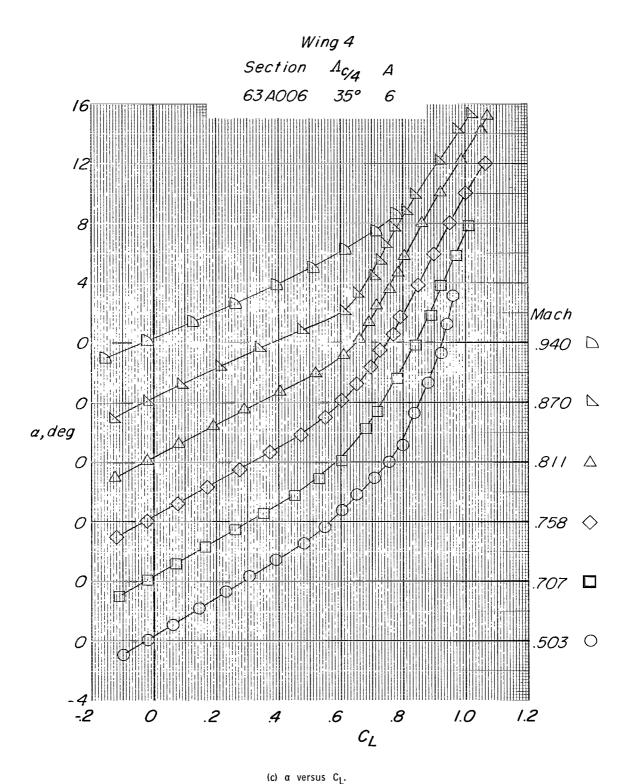
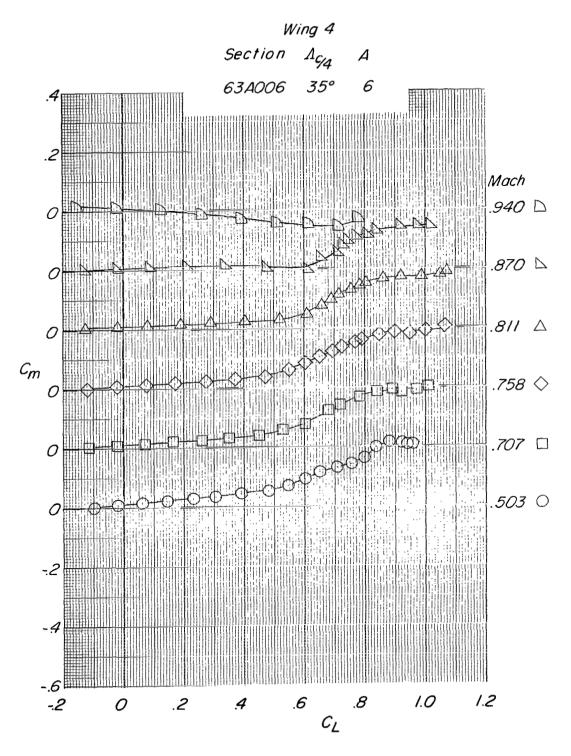
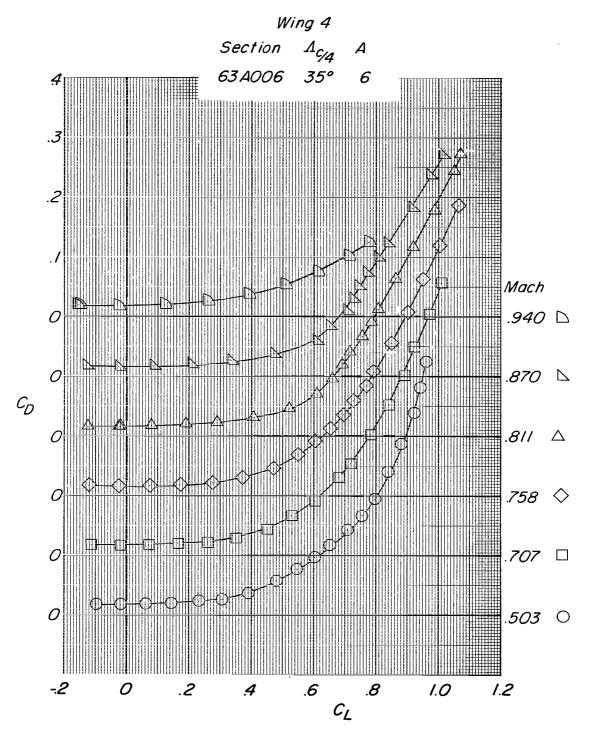


Figure 7.- Continued.



(d)  $C_{\text{m}}$  versus  $C_{\text{L}}$ . Figure 7.- Continued.



(e)  $C_D$  versus  $C_L$ . Figure 7.- Continued.

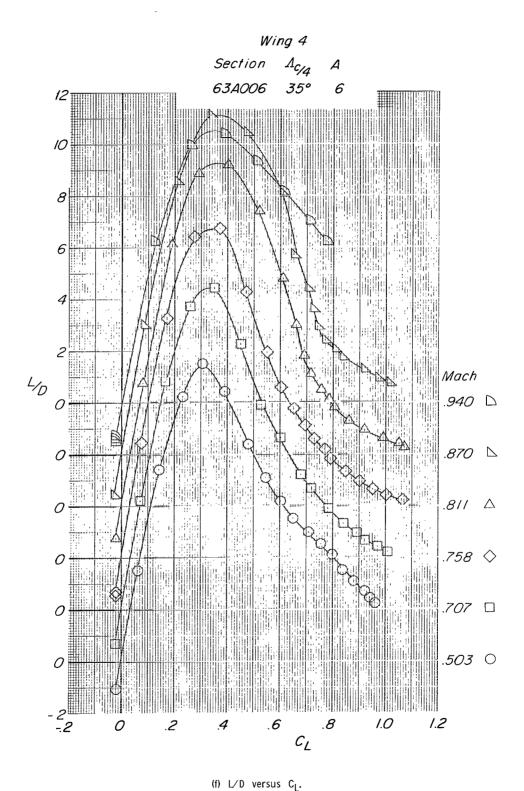
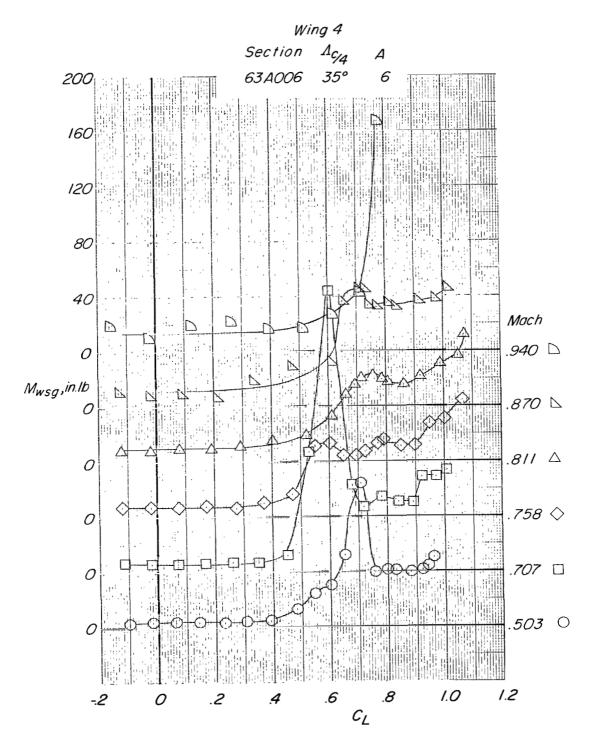


Figure 7.- Continued.



(g)  $M_{WSG}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 7.- Concluded.

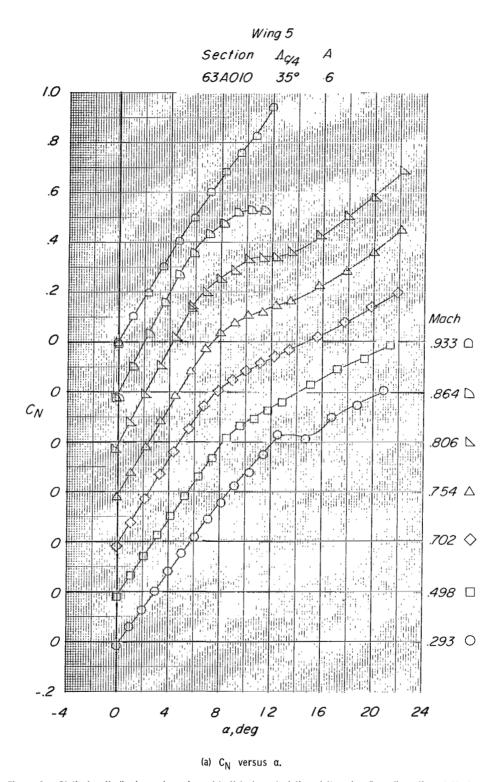
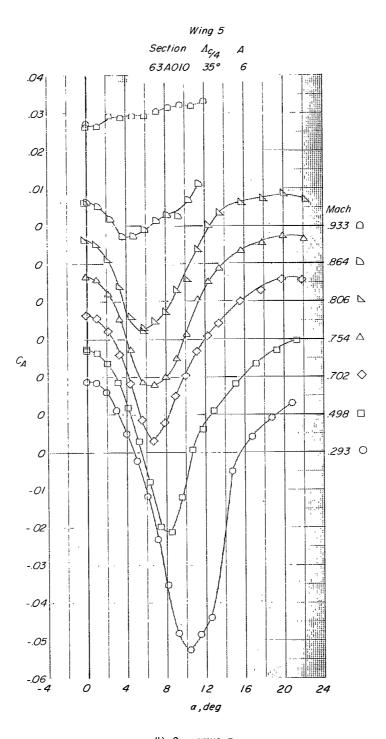
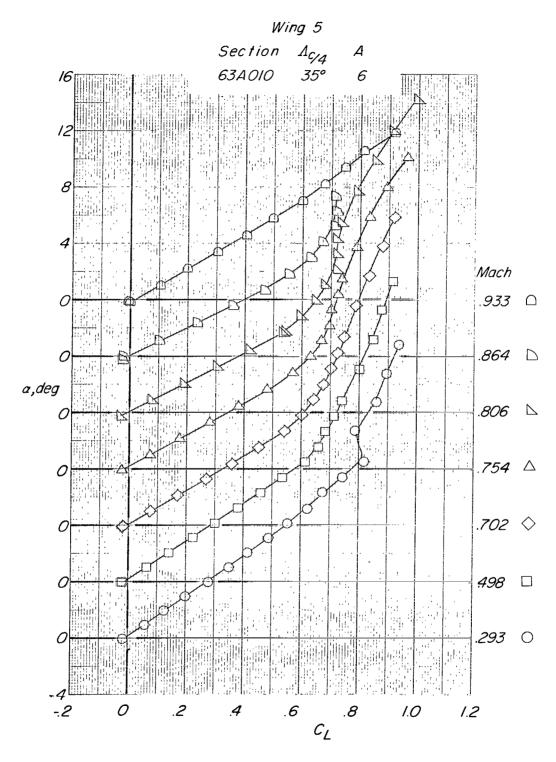


Figure 8.- Static longitudinal aerodynamic and buffet characteristics of the wing 5 configuration at Mach numbers from 0.29 to 0.93. Rounded forebody; transition grit on.

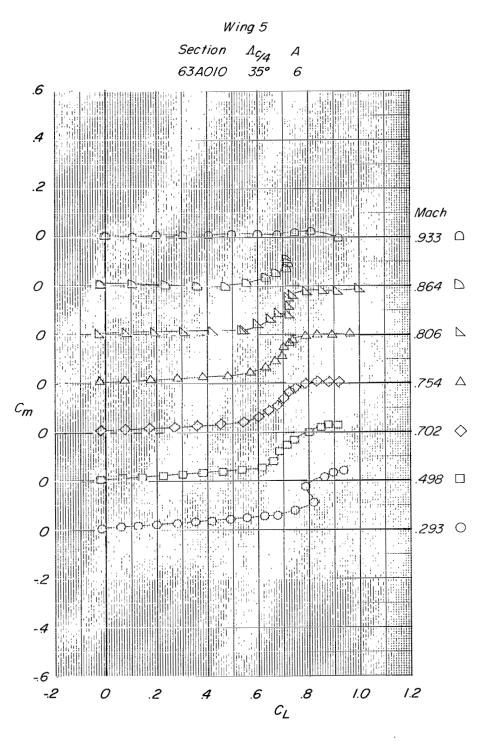


(b)  $C_{\mbox{\scriptsize A}}$  versus  $\alpha_{\mbox{\scriptsize .}}$  Figure 8.- Continued.

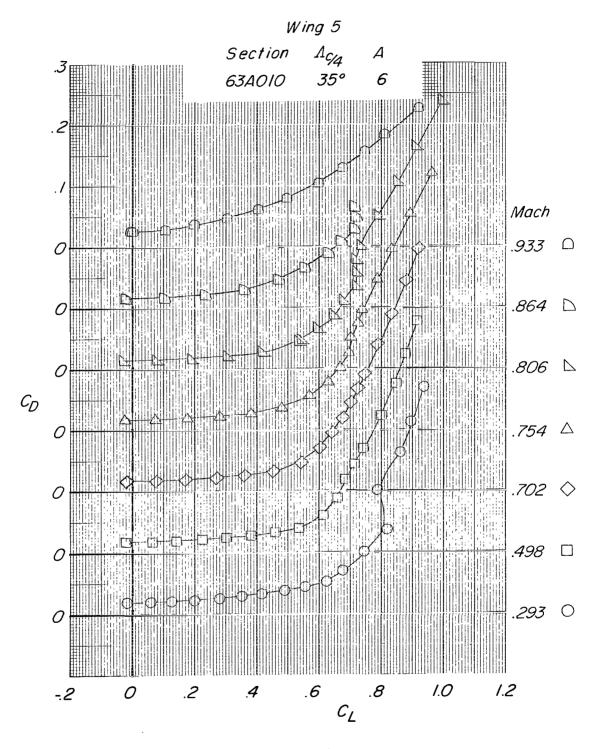


(c)  $\alpha$  versus  $C_L$ .

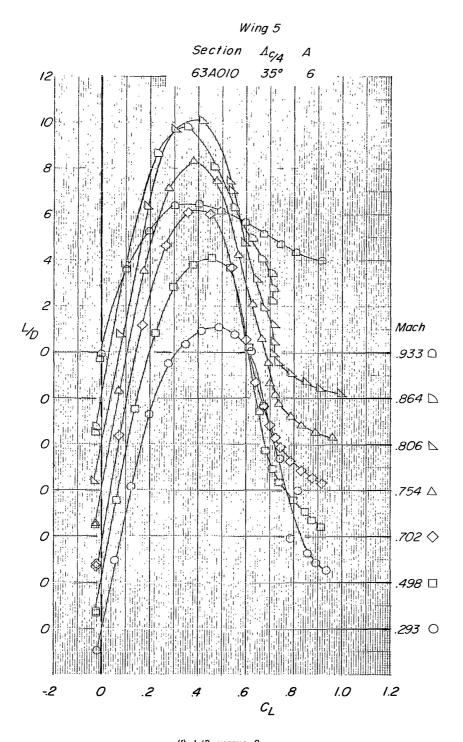
Figure 8.- Continued.



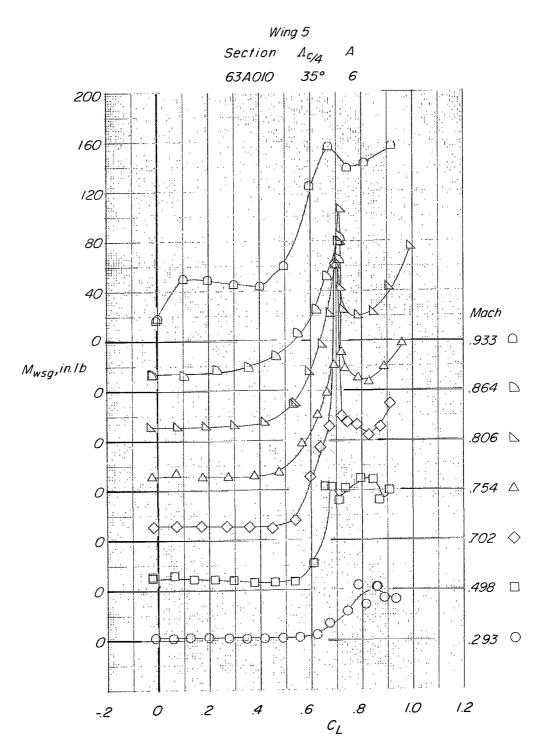
(d)  $C_{m}$  versus  $C_{L}$ . Figure 8.- Continued.



(e)  $C_D$  versus  $C_L$ . Figure 8.- Continued.



(f) L/D versus  $C_L$ . Figure 8.- Continued.



(g)  $M_{WSg}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 8.- Concluded.

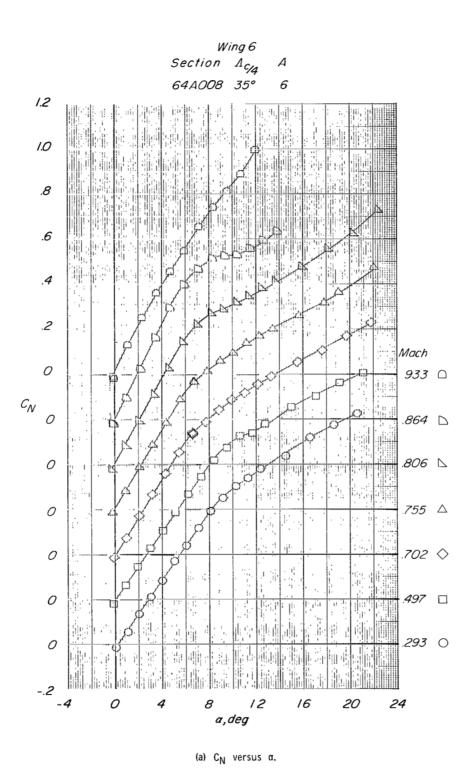
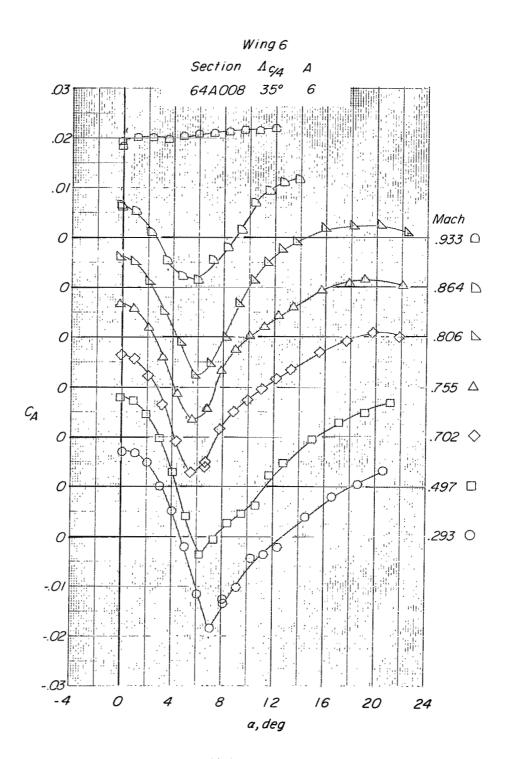
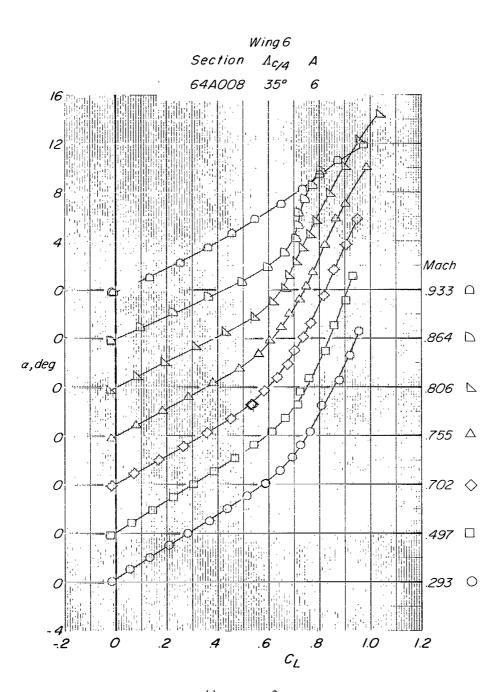


Figure 9.- Static longitudinal aerodynamic and buffet characteristics of the wing 6 configuration at Mach numbers from 0.29 to 0.93.

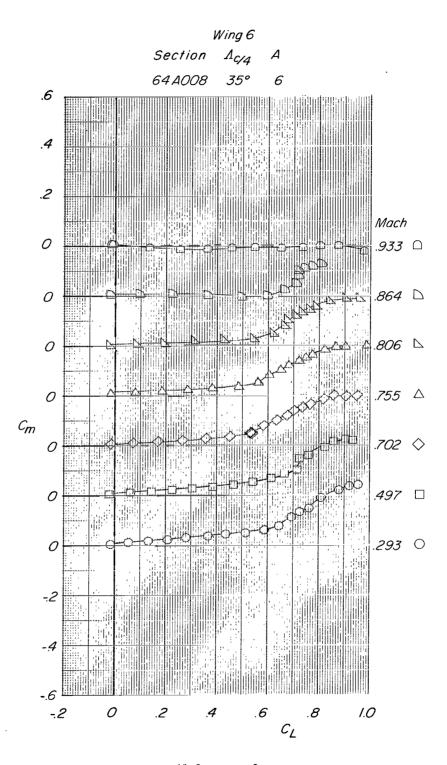
Rounded forebody; transition grit on.



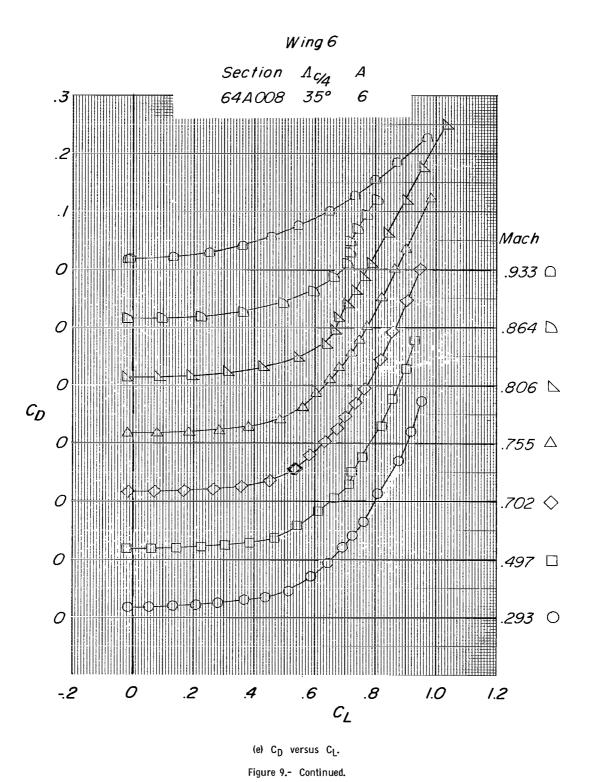
(b)  $C_{\mbox{\scriptsize A}}$  versus  $\alpha.$  Figure 9.- Continued.

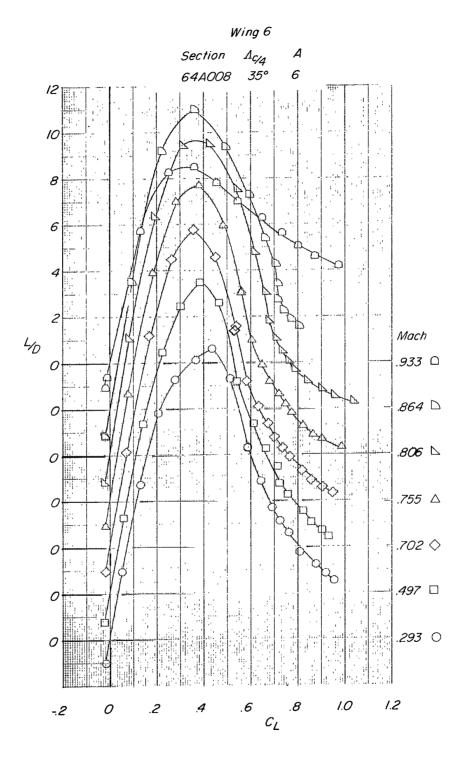


(c)  $\alpha$  versus  $C_L$ . Figure 9.- Continued.



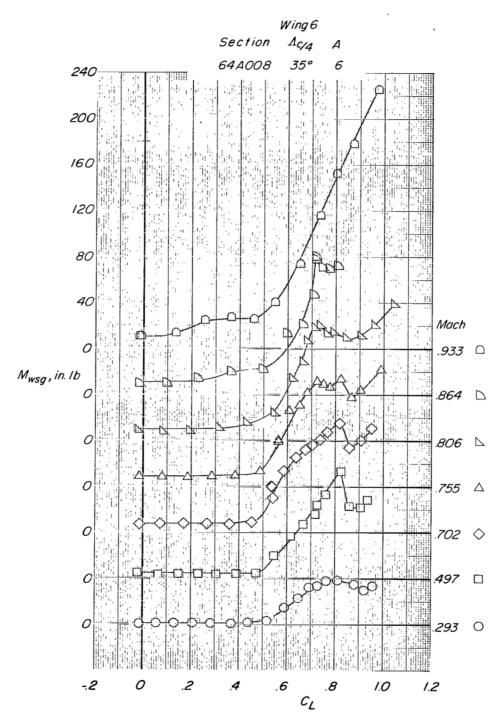
(d)  $C_m$  versus  $C_L$ . Figure 9.- Continued.





(f) L/D versus  $C_L$ . Figure 9.- Continued.

160



(g)  $M_{WSg}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 9.- Concluded.

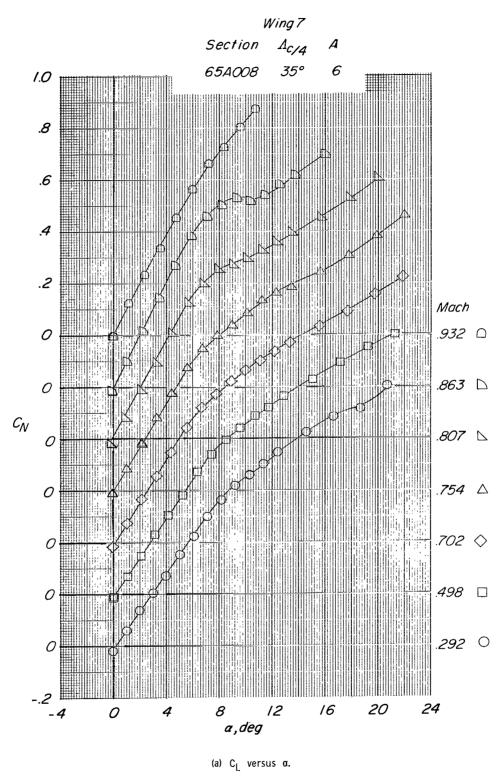
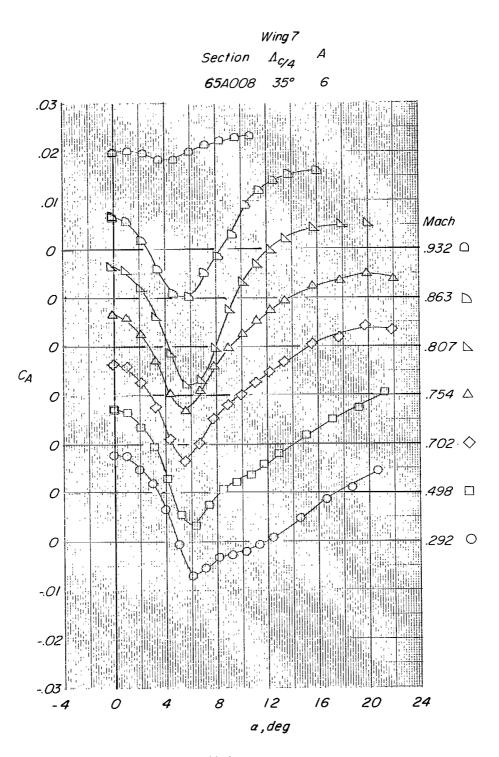


Figure 10.- Static longitudinal aerodynamic and buffet characteristics of the wing 7 configuration at Mach numbers from 0.29 to 0.93. Rounded forebody; transition grit on.



(b) C<sub>A</sub> versus α.
Figure 10.- Continued.

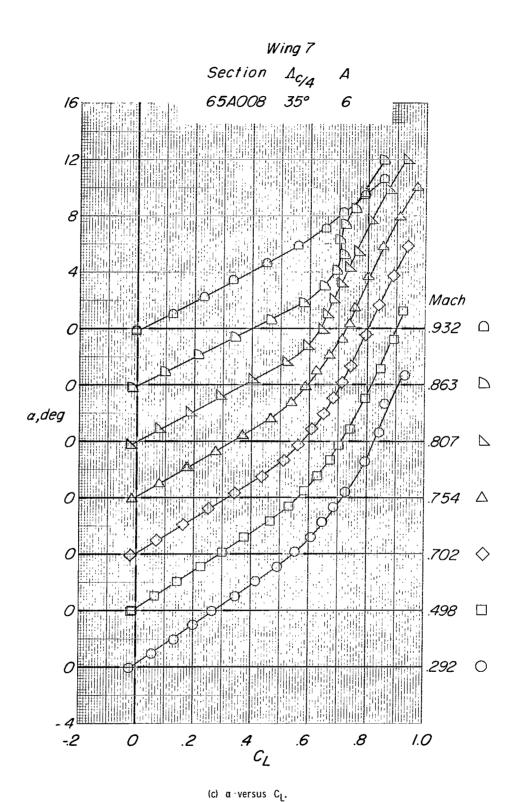
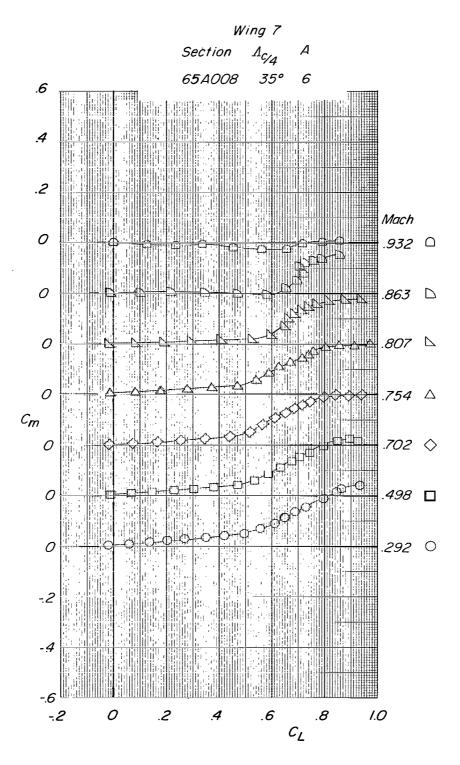
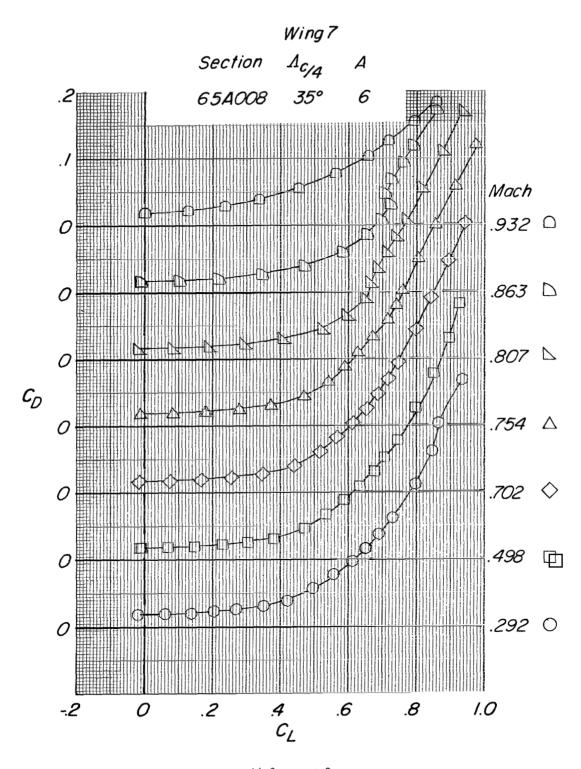


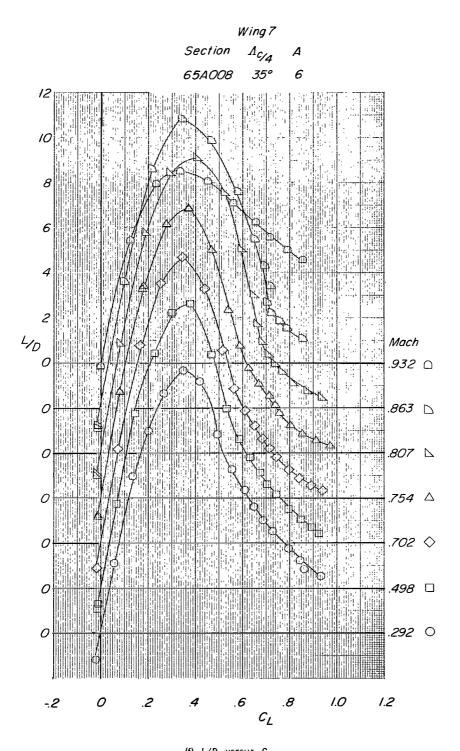
Figure 10.- Continued.



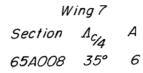
(d)  $C_m$  versus  $C_L$ . Figure 10.- Continued.

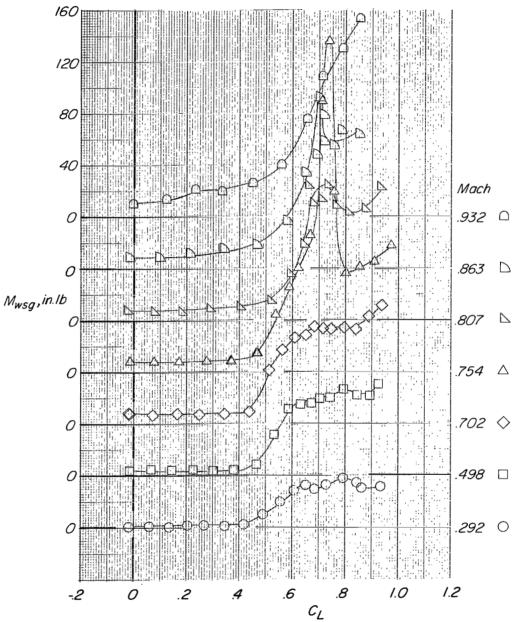


(e)  $C_D$  versus  $C_L$ . Figure 10.- Continued.



(f) L/D versus  $C_L$ . Figure 10.- Continued.





(g)  $M_{WSg}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 10.- Concluded.

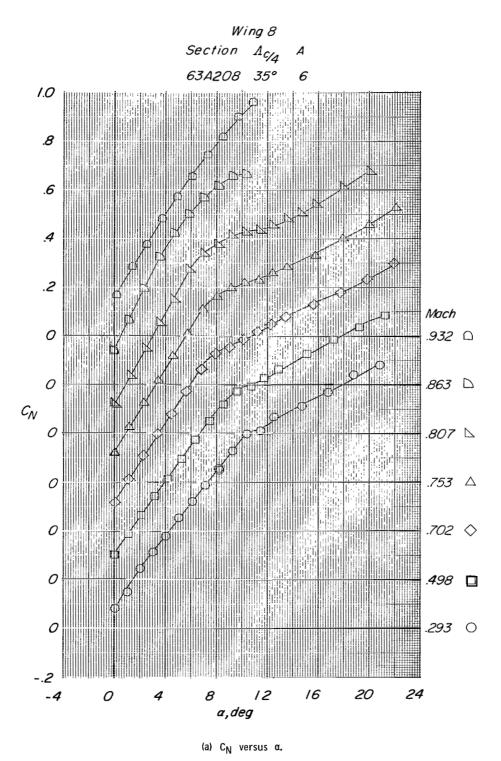
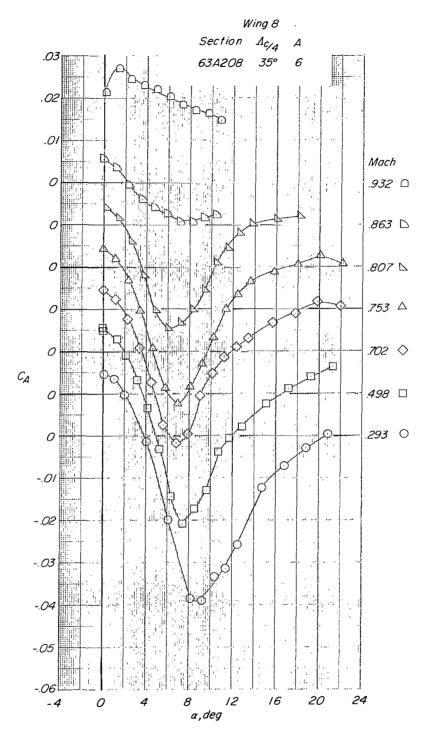


Figure 11.- Static longitudinal aerodynamic and buffet characteristics of the wing 8 configuration at Mach numbers from 0.29 to 0.93. Rounded forebody; transition grit off.



(b) C<sub>A</sub> versus α.

Figure 11.- Continued.

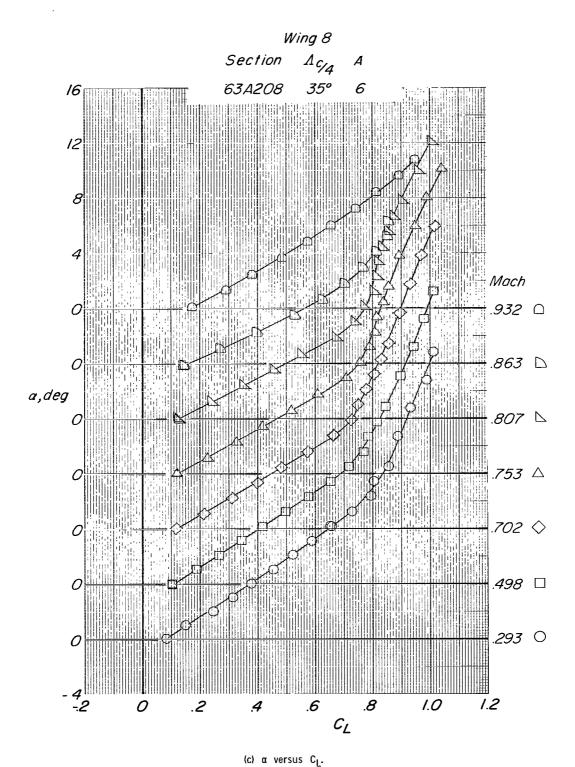
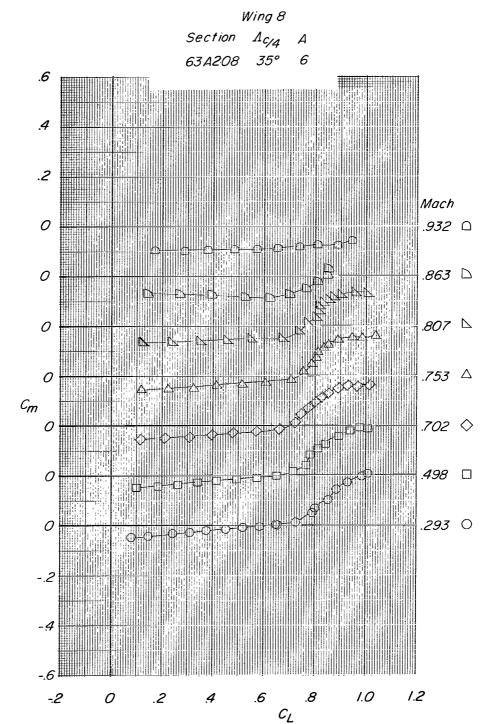
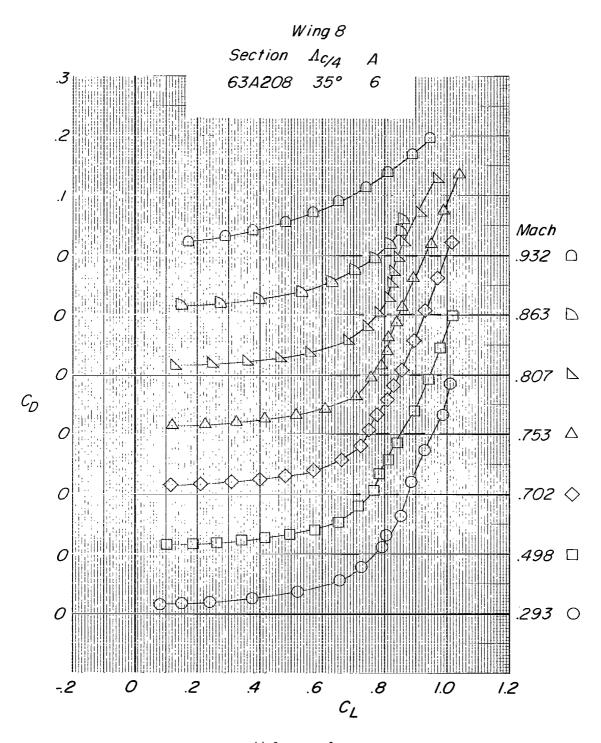


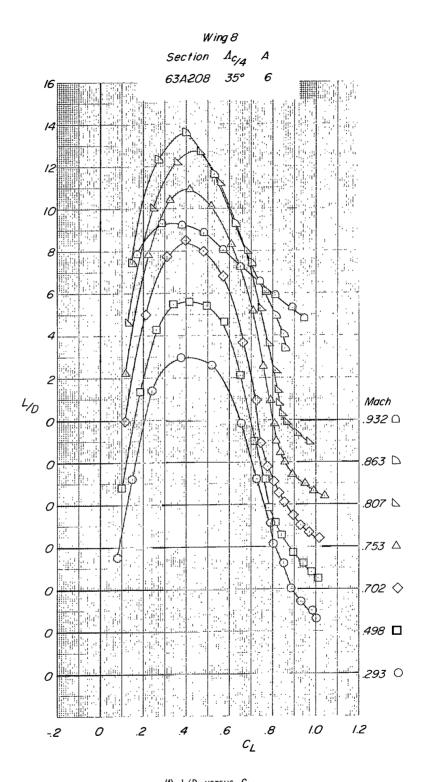
Figure 11.- Continued.



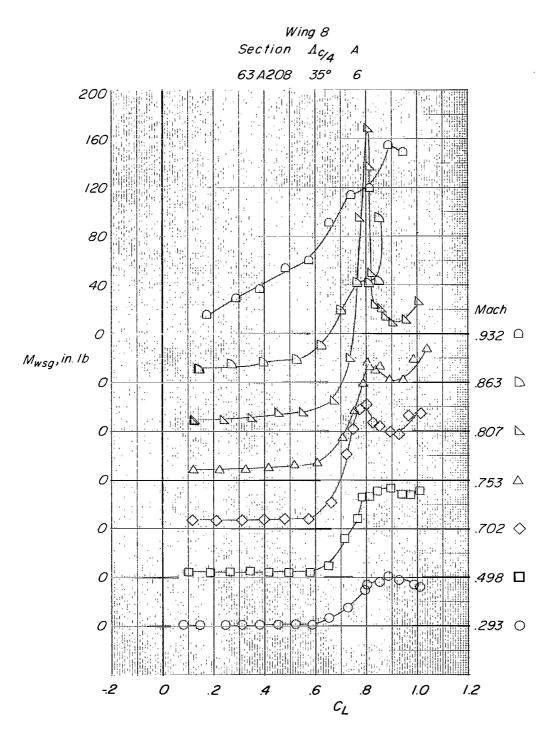
(d)  $C_{m}$  versus  $C_{L}$ . Figure 11.- Continued.



(e)  $C_D$  versus  $C_L$ . Figure 11.- Continued.



(f) L/D versus  $C_L$ . Figure 11.- Continued.



(g)  $M_{WSg}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 11.- Concluded.

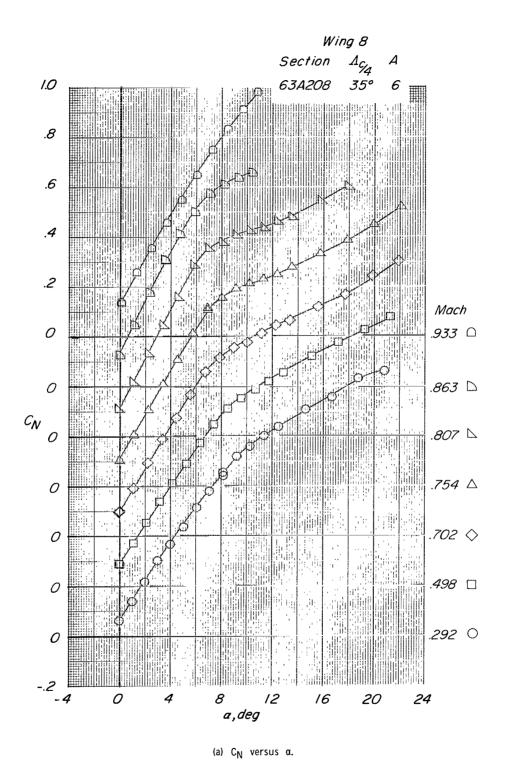
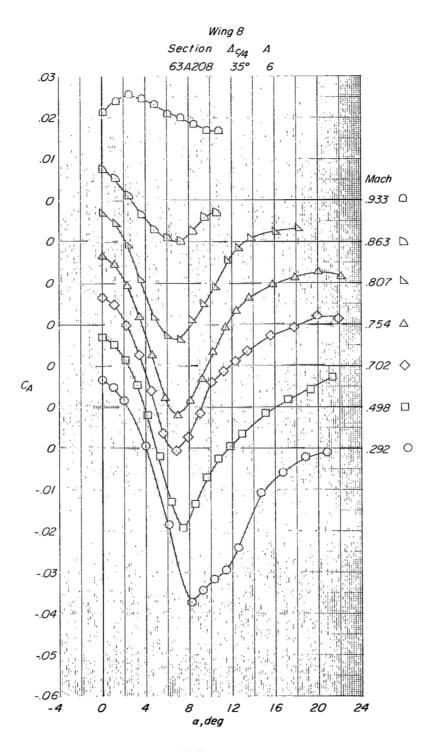
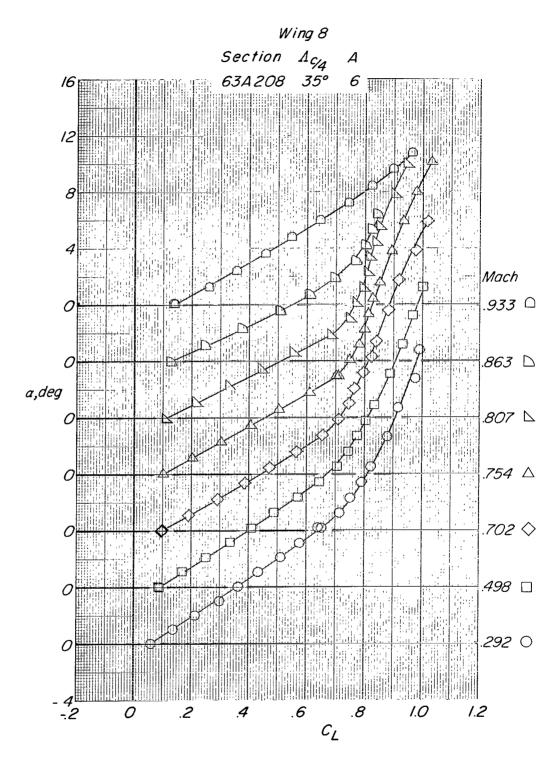


Figure 12.- Static longitudinal aerodynamic and buffet characteristics of the wing 8 configuration at Mach numbers from 0.29 to 0.93. Rounded forebody; transition grit on.

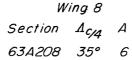


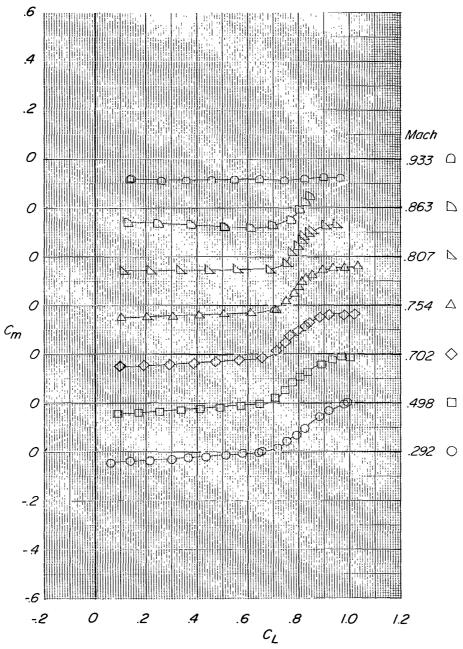
(b)  $C_{\mbox{A}}$  versus  $\alpha.$  Figure 12.- Continued.



(c)  $\alpha$  versus  $\boldsymbol{C}_{L}.$ 

Figure 12.- Continued.





(d)  $C_m$  versus  $C_L$ . Figure 12.- Continued.

(e)  $C_{D}$  versus  $C_{L}$ . Figure 12.~ Continued.

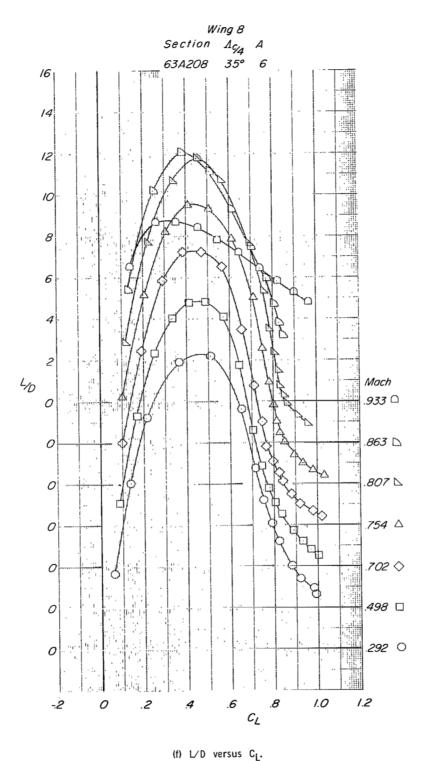
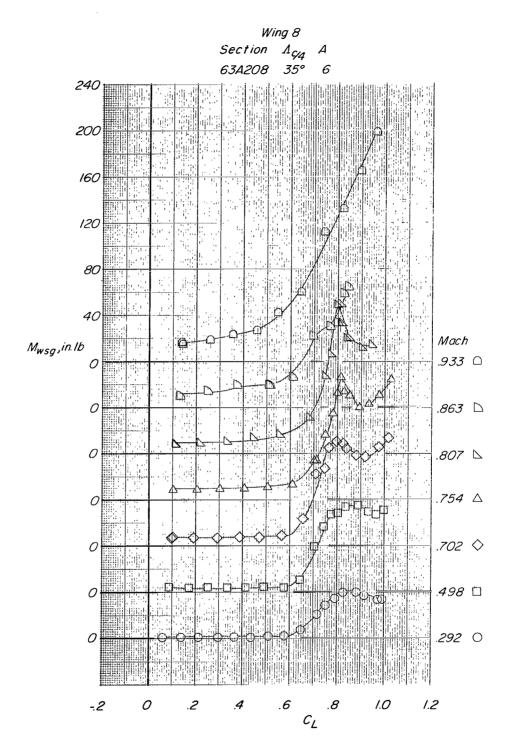


Figure 12.- Continued.



(g)  $M_{WSg}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 12.- Concluded.

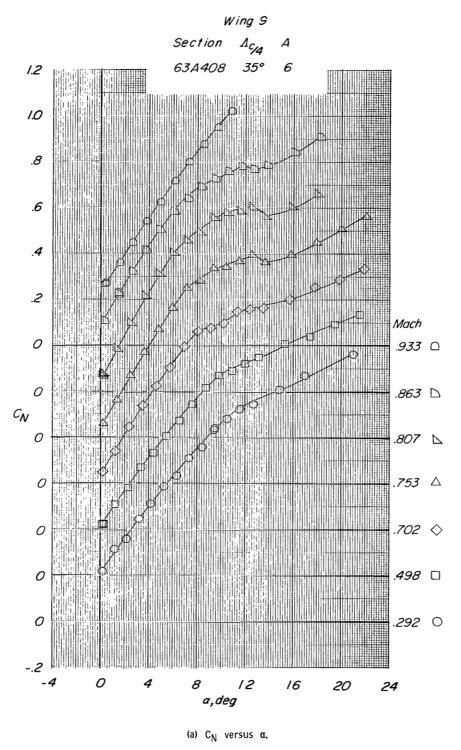
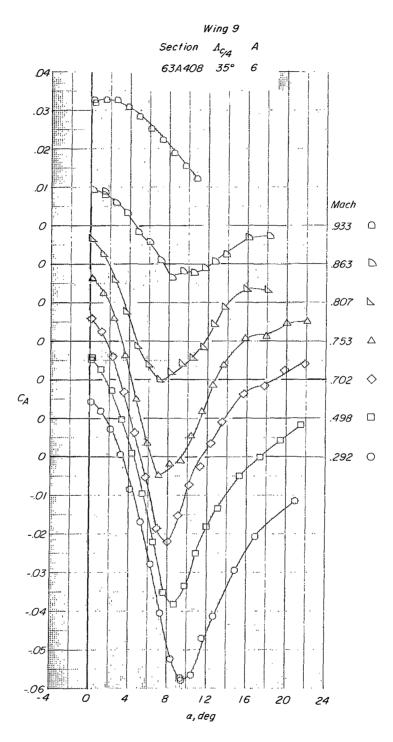
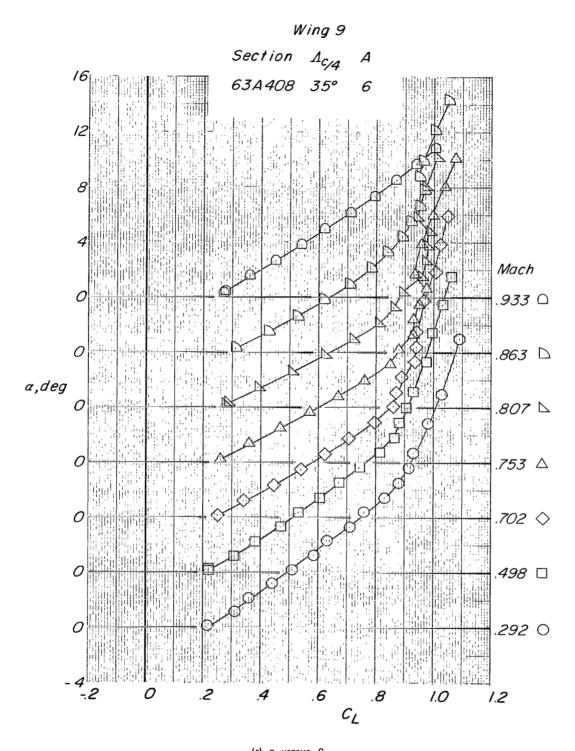


Figure 13.- Static longitudinal aerodynamic and buffet characteristics of the wing 9 configuration at Mach numbers from 0.29 to 0.93. Pointed forebody; transition grit off.



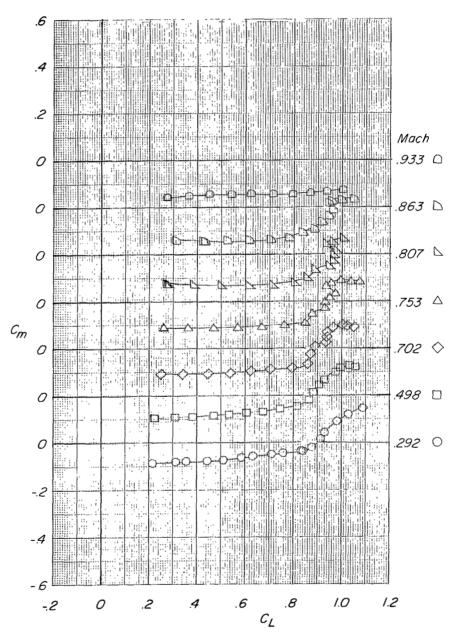
(b)  $C_{\mbox{\scriptsize A}}$  versus  $\alpha.$ 

Figure 13.- Continued.

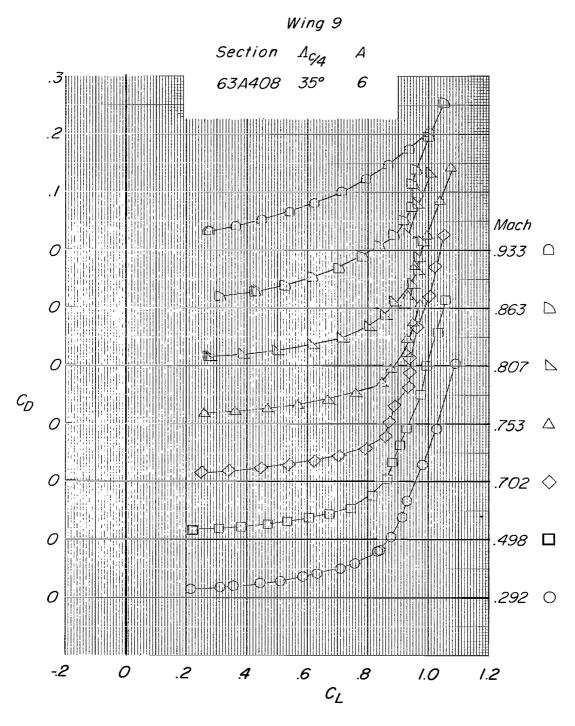


(c)  $\alpha$  versus  $C_L$ . Figure 13.- Continued.

Wing 9
Section  $\Lambda_{C/4}$  A
63A408 35° 6



(d)  $C_m$  versus  $C_L$ . Figure 13.- Continued.



(e)  $C_D$  versus  $C_L$ . Figure 13.- Continued.

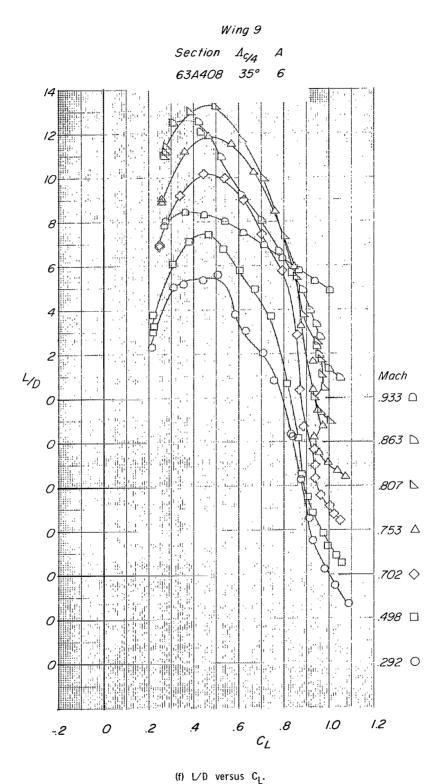
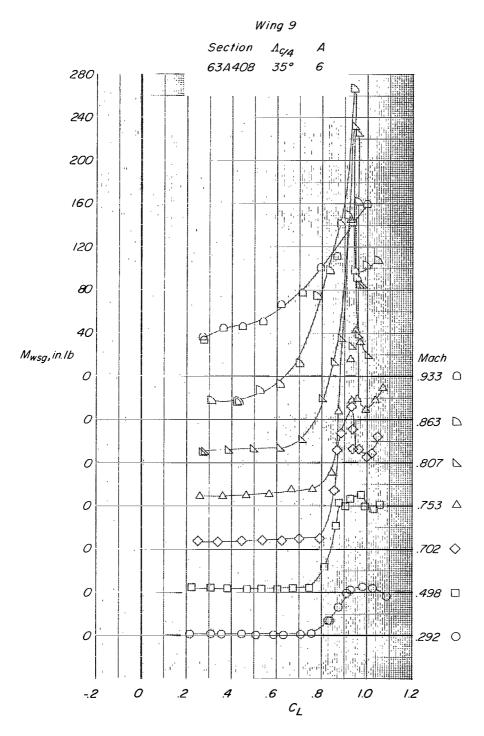


Figure 13.- Continued.



(g)  $M_{WSg}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 13.- Concluded.

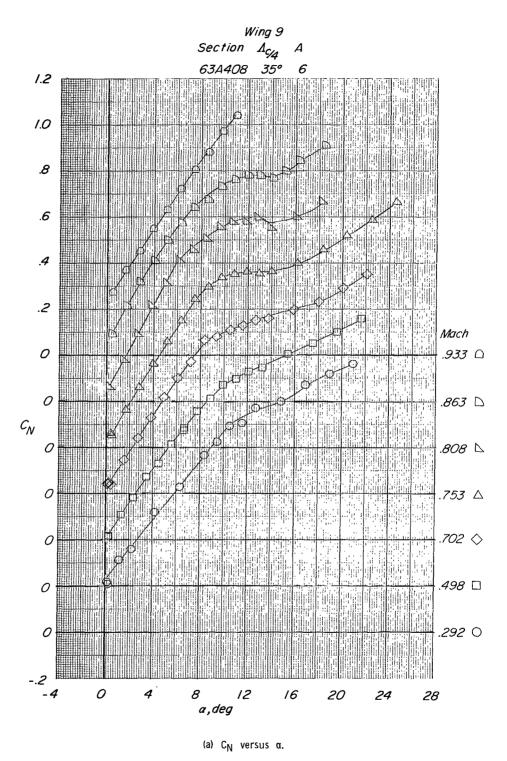
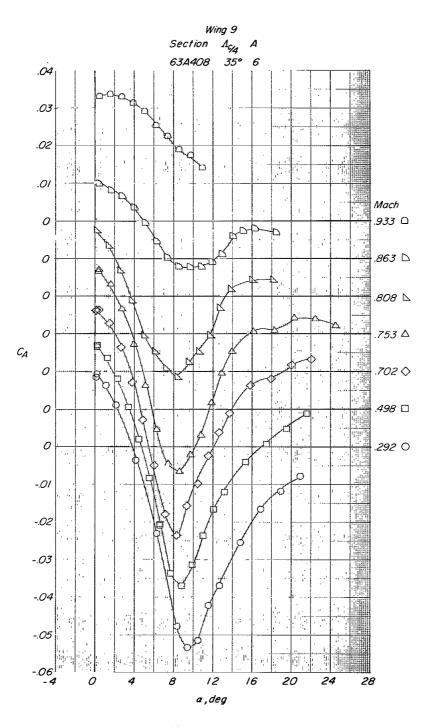
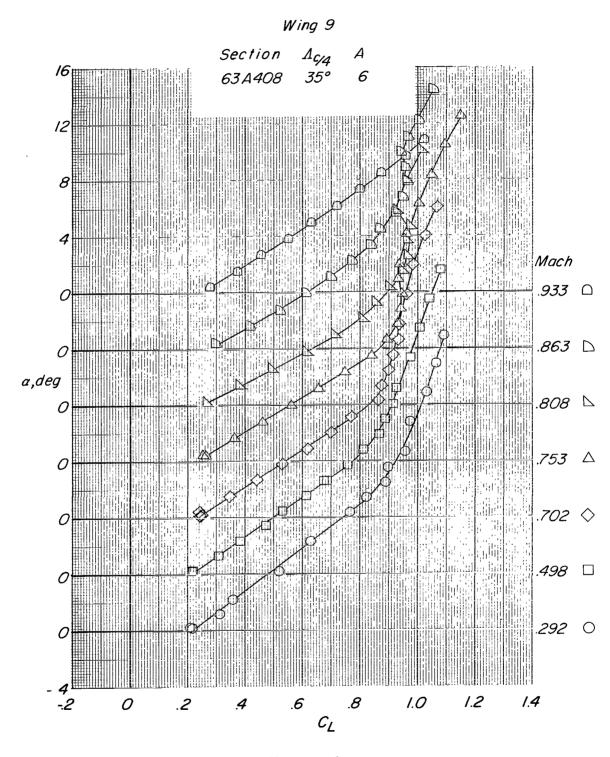


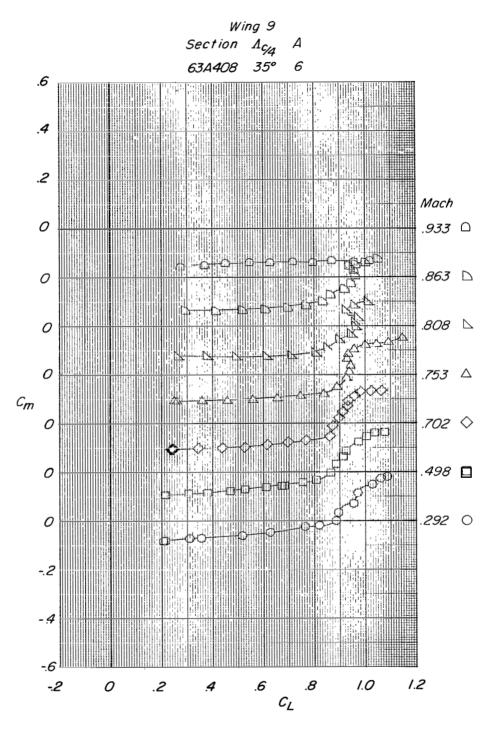
Figure 14.- Static longitudinal aerodynamic and buffet characteristics of the wing 9 configuration at Mach numbers from 0.29 to 0.93. Rounded forebody; transition grit off.



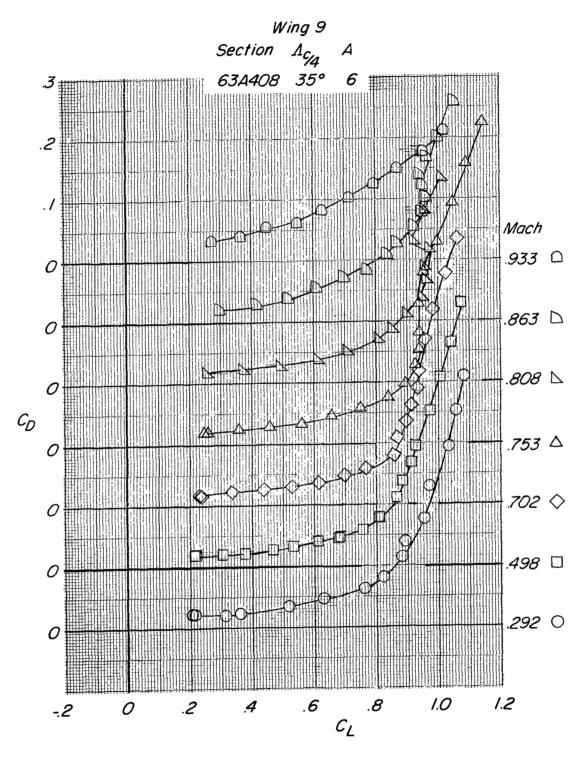
(b) C<sub>A</sub> versus α.Figure 14.- Continued.



(c)  $\alpha$  versus  $C_{\mbox{\scriptsize L}}.$  Figure 14.- Continued.



(d)  $C_{m}$  versus  $C_{L}$ . Figure 14.- Continued.



(e) C<sub>D</sub> versus C<sub>L</sub>.
Figure 14.- Continued.

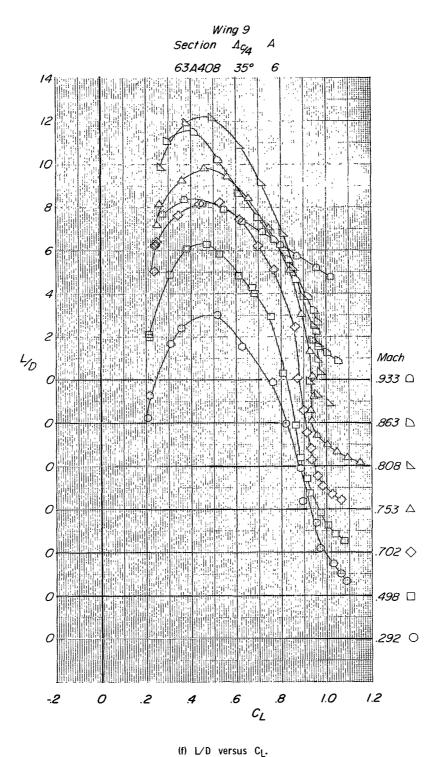
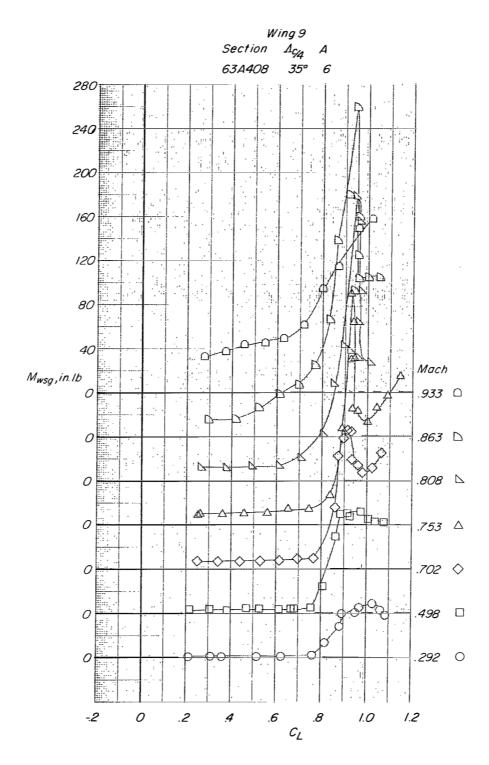


Figure 14.- Continued.



(g)  $M_{WSg}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 14.- Concluded.

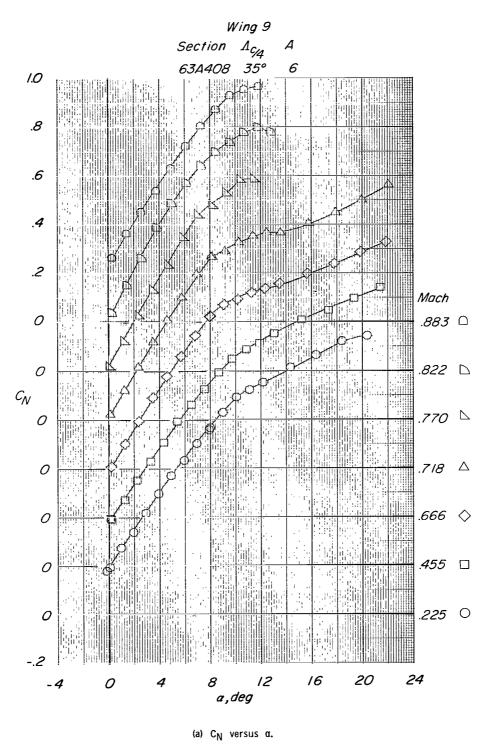
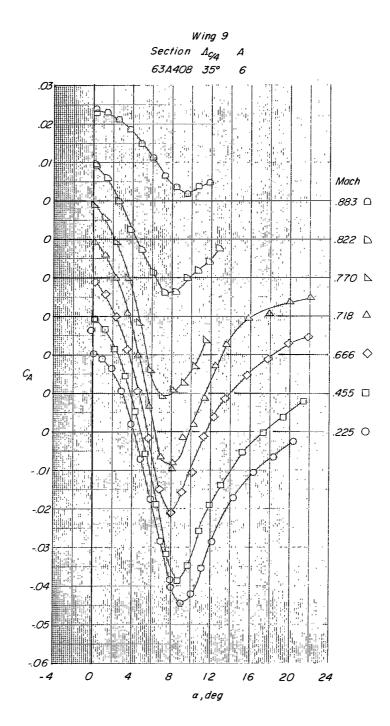
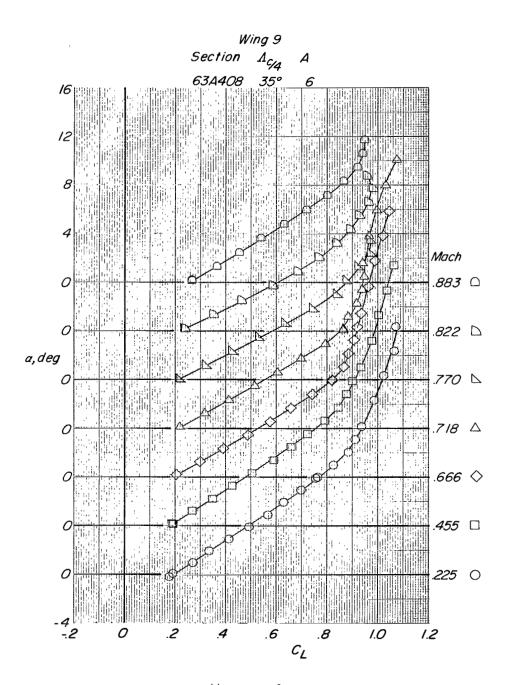


Figure 15.- Static longitudinal aerodynamic and buffet characteristics of the wing 9 configuration at Mach numbers from 0.23 to 0.88. Rounded forebody; transition grit on.



(b)  $C_{\mbox{\scriptsize A}}$  versus  $\alpha.$ 

Figure 15.- Continued.



(c)  $\alpha$  versus  $\text{C}_{\text{L}}\text{.}$ 

Figure 15.- Continued.

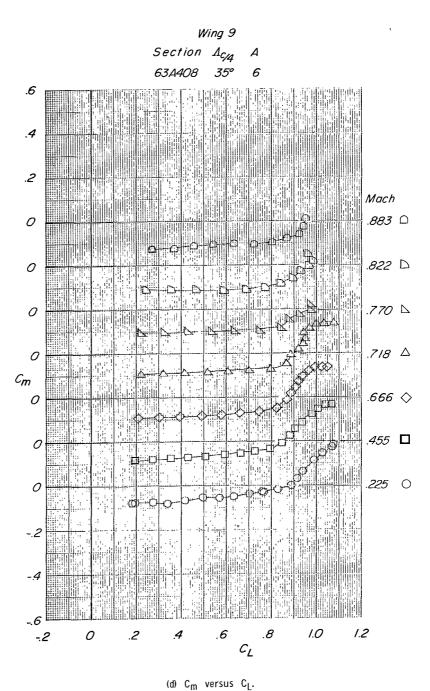
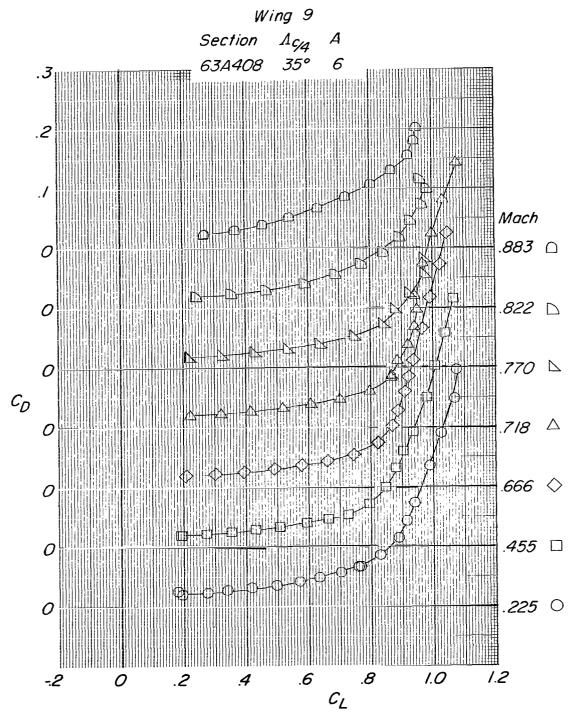
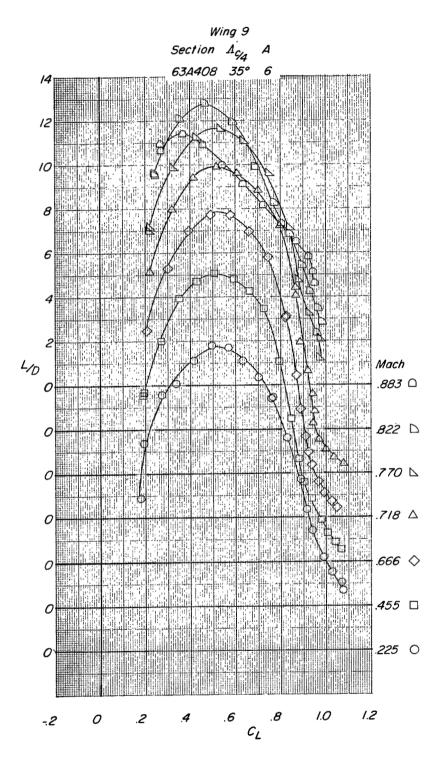


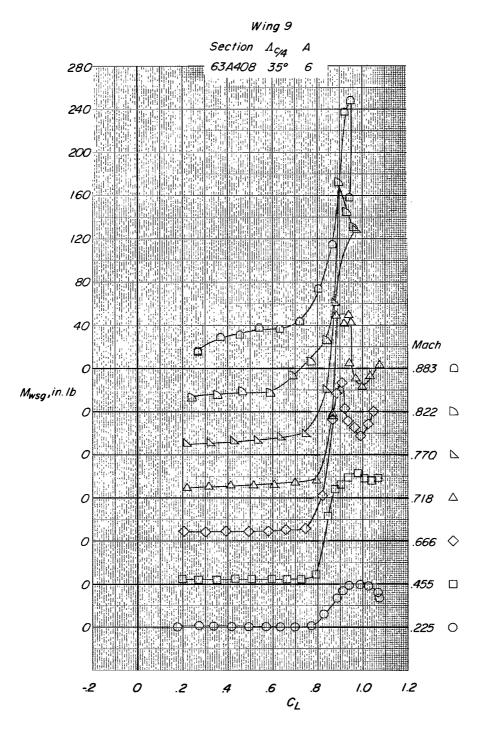
Figure 15.- Continued.



(e)  $C_D$  versus  $C_L$ . Figure 15.- Continued.



(f) L/D versus C<sub>L</sub>.
Figure 15.- Continued.



(g)  $M_{wsg}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 15.- Concluded.

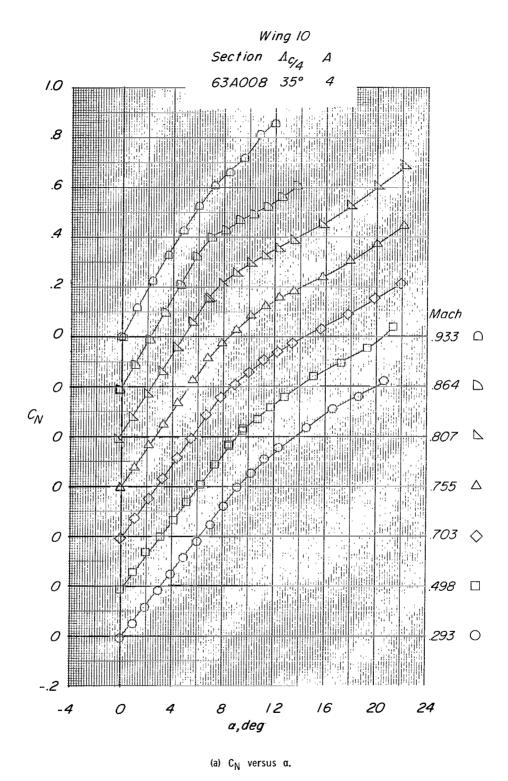


Figure 16.- Static longitudinal aerodynamic and buffet characteristics of the wing 10 configuration at Mach numbers from 0.29 to 0.93. Rounded forebody; transition grit on.

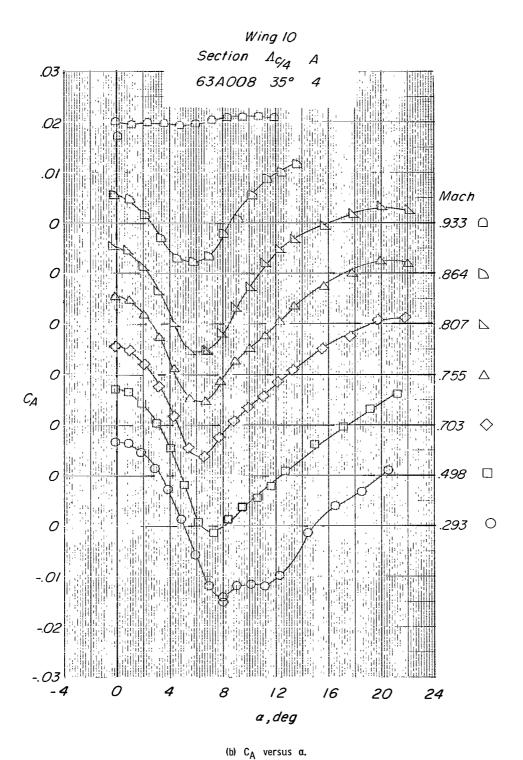
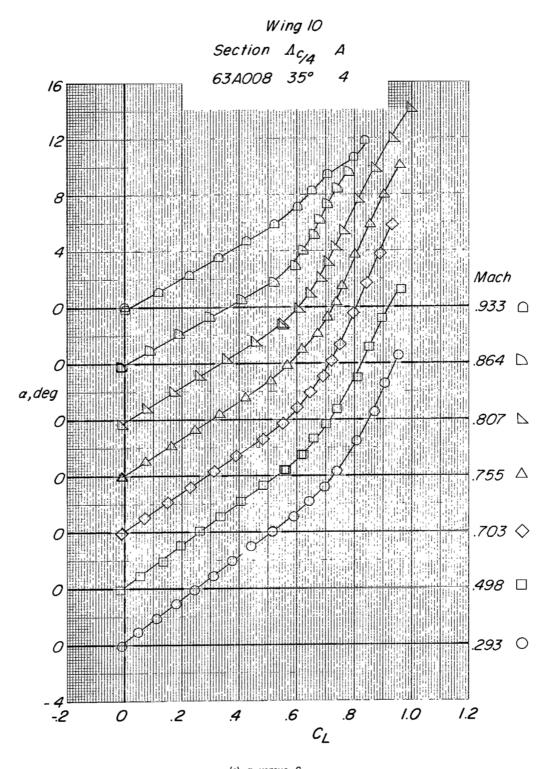
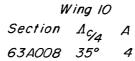
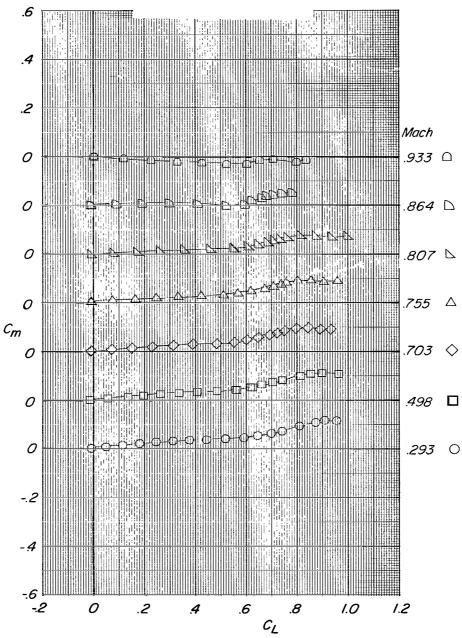


Figure 16.- Continued.

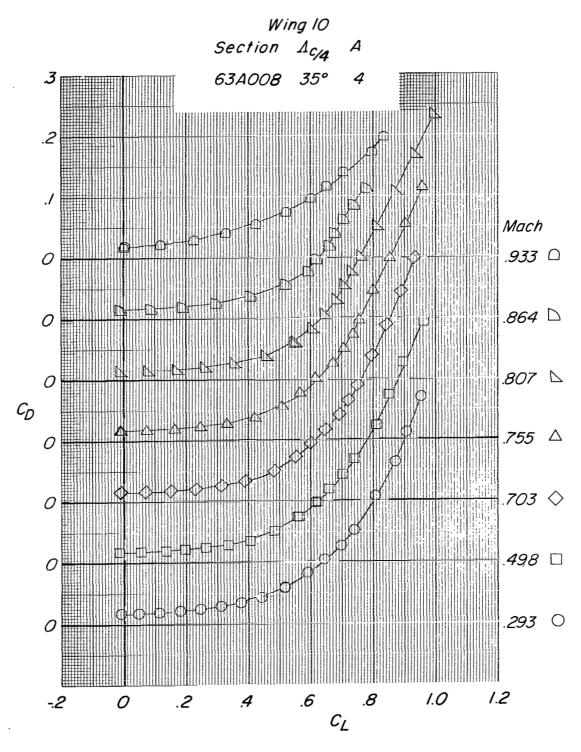


(c)  $\alpha$  versus  $C_{\mbox{\scriptsize L}}.$  Figure 16.- Continued.

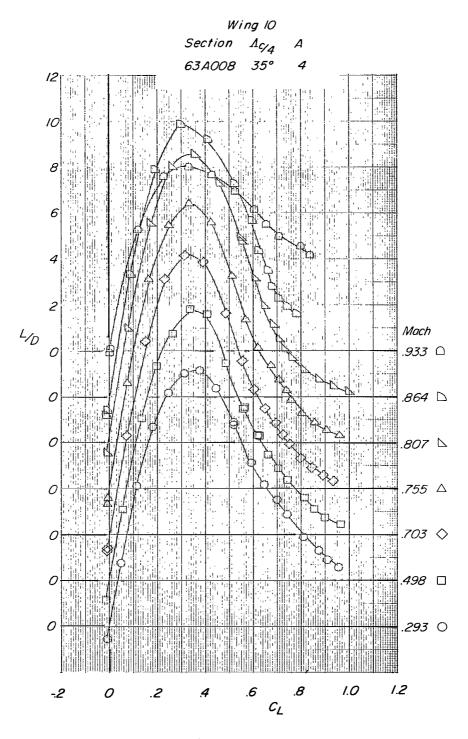




(d)  $C_{m}$  versus  $C_{L}$ . Figure 16.- Continued.

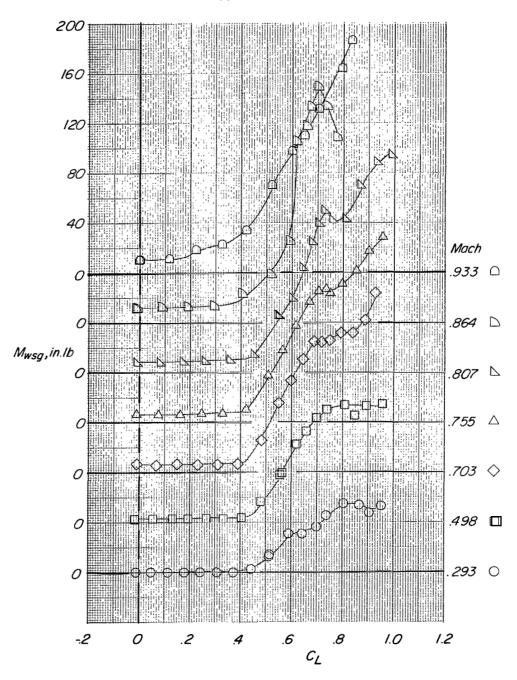


(e) C<sub>D</sub> versus C<sub>L</sub>. Figure 16.- Continued.



(f) L/D versus  $C_L$ . Figure 16.- Continued.

Wing IO
Section  $\Lambda_{c/4}$  A
63A008 35° 4



(g)  $M_{WSG}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 16.- Concluded.

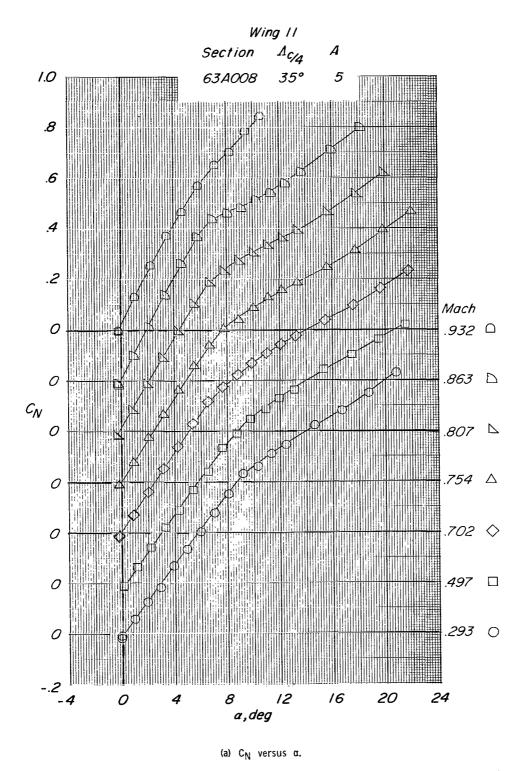


Figure 17.- Static longitudinal aerodynamic and buffet characteristics of the wing 11 configuration at Mach numbers from 0.29 to 0.93. Rounded forebody; transition grit on.

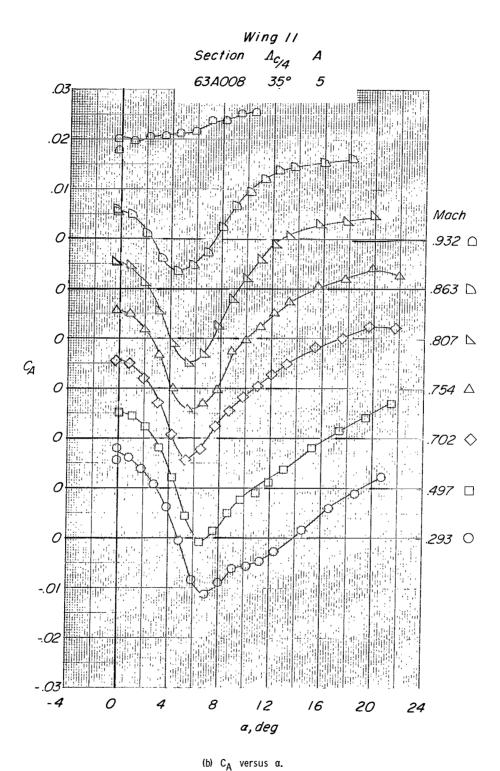


Figure 17.- Continued.

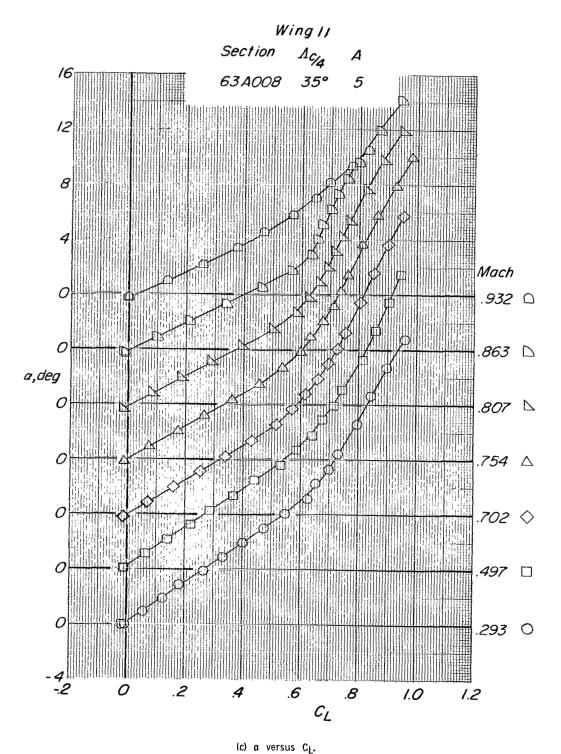
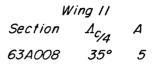
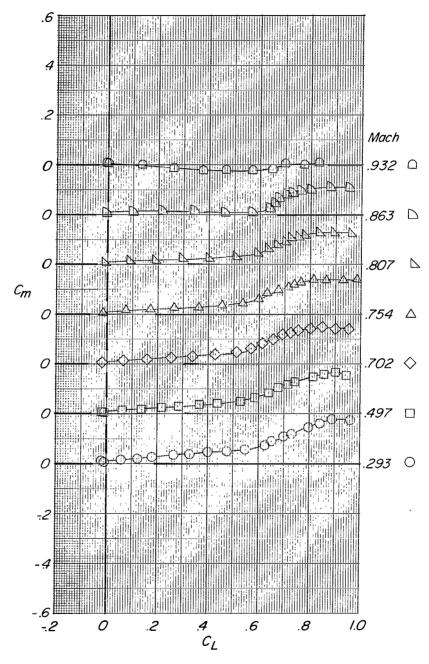


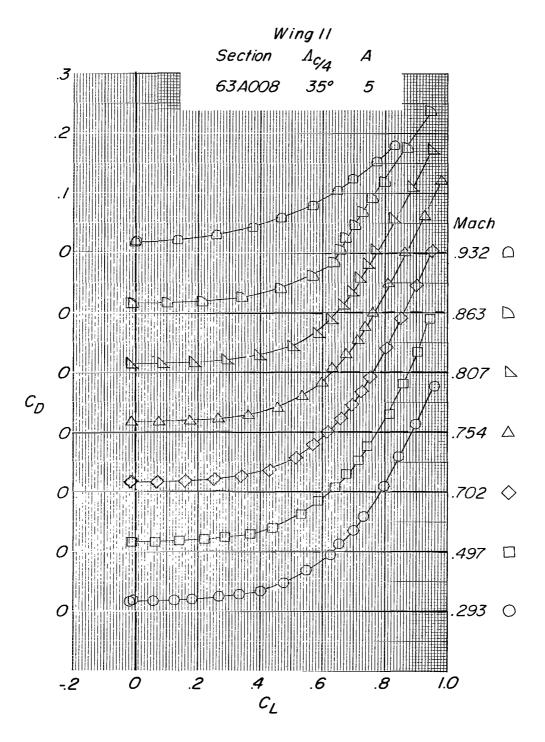
Figure 17.- Continued.



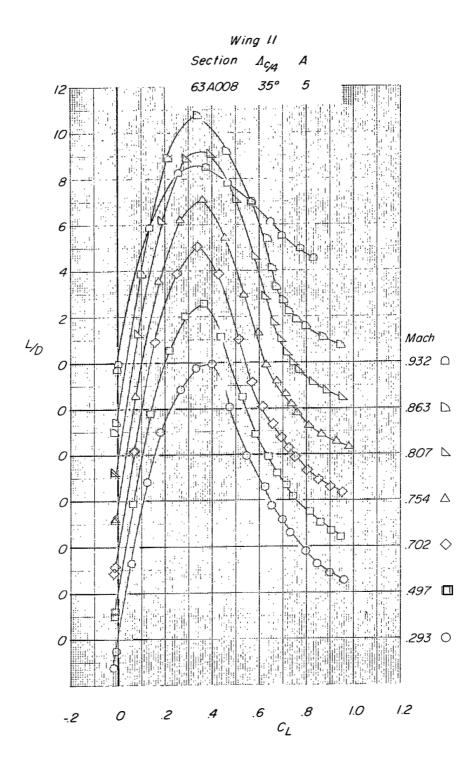


(d)  $C_m$  versus  $C_L$ .

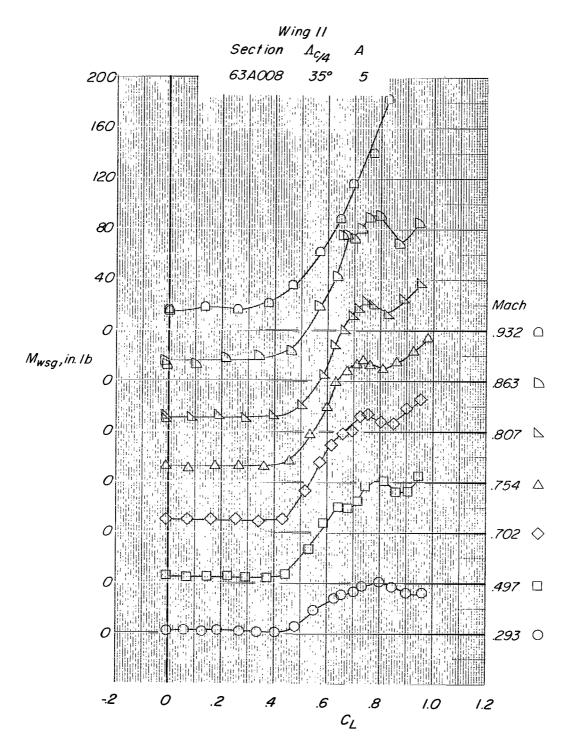
Figure 17.- Continued.



(e)  $C_D$  versus  $C_L$ . Figure 17.- Continued.



(f) L/D versus  $C_L$ . Figure 17.- Continued.



(g)  $M_{WSg}$  versus  $C_L$ . (1 in. lb = 0.113 m-N.) Figure 17.- Concluded.

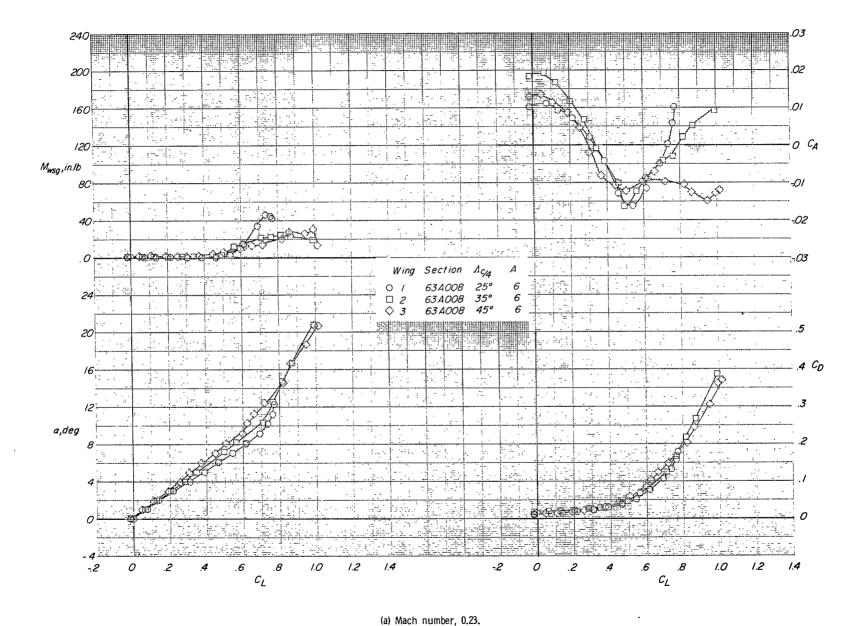
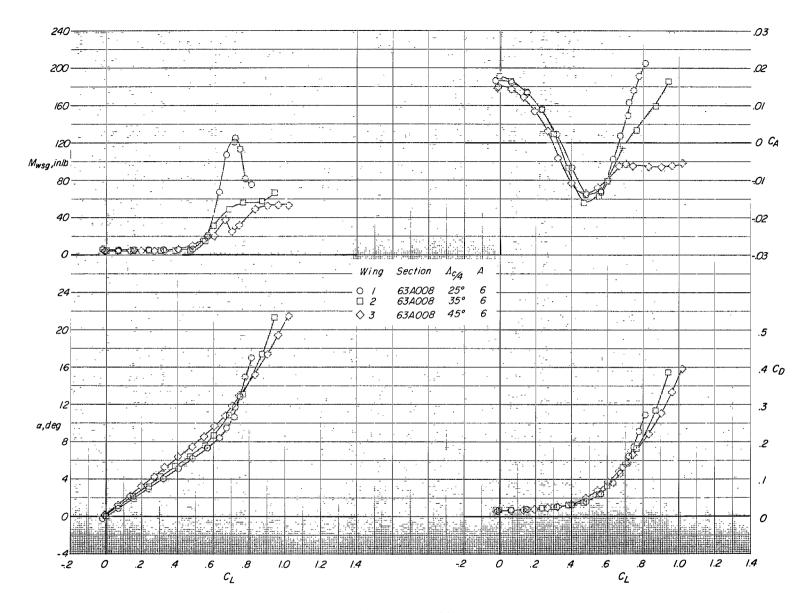
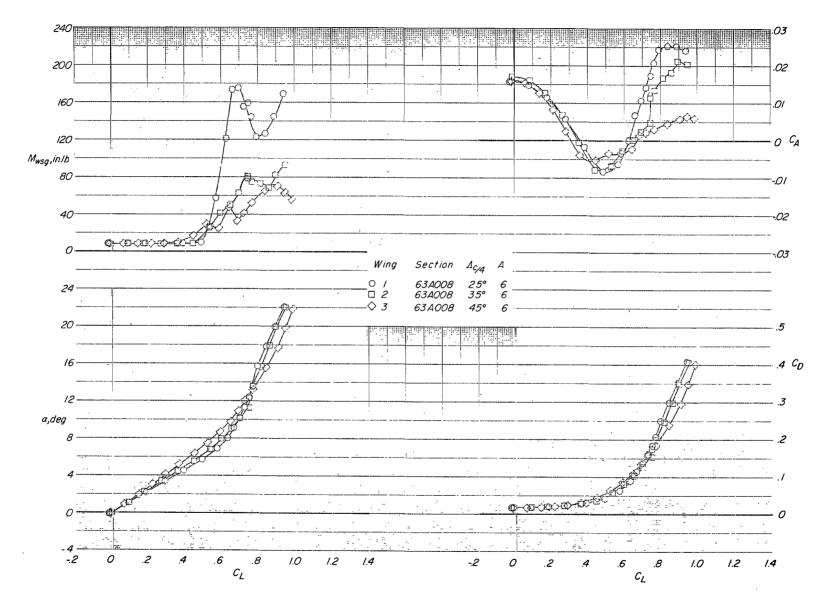


Figure 18.- Effect of wing sweep on the variations of  $M_{WSG}$ ,  $\alpha$ ,  $C_A$ , and  $C_D$  with  $C_L$ . (1 in. Ib = 0.113 m-N.)



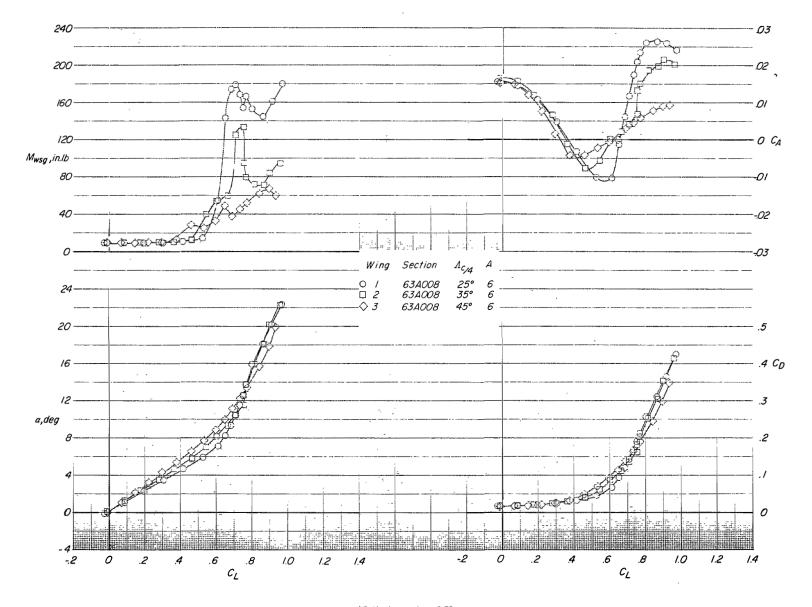
(b) Mach number, 0.46.

Figure 18.- Continued.



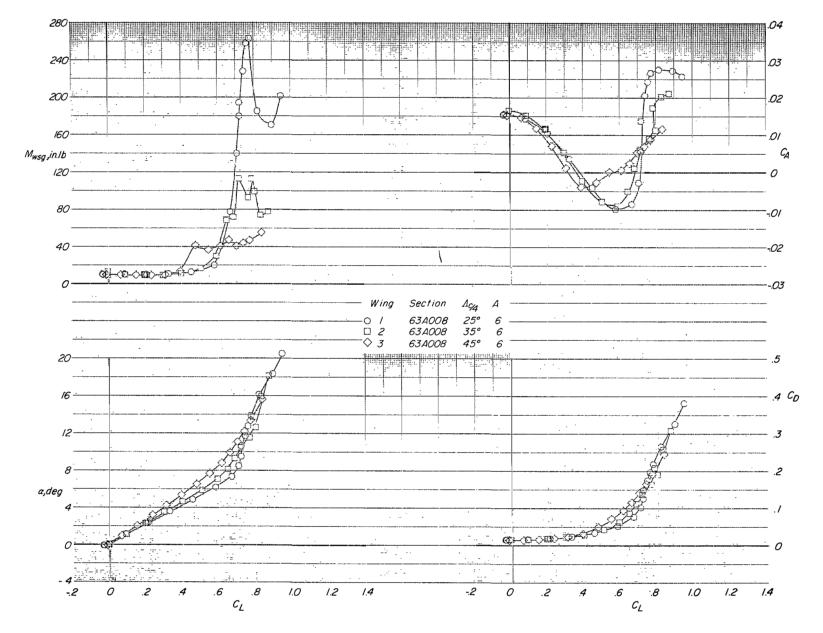
(c) Mach number, 0.67.

Figure 18.- Continued.



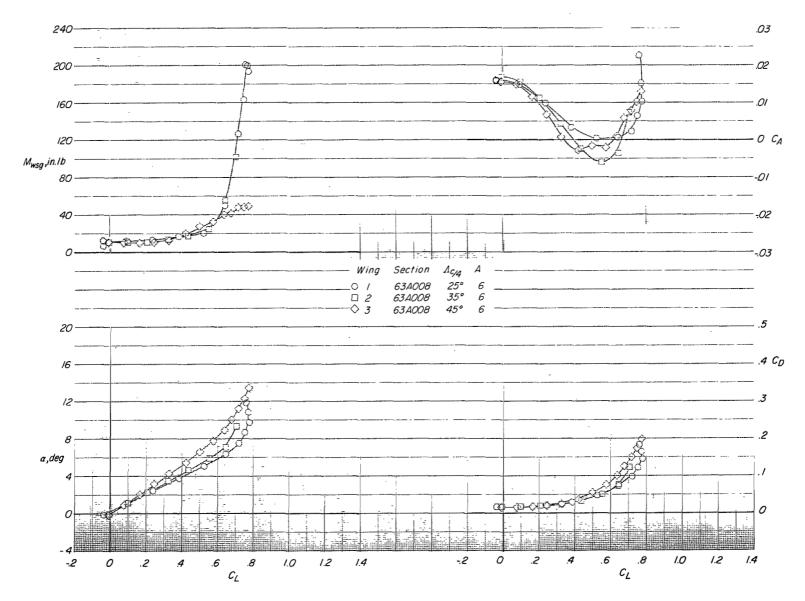
(d) Mach number, 0.72.

Figure 18.- Continued.



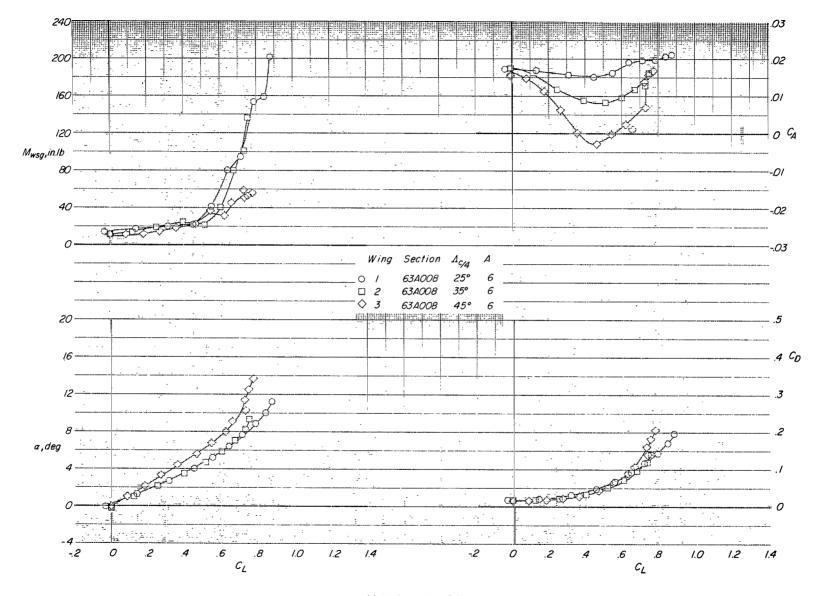
(e) Mach number, 0.77.

Figure 18.- Continued.



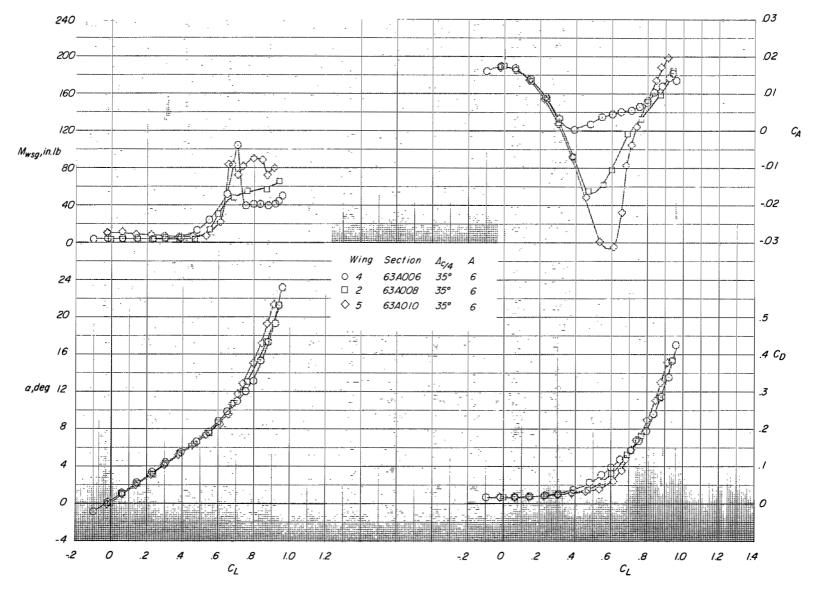
(f) Mach number, 0.82.

Figure 18.- Continued.



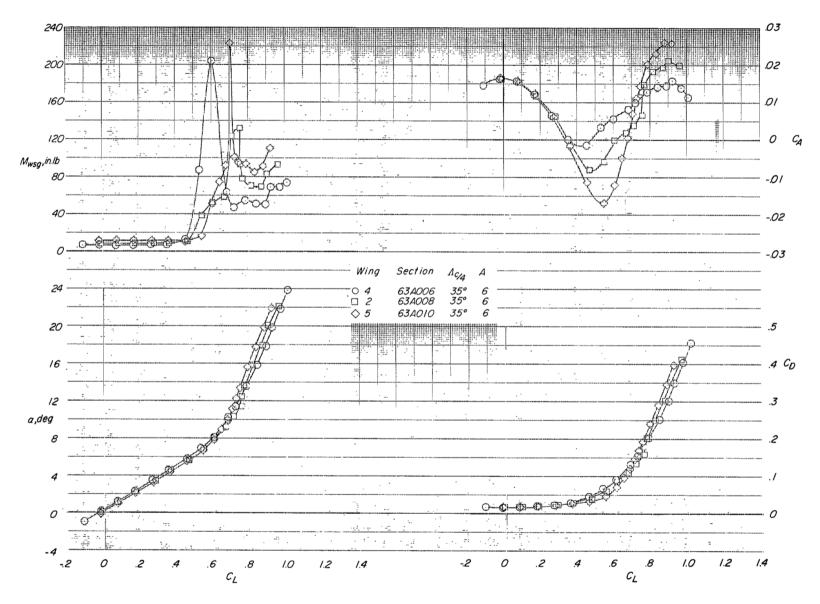
(g) Mach number, 0.88.

Figure 18.- Concluded.



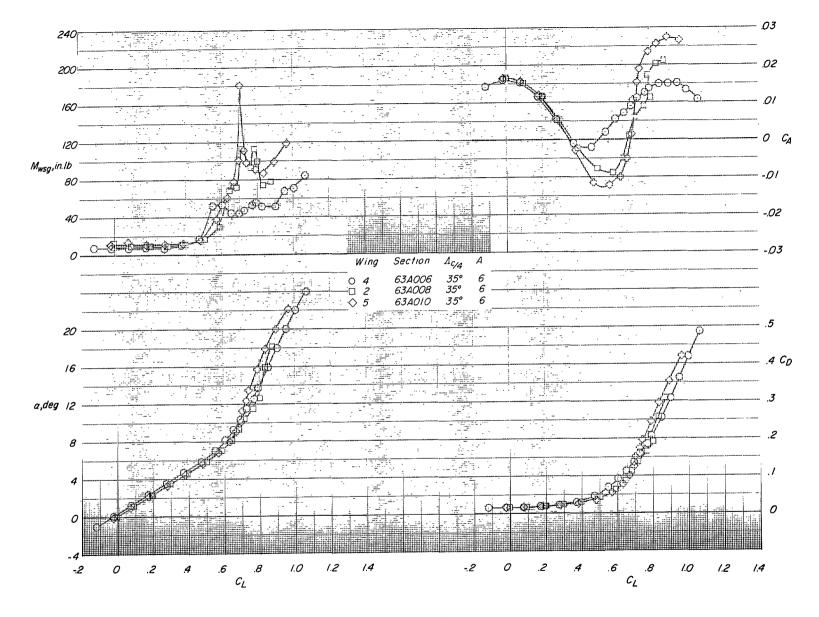
(a) Mach number, 0.46 for wing 2; 0.50 for wings 4 and 5.

Figure 19.- Effect of thickness-to-chord ratio on the variations of  $M_{WSQ}$ ,  $\alpha$ ,  $C_A$ , and  $C_D$  with  $C_L$ . (1 in. lb = 0.113 m-N.)



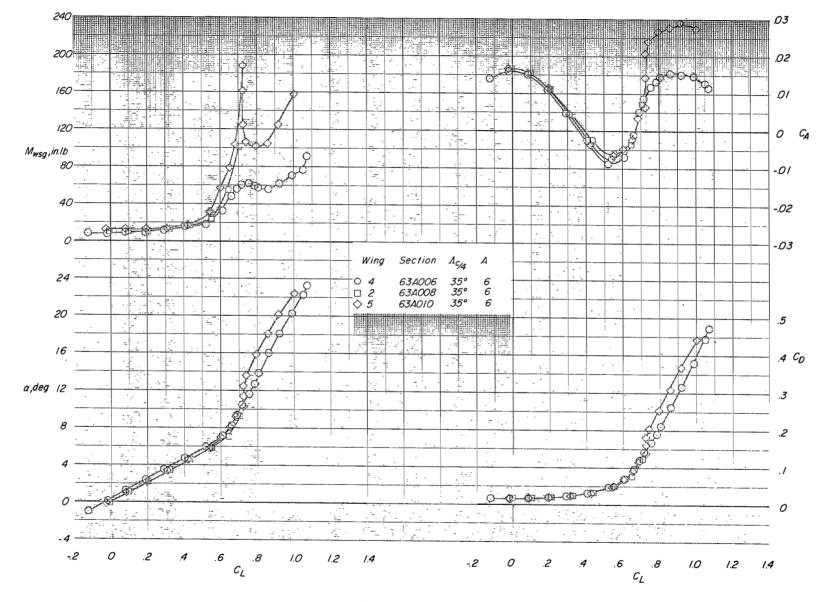
(b) Mach number, 0.71.

Figure 19.- Continued.

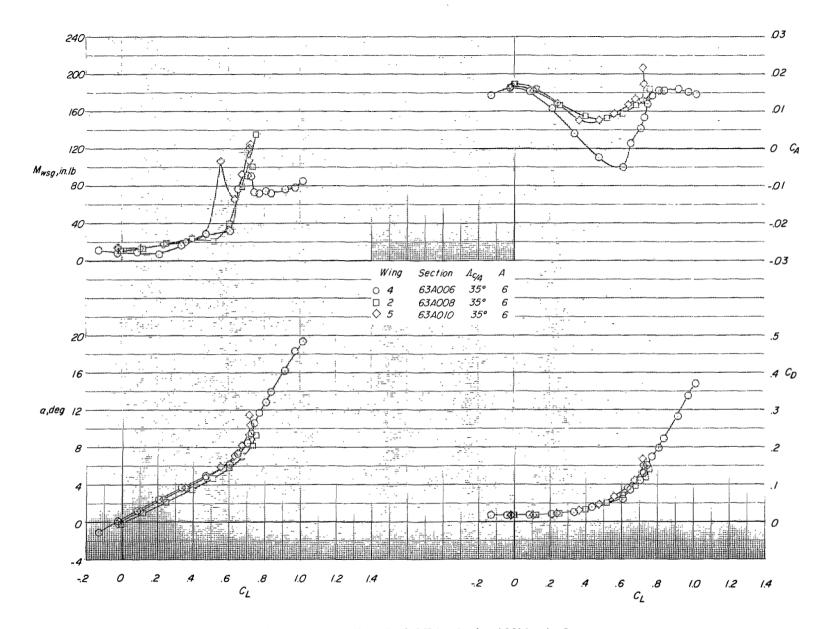


(c) Mach number, 0.76.

Figure 19.- Continued.

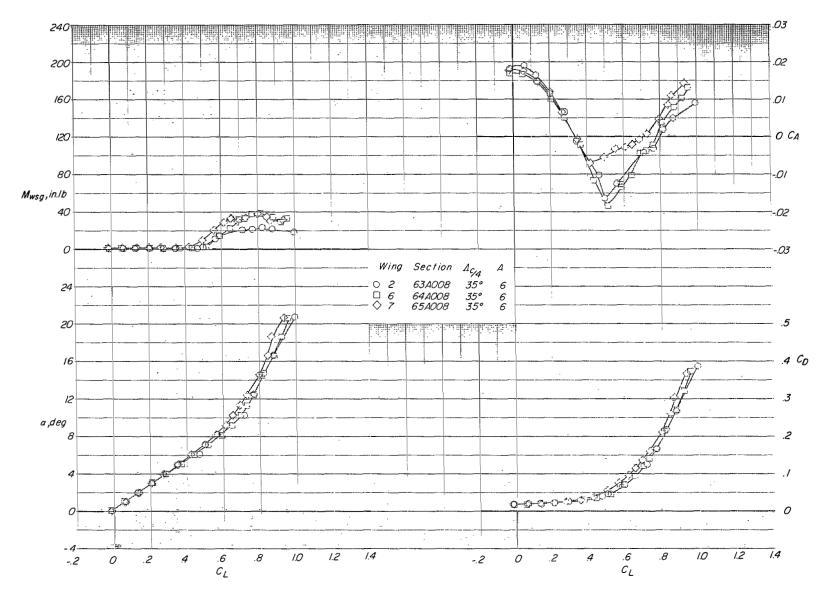


(d) Mach number, 0.81. Figure 19.- Continued.



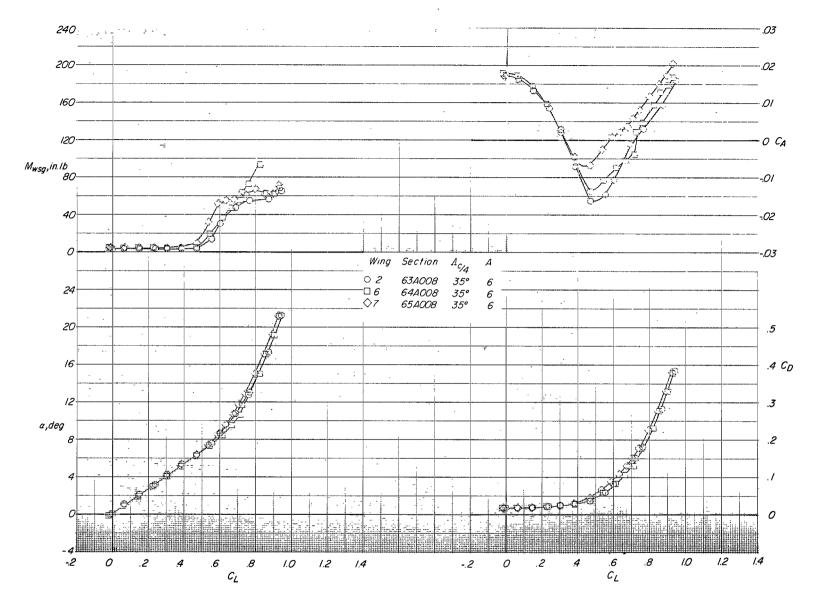
(e) Mach number, 0.88 for wing 2; 0.87 for wing 4; and 0.86 for wing 5.

Figure 19.- Concluded.



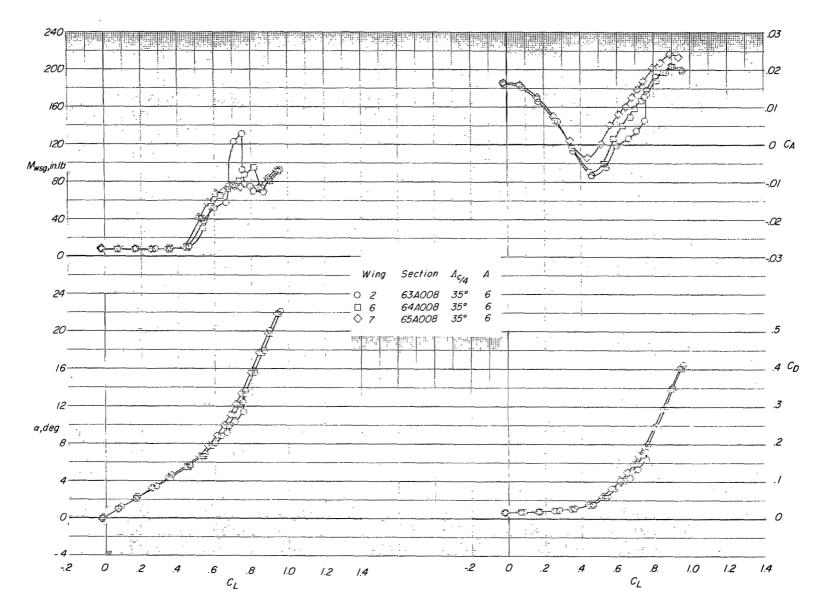
(a) Mach number, 0.23 for wing 2; 0.29 for wings 6 and 7.

Figure 20.- Effect of position of maximum thickness on the variations of  $M_{WSG}$ ,  $\alpha$ ,  $C_A$ , and  $C_D$  with  $C_L$ . (1 in. Ib = 0.113 m-N.)



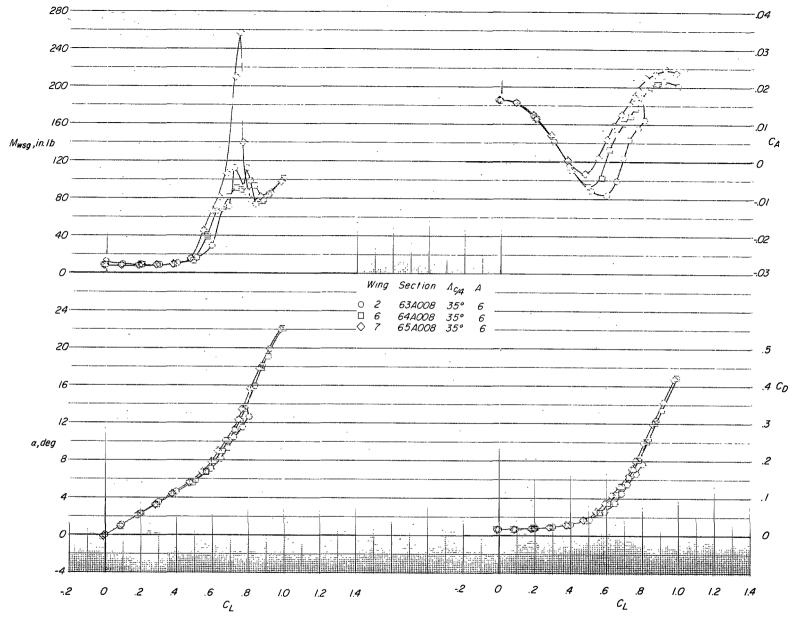
(b) Mach number, 0.46 for wing 2; 0.50 for wings 6 and 7.

Figure 20.- Continued.



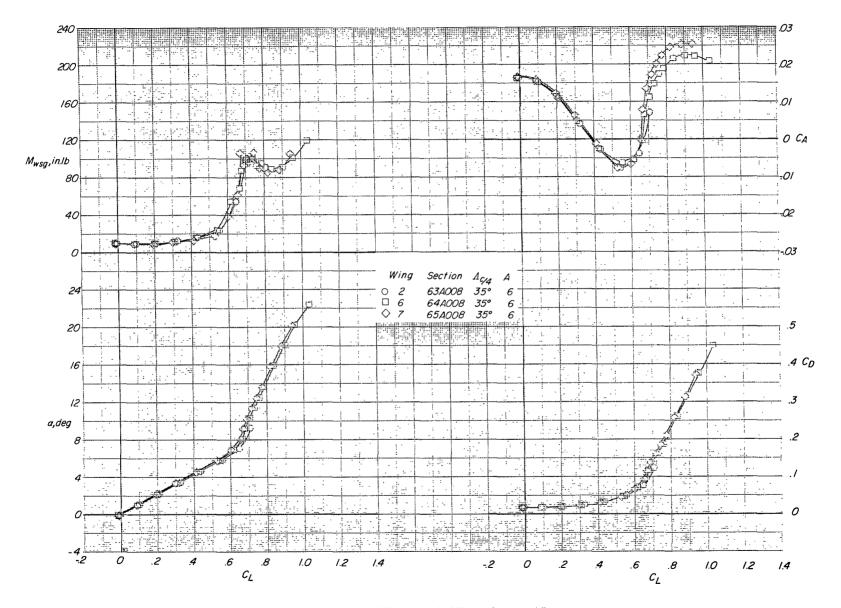
(c) Mach number, 0.72 for wing 2; 0.70 for wings 6 and 7.

Figure 20.- Continued.



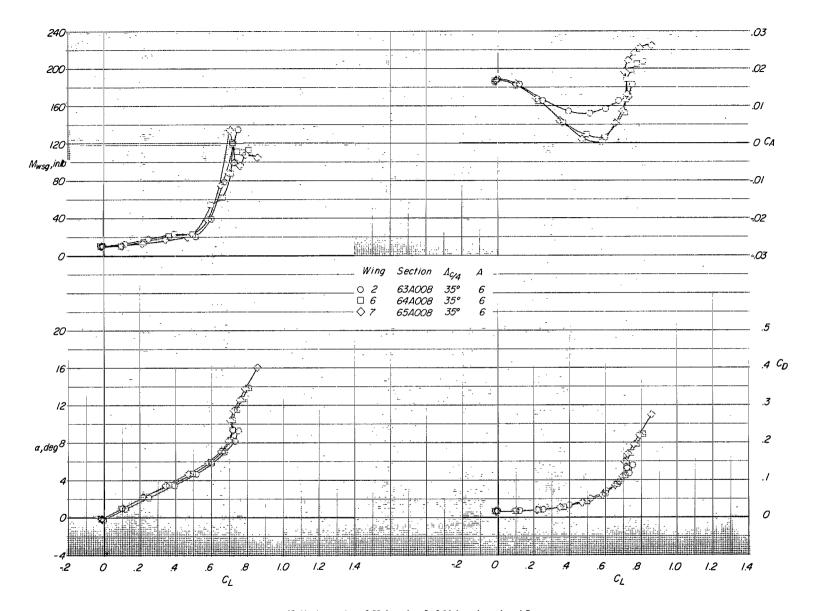
(d) Mach number, 0.77 for wing 2; 0.76 for wings 6 and 7.

Figure 20.- Continued.



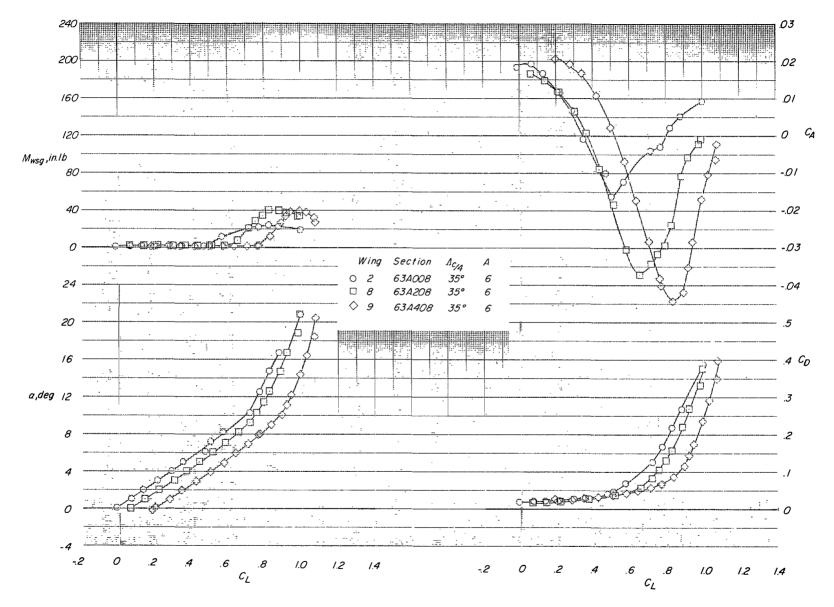
(e) Mach number, 0.82 for wing 2; 0.81 for wings 6 and 7.

Figure 20.- Continued.



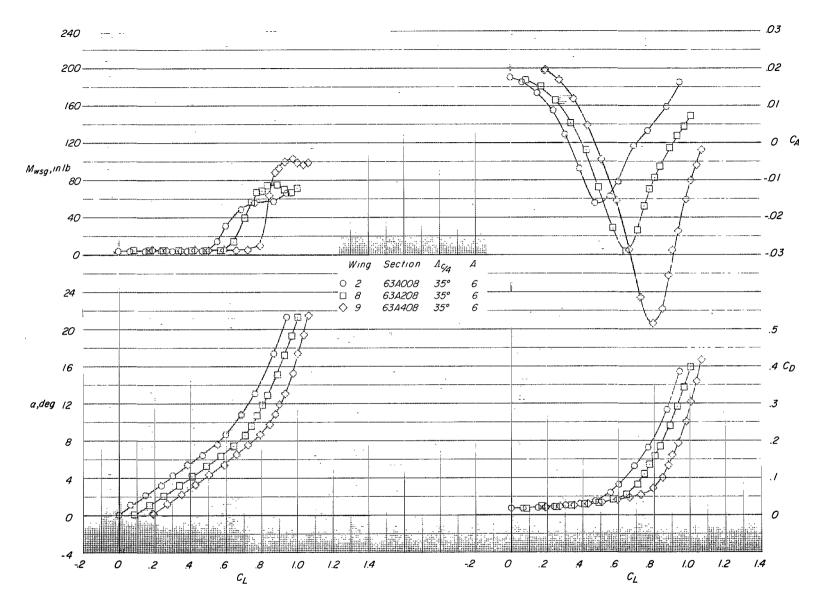
(f) Mach number, 0.88 for wing 2; 0.86 for wings 6 and 7.

Figure 20.- Concluded.



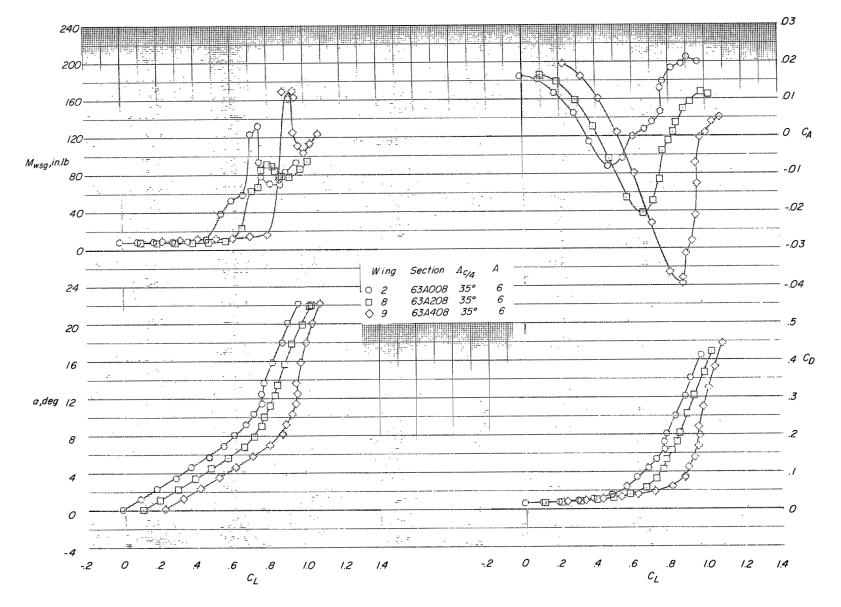
(a) Mach number, 0.23 for wings 2 and 9; 0.29 for wing 8.

Figure 21.- Effect of camber on the variations of  $M_{WSQ}$ ,  $\alpha$ ,  $C_A$ , and  $C_D$  with  $C_L$ . (1 in. lb = 0.113 m-N.)



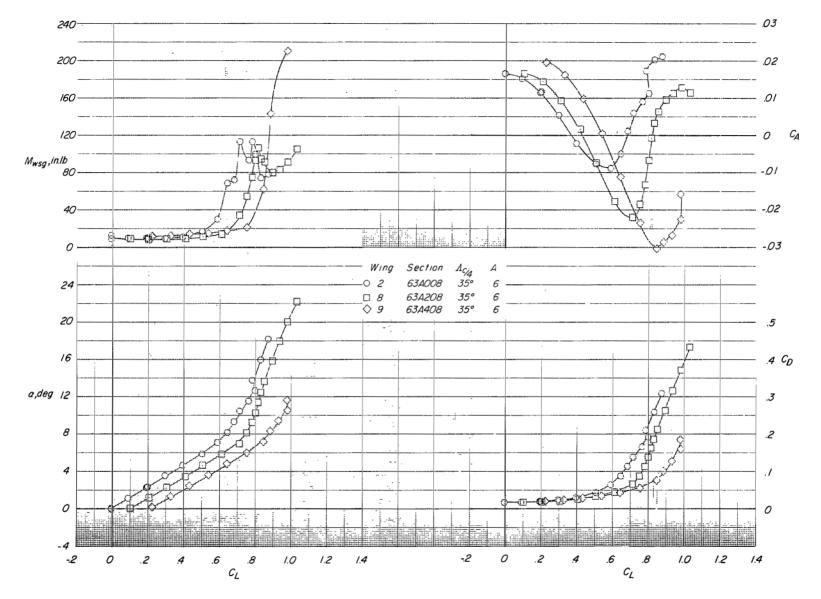
(b) Mach number, 0.46 for wings 2 and 9; 0.50 for wing 8.

Figure 21.- Continued.



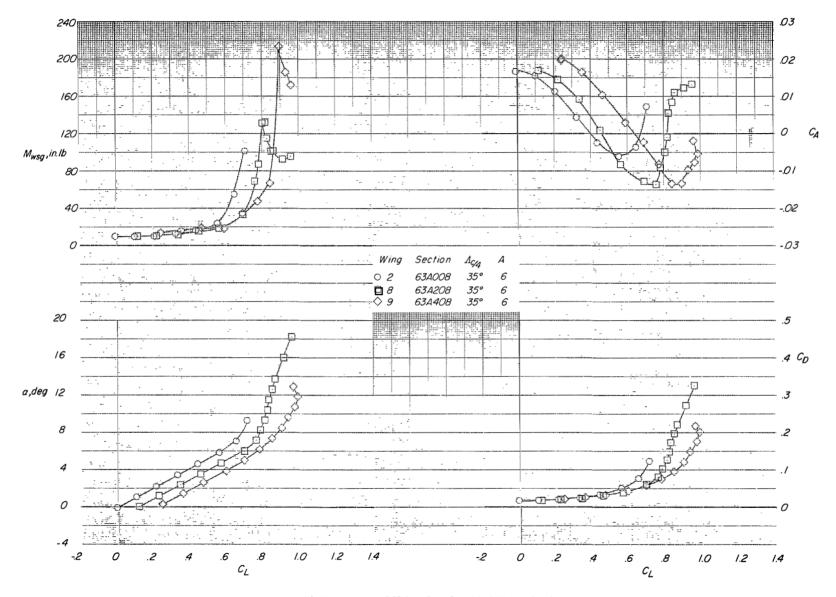
(c) Mach number, 0.72 for wings 2 and 9; 0.70 for wing 8.

Figure 21.- Continued.



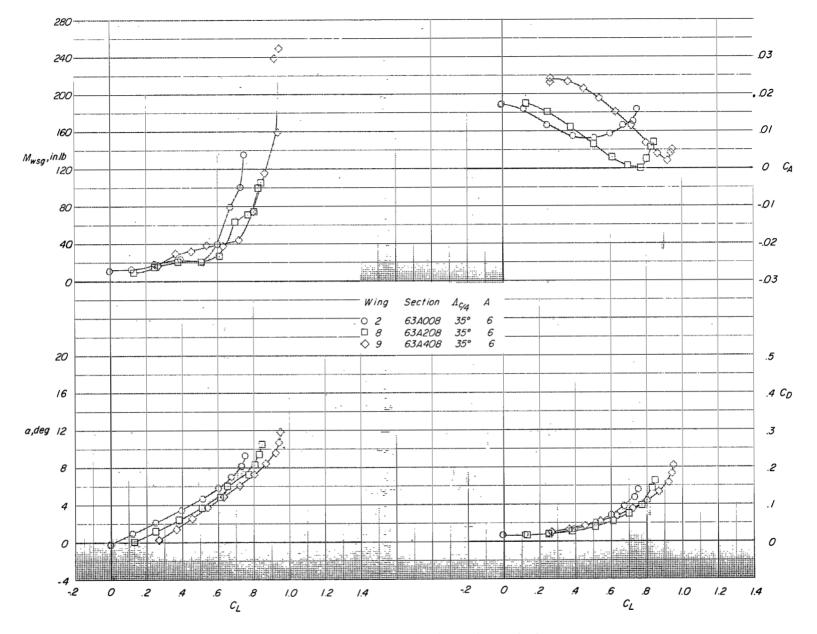
(d) Mach number, 0.77 for wings 2 and 9; 0.75 for wing 8.

Figure 21.- Continued.



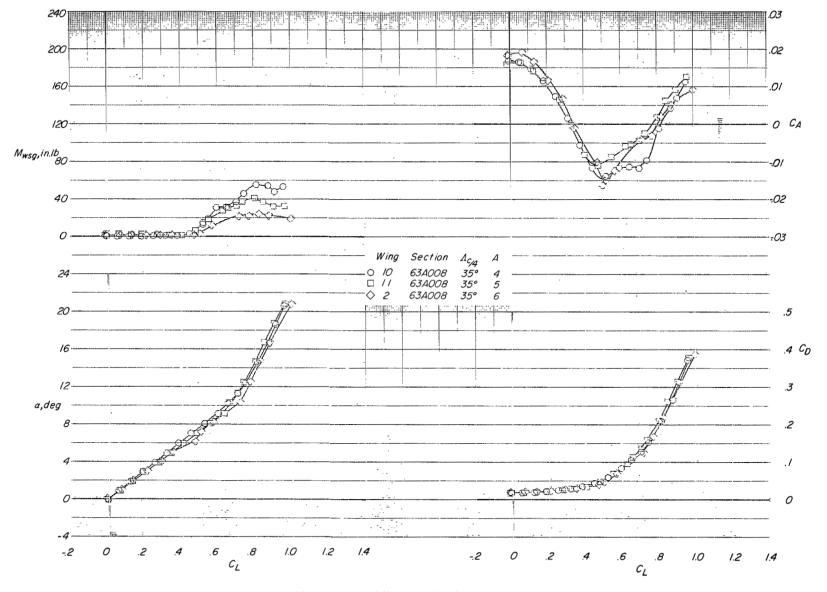
(e) Mach number, 0.82 for wings 2 and 9; 0.81 for wing 8.

Figure 21.- Continued.



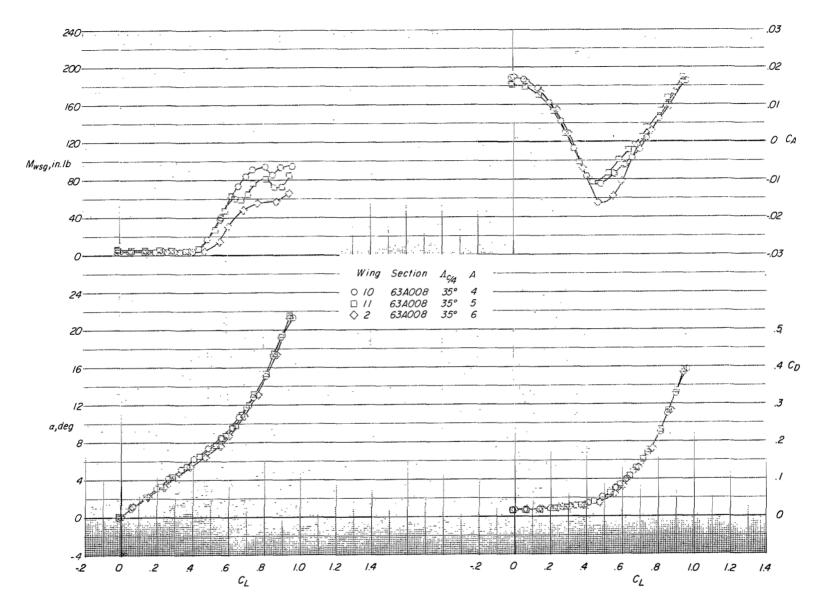
(f) Mach number, 0.88 for wings 2 and 9; 0.86 for wing 8.

Figure 21.- Concluded.



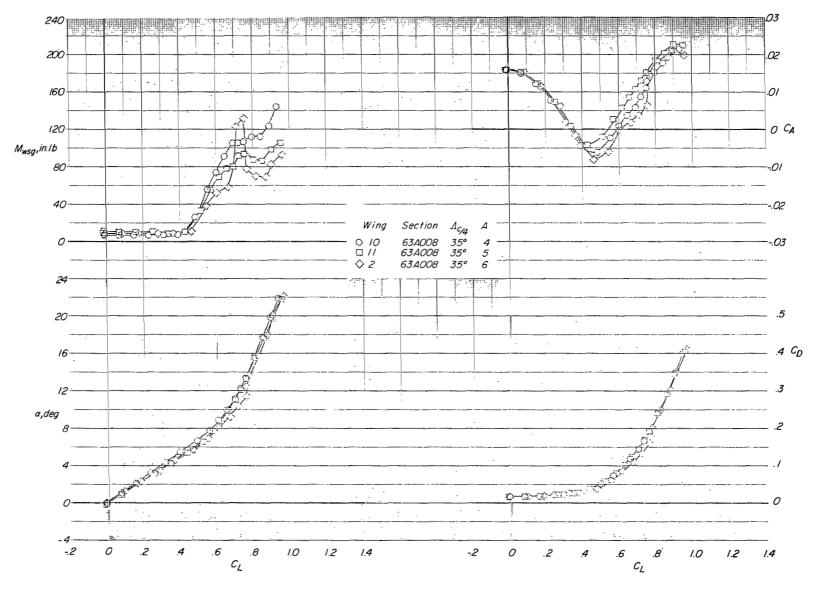
(a) Mach number, 0.23 for wing 2; 0.29 for wings 10 and 11.

Figure 22.- Effect of aspect ratio on the variations of  $M_{WSG}$ ,  $\alpha$ ,  $C_A$ , and  $C_D$  with  $C_L$ . (1 in. lb = 0.113 m-N.)



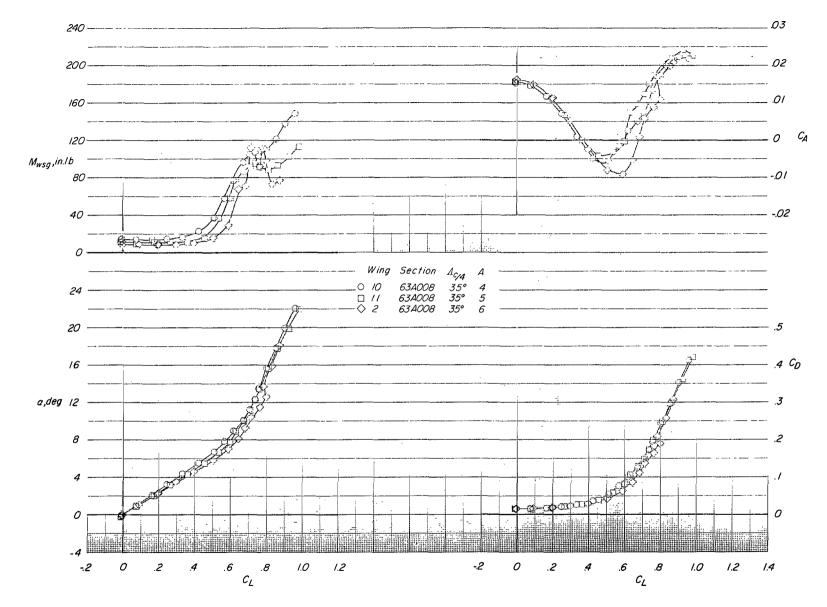
(b) Mach number, 0.46 for wing 2; 0.50 for wings 10 and 11.

Figure 22.- Continued.



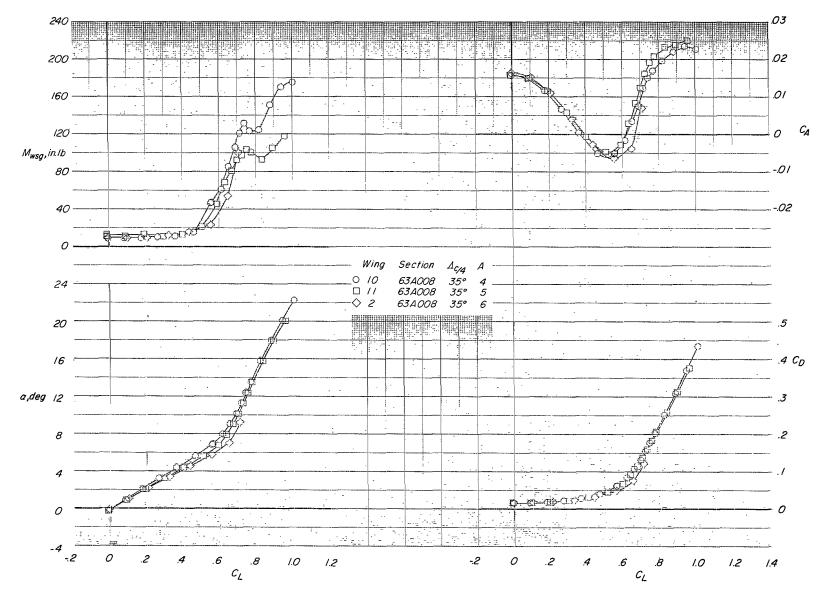
(c) Mach number, 0.72 for wing 2; 0.70 for wings 10 and 11.

Figure 22.- Continued.



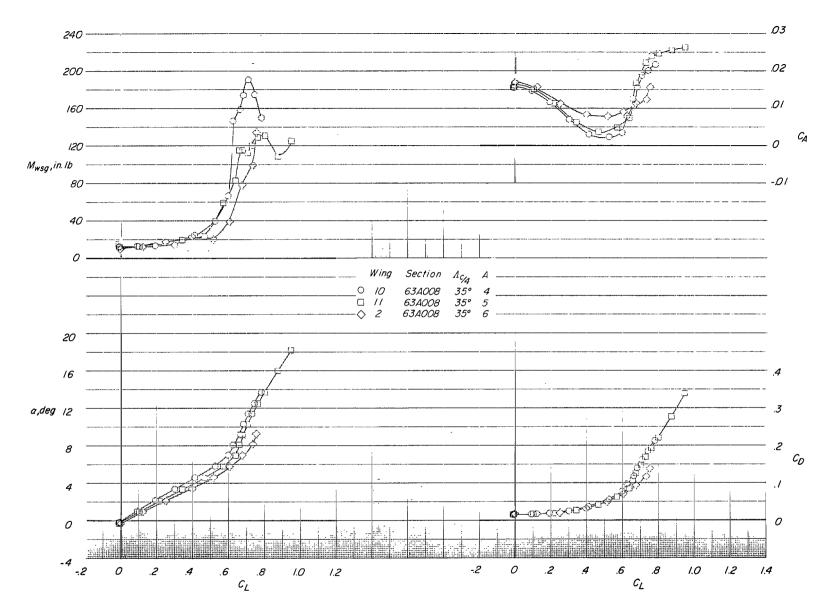
(d) Mach number, 0.77 for wing 2; 0.75 for wings 10 and 11.

Figure 22.- Continued.



(e) Mach number, 0.82 for wing 2; 0.81 for wings 10 and 11.

Figure 22.- Continued.



(f) Mach number, 0.88 for wing 2; 0.86 for wings 10 and 11.

Figure 22.- Concluded.

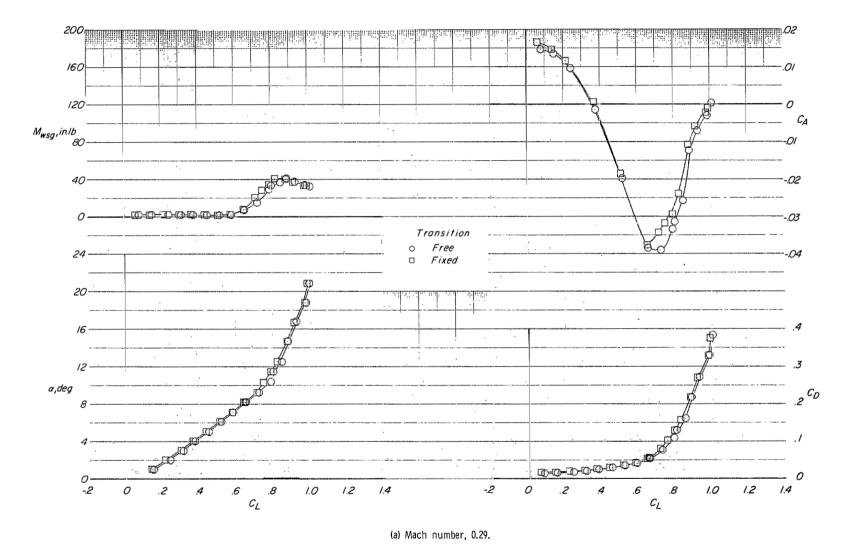
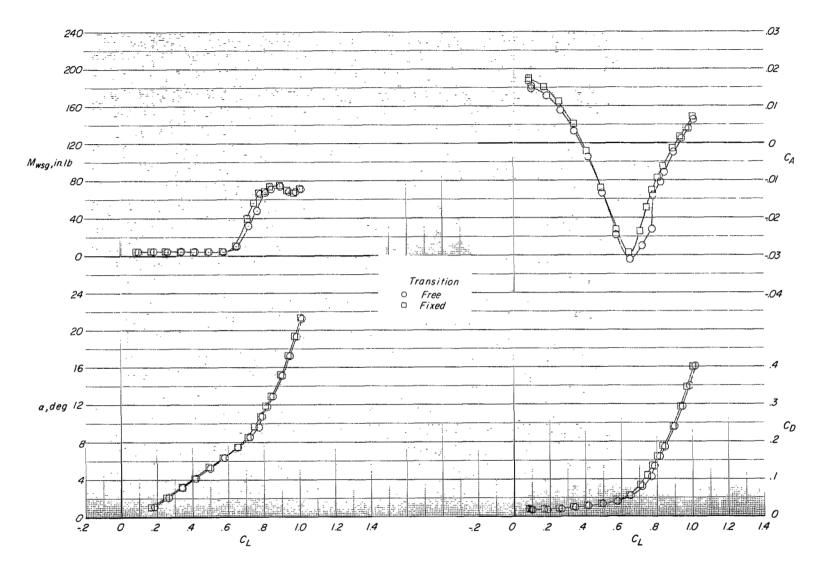
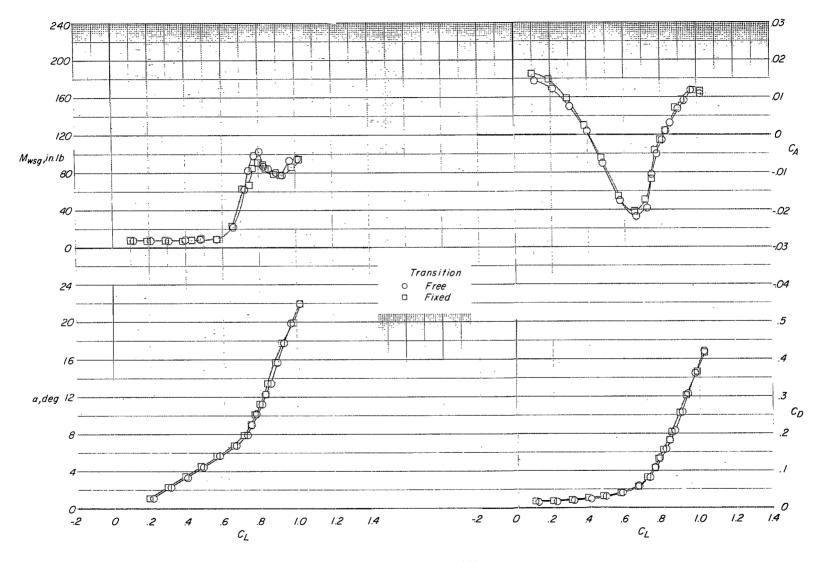


Figure 23.- Effect of transition grit on the variations of  $M_{WSG}$ ,  $\alpha$ ,  $C_A$ , and  $C_D$  with  $C_L$  for wing 8. (1 in. lb = 0.113 m-N.)



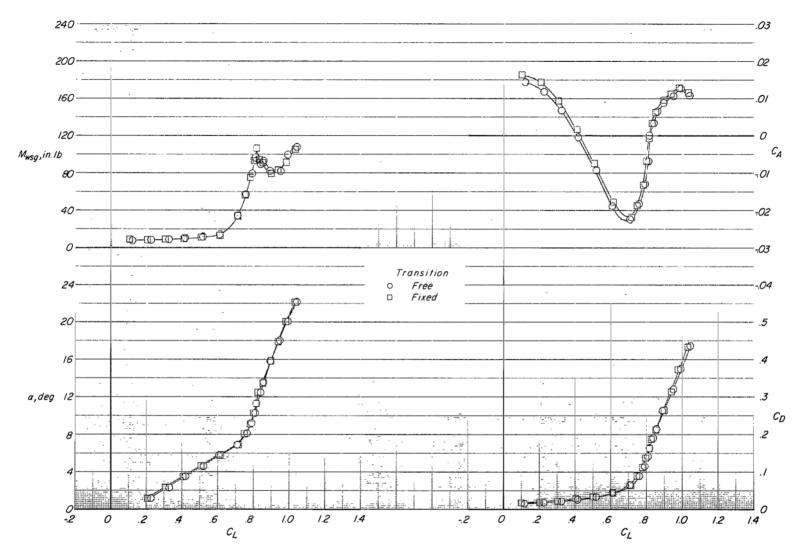
(b) Mach number, 0.50.

Figure 23.- Continued.



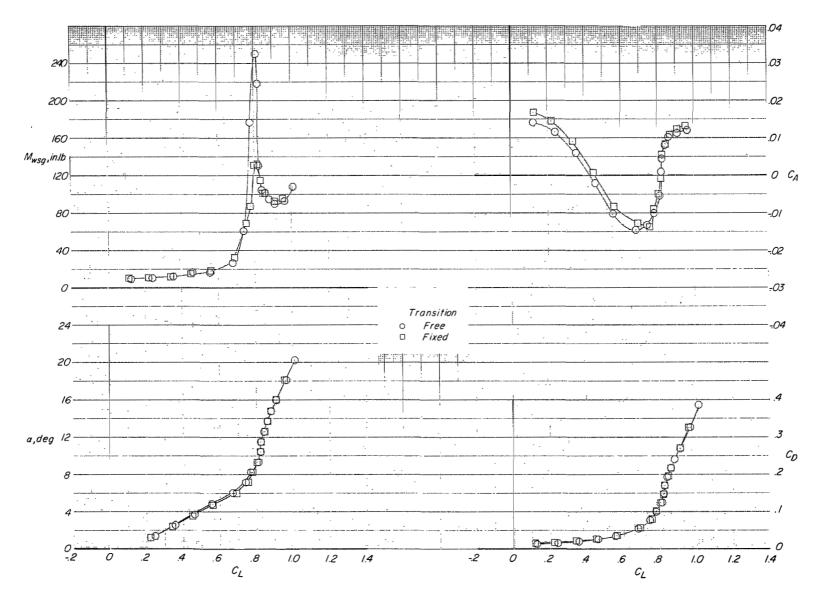
(c) Mach number, 0.70.

Figure 23.- Continued.



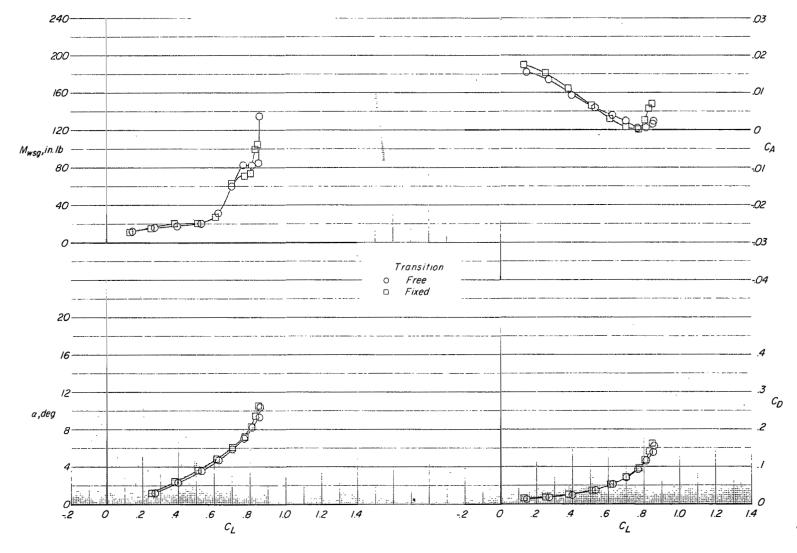
(d) Mach number, 0.75.

Figure 23.- Continued.



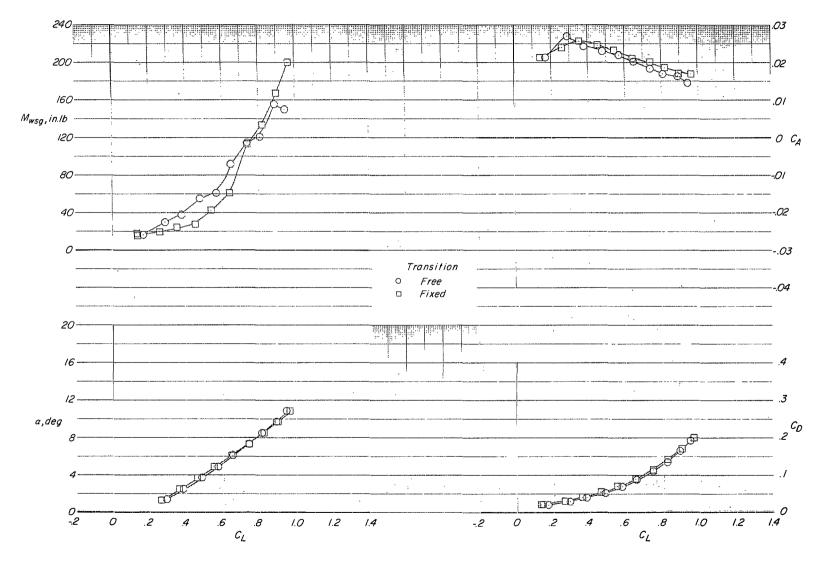
(e) Mach number, 0.81.

Figure 23.- Continued.



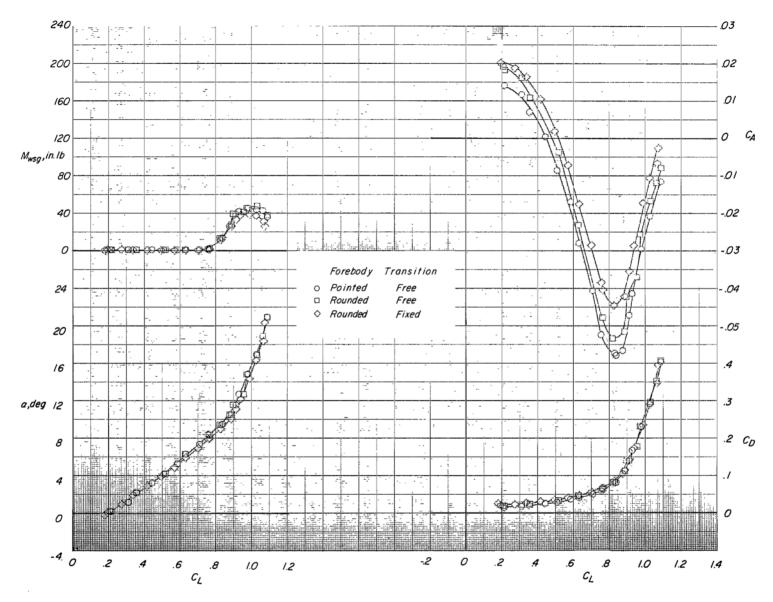
(f) Mach number, 0.86.

Figure 23.- Continued.



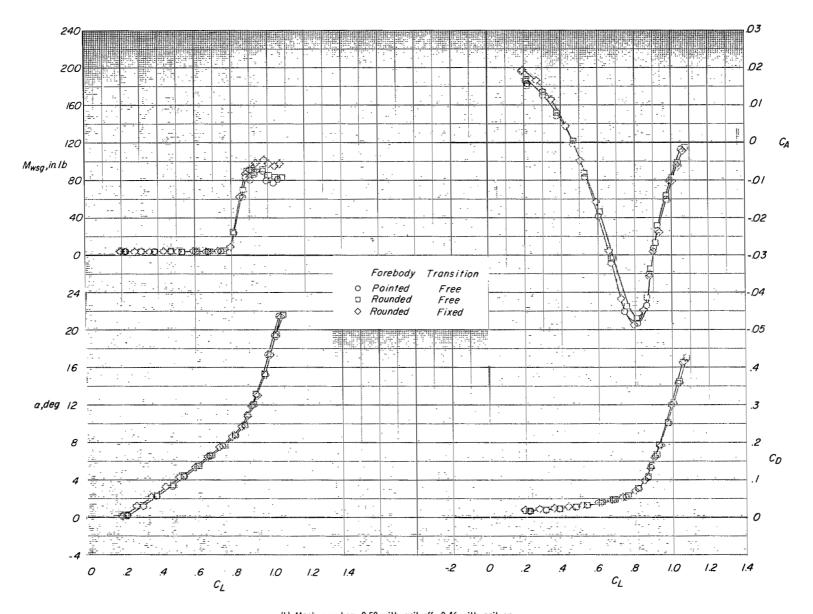
(g) Mach number, 0.93.

Figure 23.- Concluded.



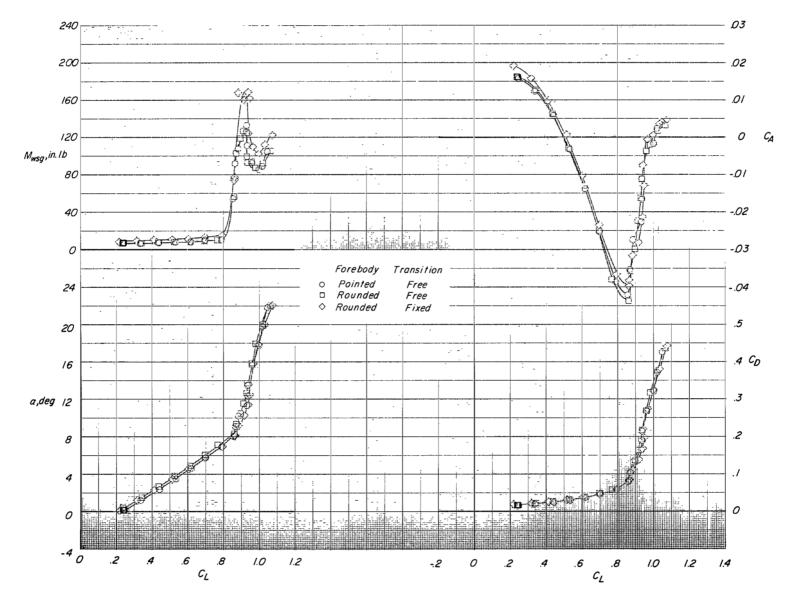
(a) Mach number, 0.29 with grit off; 0.23 with grit on.

Figure 24.- Effect of forebody shape and transition grit on the variations of  $M_{WSG}$ ,  $\alpha$ ,  $C_A$ , and  $C_D$  with  $C_L$  for wing 9. (1 in. lb = 0.113 m-N.)



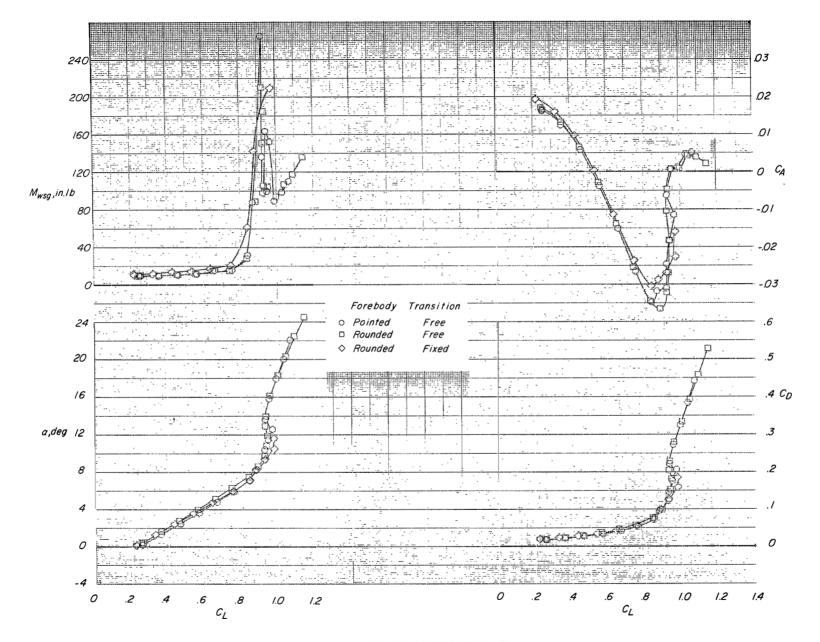
(b) Mach number, 0.50 with grit off; 0.46 with grit on.

Figure 24.- Continued.



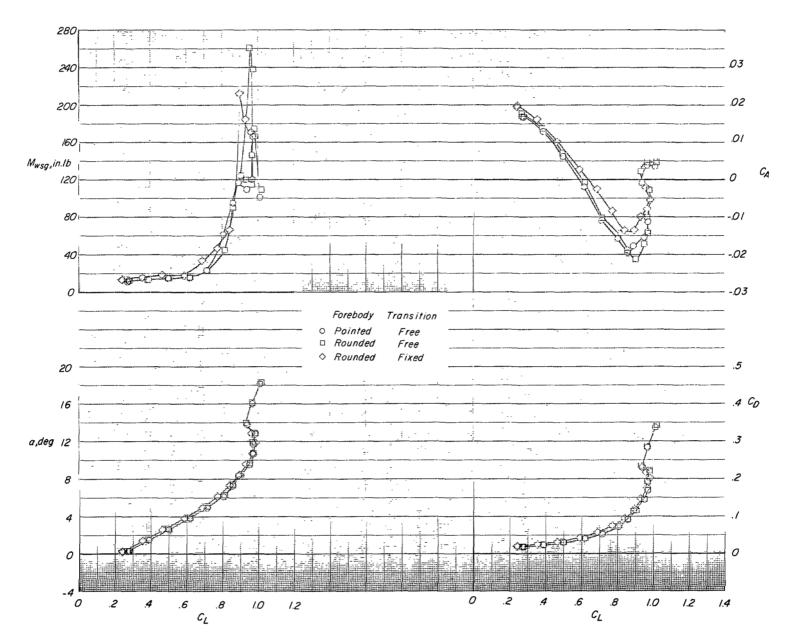
(c) Mach number, 0.70 with grit off; 0.72 with grit on.

Figure 24.- Continued.



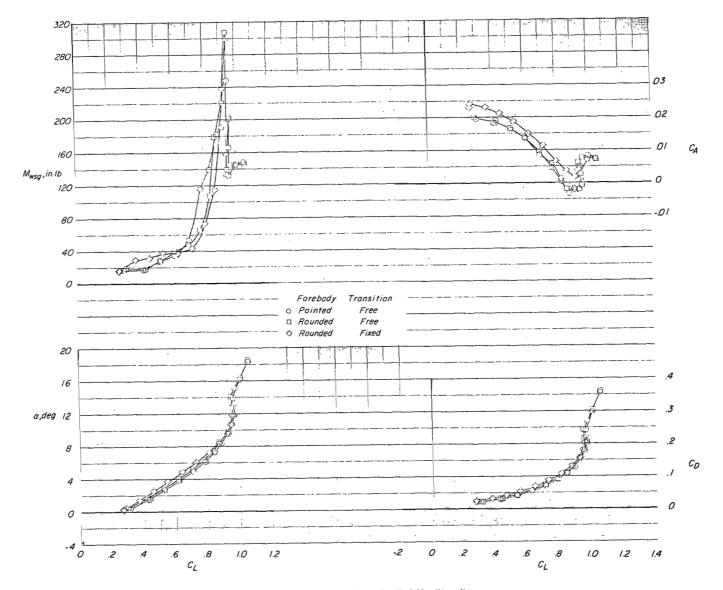
(d) Mach number, 0.75 with grit off; 0.77 with grit on.

Figure 24.- Continued.



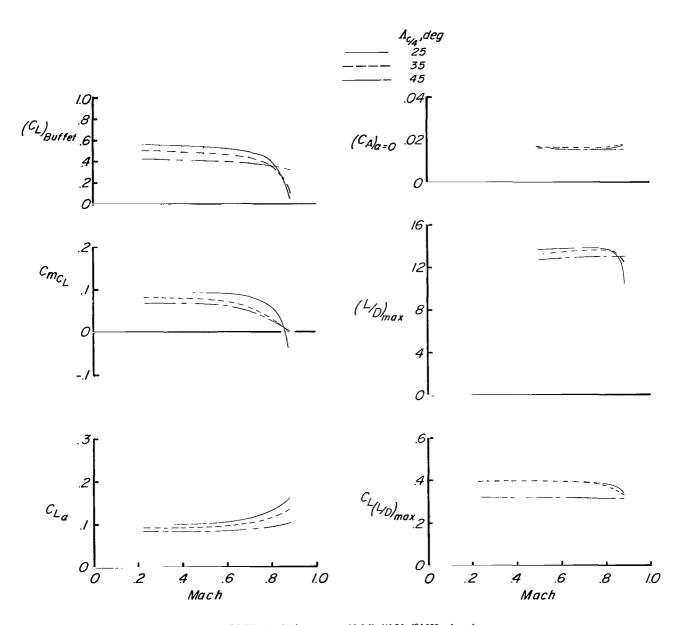
(e) Mach number, 0.81 with grit off; 0.82 with grit on.

Figure 24.- Continued.



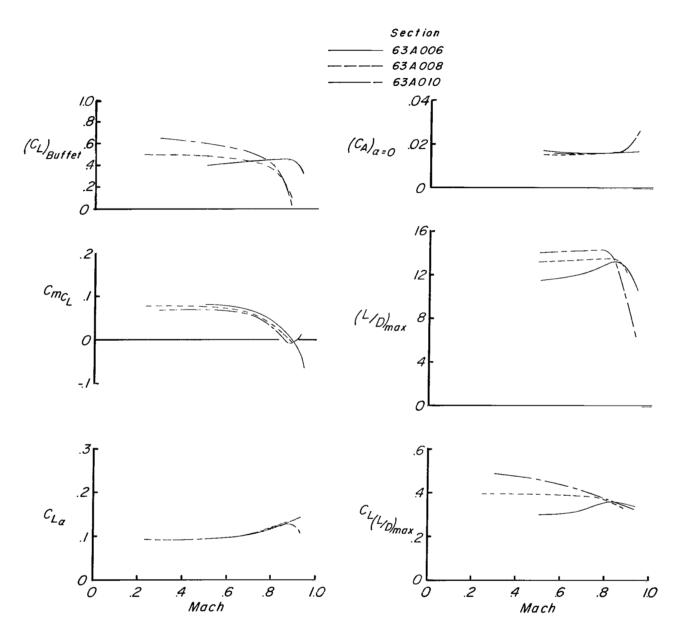
(f) Mach number, 0.86 with grit off; 0.88 with grit on.

Figure 24.- Concluded.



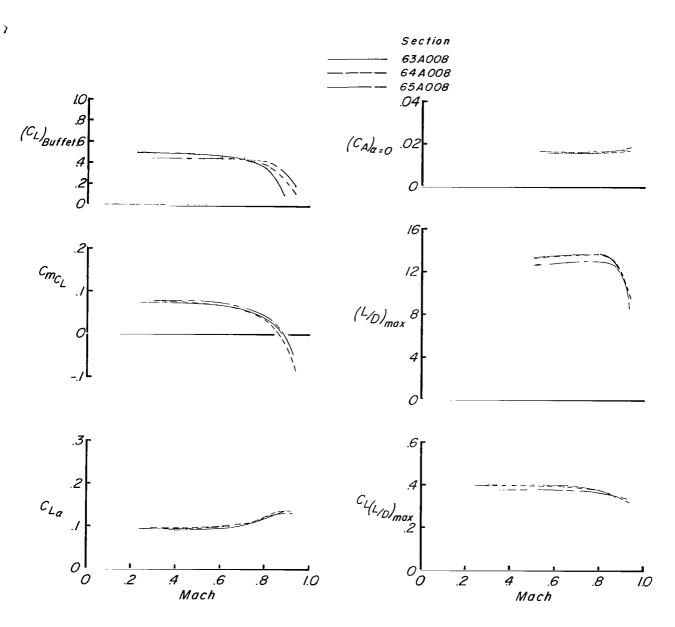
(a) Effects of wing sweep. Airfoil, NACA 63A008; A = 6.

Figure 25.- Summaries of the longitudinal aerodynamic and buffet characteristics of the test configurations.



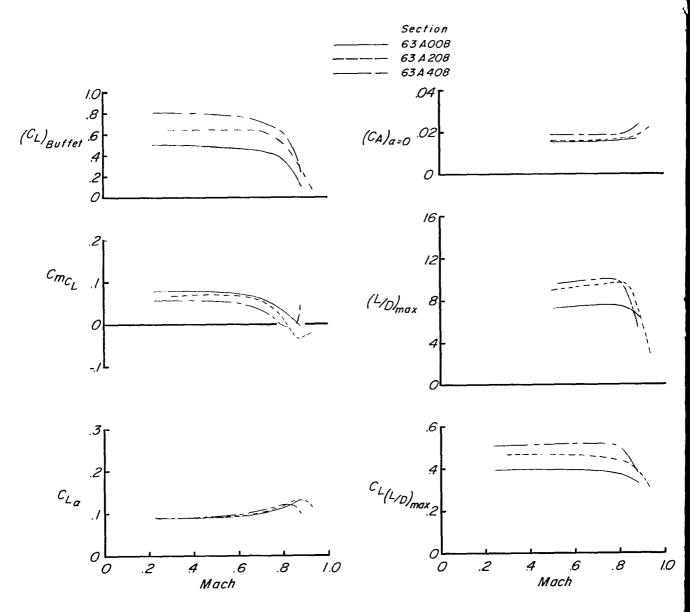
(b) Effects of thickness-to-chord ratio.  $\Lambda_{C/4} = 35^{\circ}$ ; A = 6.

Figure 25.- Continued.

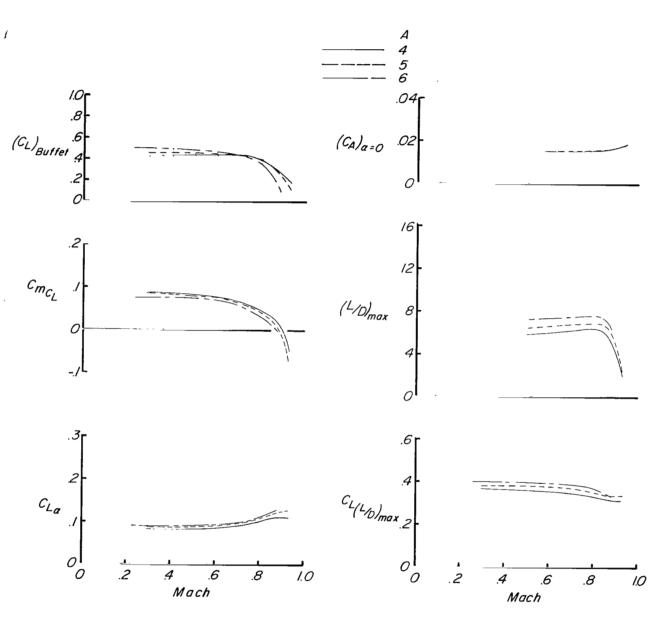


(c) Effects of position-of-maximum thickness.  $\Lambda_{c/4} = 35^{\circ}$ ; A = 6.

Figure 25.- Continued.



(d) Effects of camber.  $\Lambda_{\rm C/4}=35^{\rm o};~\rm A=6.$  Figure 25.- Continued.



(e) Effects of aspect ratio. Airfoil, NACA 63A008;  $\Lambda_{\text{C}/\text{4}} = 35^{\circ}$ . Figure 25.- Concluded.

NASA-Langley, 1970 — 1 L-7011

# NATIONAL AERONAUTICS AND SPACE ADMINISTRATION WASHINGTON, D. C. 20546

OFFICIAL BUSINESS

## FIRST CLASS MAIL



POSTAGE AND FEES PAID NATIONAL AERONAUTICS A SPACE ADMINISTRATION

OBU OOL 26 51 BDS 70165 00903 AIR FORCE WEAPONS LABORATORY /WEGE/ KIKTLAND AFB, NEW MEXICO 87117

ATT & LOW BALL OF CHIEF . TICHE I LASTRY

POSTMASTER:

If Undeliverable (Section 15 Postal Manual) Do Not Reti

"The aeronautical and space activities of the United States shall be conducted so as to contribute . . . to the expansion of human knowledge of phenomena in the atmosphere and space. The Administration shall provide for the widest practicable and appropriate dissemination of information concerning its activities and the results thereof."

- NATIONAL AERONAUTICS AND SPACE ACT OF 1958

## NASA SCIENTIFIC AND TECHNICAL PUBLICATIONS

TECHNICAL REPORTS: Scientific and technical information considered important, complete, and a lasting contribution to existing knowledge.

TECHNICAL NOTES: Information less broad in scope but nevertheless of importance as a contribution to existing knowledge.

## TECHNICAL MEMORANDUMS:

Information receiving limited distribution because of preliminary data, security classification, or other reasons.

CONTRACTOR REPORTS: Scientific and technical information generated under a NASA contract or grant and considered an important contribution to existing knowledge.

TECHNICAL TRANSLATIONS: Information published in a foreign language considered to merit NASA distribution in English.

SPECIAL PUBLICATIONS: Information derived from or of value to NASA activities. Publications include conference proceedings, monographs, data compilations, handbooks, sourcebooks, and special bibliographies.

#### TECHNOLOGY UTILIZATION

PUBLICATIONS: Information on technology used by NASA that may be of particular interest in commercial and other non-aerospace applications. Publications include Tech Briefs, Technology Utilization Reports and Technology Surveys.

Details on the availability of these publications may be obtained from:

SCIENTIFIC AND TECHNICAL INFORMATION DIVISION

NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

Washington, D.C. 20546